

**FINAL**



# **SHEPLEY'S HILL LANDFILL SUPPLEMENTAL GROUNDWATER AND LANDFILL CAP ASSESSMENT FOR LONG-TERM MONITORING AND MAINTENANCE – ADDENDUM REPORT**

**SHEPLEY'S HILL LANDFILL**

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**FORMER FORT DEVENS ARMY INSTALLATION, DEVENS, MA**

**AUGUST 2011**

**BOOK 1 OF 4**

**Prepared for:  
US Army Corp of Engineers  
New England District  
Concord, Massachusetts**

**Prepared by:  
Sovereign Consulting Inc.  
Contract No.: W912WJ-10-D-0003  
Delivery Order: 0002**



# TRANSMITTAL MEMO

## Copies

To: Ginny Lombardo – USEPA CD / Attachments  
David Chaffin – MADEP CD / Attachments  
Hui Liang – MADEP CD / Attachments  
Carolyn L. McCreary – Ayer Board of Selectmen CD / Attachments  
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From: Philip McBain – Sovereign Consulting Inc.

Cc: Bob Simeone – BEC, Devens RFTA CD / Daptiv / Attachments  
Ellen Iorio – USACE New England District 2 - CD / Daptiv / Attachments  
USACE Omaha NE – HTRW CX CD  
Marc Cicalese – Sovereign Consulting CD / Attachments  
Ron Ostrowski – Mass Development CD / Attachments  
(including 1 copy to Haley & Aldrich)

Date 19 August 2011

Subject: **Shepley's Hill Landfill – Supplemental Groundwater and Landfill Cap  
Assessment for Long-term Monitoring and Maintenance Addendum Report  
(Final Version)**  
Contract Number GS-10F-0230J, Delivery Order W912WJ-05-F-0037

On behalf of the US Army Corps of Engineers (USACE) New England District and the Army BRAC Environmental Office at Devens, Sovereign is pleased to provide the following attachments:

1. CD
2. Binder Cover Pages and Spines
3. Replacement Report Text
4. Replacement Figure 30
5. Insert to Supplement Appendix I
6. Insert to Supplement Appendix K

These items are provided to update the May 2011 version of the Shepley's Hill Landfill Supplemental Groundwater and Landfill Cap Assessment for Long-term Monitoring and maintenance Addendum Report.

Please contact Bob Simeone or myself, if there are questions regarding the attachments

Sincerely



Philip D McBain, LSP  
Project Manager

Enclosure: As noted above



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Ron Ostrowski – Mass Development CD / Attachments  
Marc Cicalese – Sovereign Consulting CD / Attachments  
(including 1 copy to Haley & Aldrich)

Date 6 June 2011

Subject: **Shepley's Hill Landfill – Supplemental Groundwater and Landfill Cap  
Assessment for Long-term Monitoring and Maintenance Addendum Report  
(Army Draft)**  
Contract Number GS-10F-0230J, Delivery Order W912WJ-05-F-0037

On behalf of the US Army Corps of Engineers (USACE) New England District and the Army BRAC Environmental Office at Devens, Sovereign is pleased to provide the following attachments:

1. CD
2. Binder Cover Pages and Spines
3. Replacement Report Text
4. Replacement Figures (2-28, 45, and 55-57)
5. Replacement Table 2 and Table 7
6. Insert to Supplement Appendix I
7. New Appendix K
8. New Appendix L

These items are provided to update the December 2010 version of the Shepley's Hill Landfill Supplemental Groundwater and Landfill Cap Assessment for Long-term Monitoring and maintenance Addendum Report.

## TRANSMITTAL MEMO

Please contact Bob Simeone or myself, if there are questions regarding the attachments

Sincerely

Philip D McBain, LSP  
Project Manager

Enclosure: Shepley's Hill Landfill Supplemental Groundwater and Landfill Cap Assessment for Long-term Monitoring and Maintenance Addendum Report, May 2011.

**Army Response to MassDEP Comments dated 30 June 2011**  
**On**  
**DRAFT FINAL SHEPLEY'S HILL LANDFILL SUPPLEMENTAL GROUNDWATER AND LANDFILL CAP**  
**ASSESSMENT FOR LONG-TERM MONITORING AND MAINTENANCE – ADDENDUM REPORT**

**Former Fort Devens Army Installation**  
**August 5 2011**

1. Section 5.1: To address the discrepancies with the presumed bedrock depths acknowledged here (refer to MassDEP Comments 1 and 9 on the draft report), the Army agreed during the May 19, 2011 BCT meeting to install a monitoring well transect across Nonacoicus Brook in the vicinity of temporary well SHM-10-08. The well drilling method used to install the wells will be capable of confirming the presence of an east-west trending bedrock trough beneath the brook. Well screens will be placed at depths appropriate to serve as long-term monitoring points and sentinel well between the site and the MacPherson water supply well.

*Response: Such changes or enhancements to the current groundwater LTM network will be performed pending implementation of an updated remedy for SHL.*

2. Section 6.3: The supplemental analysis provided here does not strengthen the hypothesis that arsenic precipitates along a “redox boundary” in the vicinity of Nonacoicus Brook; valid alternative hypotheses remain (refer to MassDEP Comment 2 on the draft report):
  - The configured cross-sections C-C' and D-D' do not demonstrate that the plume terminated south of cross-section C-C'. An almost 200-foot gap through which the plume could extend to the northwest separates wells SHM-10-20 and SHM-10-26 on cross-section C-C'.
  - The results from the 2010 field effort indicate that vertical flow and discharge to Nonacoicus Brook and adjacent wetlands, rather than precipitation along a “redox boundary”, may explain the observed arsenic distribution. In particular, cross sections D-D' and F-F' indicate that the plume may ascend from depth to discharge points in Nonacoicus Brook and the adjacent wetlands (note the upward trajectory of the plume core between wells SHM-10-27 and SHM-10-21 in Figure 9 and between SHM-10-23 and SHM-10-19 in Figure 11).

Rather than undertaking additional studies in an attempt to obtain conclusive results, which may not be feasible due to the complex geochemical conditions in the vicinity of Nonacoicus Brook, the Army agreed during the May 19, 2011 BCT meeting to implement a surface water

and groundwater monitoring program that includes periodic collection and analysis of surface water samples from the portion of the brook where discharge of site-impacted groundwater may occur and installation of periodic sampling of a monitoring wells transect across Nonacoicus Brook in the vicinity of temporary well SHM-10-08 (refer to previous comment).

*Response:* The Army respectively disagrees. In regards to the 200-foot gap cited between SHM-10-20 and SHM-10-26, the wells SHM-10-21, SHM-10-10, and SHM-10-22 are located between this gap, but located along the upgradient D-D' cross-section line. The highest concentration reported within the profiling samples reported an arsenic concentration of 349-ug/l (SHM-10-21 at 41-foot sampling depth). The remaining two locations reported arsenic concentrations less than 2.5-ug/l. Higher concentrations of Arsenic were reported within wells SHM-10-21, SHM-19, and SHM-10-17, which are east of this gap, and evaluated by the downgradient wells SHM-10-20 and SHM-10-18. These wells indicate a reduction in the dissolved arsenic concentrations from a high of 1,860-ug/l (D-D' line in well SHM-10-17) to a concentration of 429-ug/l (C-C' line in well SHM-10-20).

Bedrock contouring also plays a part in this upward trend reflected in Figures 9 and 10. Next, surface water and sediment sampling conducted by Harding in 2002 and AMEC in 2007 show no conclusive evidence that SHL is a source of a surface water / sediment impact. Each of these two sampling programs reported the highest arsenic concentrations within samples obtained from the upstream Sawmill Brook sampling points. Future surface water / sediment sampling will be performed periodically to confirm these results pending implementation of an updated remedy for SHL.

3. Section 6.4.2.2: The supplemental analysis presented here does not strengthen the hypothesis that the wetlands that were buried beneath the landfill acted as a significant source of dissolved carbon or dissolved arsenic contamination before the landfill was constructed (refer to MassDEP Comment 3 on the draft report). While the cited literature indicates that the geochemical conditions associated with wetlands and peat are generally reducing, the presence of peat is not sufficient to demonstrate a significant groundwater impact attributable to a wetland: the presence of a pre-existing flow regime that transported reducing groundwater from those wetlands to a significant portion of the underlying and downgradient aquifer is also necessary. The report does not include such a demonstration. Further, the cited literature concerning conditions in Bangladesh appears to be more representative of current site conditions than pre-landfill condition; the situation in Bangladesh involves peat that was buried, not peat in existing wetland, and therefore reveals little about the pre-landfill conditions at Devens. In summary, the pre-landfill impacts of the now-buried wetlands are not known and the potential impacts on the remedial alternatives are not known. In particular, the claim that landfill removal would only reduce carbon input by 25 to 50 percent is not reliable.

*Response:* The Army respectively disagrees with MassDEPs opinion. The fact that peat formed at the site mandates that reducing conditions exist (and existed at the site). Peat



*cannot form under oxidative conditions, which was the point of citing the textbook and research references. This is not a site-specific phenomena but a proven scientific fact. While it is impossible to prove through sampling or other investigative methods the methods of arsenic migration in the subsurface prior to the landfill placement, the existence of peat necessitates reducing conditions. The presence of reducing conditions coupled with the presence of arsenic in aquifer sands documented through this and other studies by the Army, USEPA and MassDEP indicates that arsenic mobilization must have occurred during these times. This transport mechanism and site model is exhaustively documented in scientific literature. Moreover the peat deposits were not at the original, pre-landfill, ground surface. Rather, as noted in the literature they were buried beneath the wetland and wetland sediments which again is a requirement for their formation.*

4. Section 8.2: The suggestion that wetlands located north of the site contribute to conditions that have mobilized and will continue to mobilize arsenic is inconsistent with data presented in the report. For example, arsenic concentrations in the shallow groundwater samples collected in and near the wetlands associated with Nonacoicus Brook did not exceed 10-ug/l (e.g., Figure 6 and 11). Similarly, arsenic concentrations in shallow groundwater samples recently collected from SHM-99-31A, located in or immediately downgradient of the wetland located between the north end of the landfill and Molumco Road, did not exceed 25 ug/l (refer to 2010 Annual Report).

*Response:* *This comment is similar to that posed by the EPA in the BCT meeting in that they observed strongly reducing conditions at Plow Shop Pond but found little arsenic in solution. The reason for this is as follows:*

- *Arsenic concentrations are considerably lower in the sands north of the landfill. As noted recently by the EPA and Gannet Fleming, arsenic enrichment of the sands occurs from weathering of arsenopyrite in bedrock in Shepley's Hill. This is the probable source of arsenic enrichment in the area and occurs primarily in the center of the landfill where the highest arsenic concentrations are found.*
  - *Sulfate reduction to sulfide also limits arsenic solubility at the site. Under strongly reducing conditions arsenic sulfides form which have been found in the form of framboidal pyrite (enriched in arsenic) throughout the site. Arsenic variability is to be expected due to the geologic origin of arsenic and the resulting solubility controls. The revised CSM addresses this issue.*
5. *In addition abundant literature, now noted in the revised SAR demonstrates that peat and wetlands will mobilize arsenic to varying but often high concentrations of arsenic (see revised SAR, Section 6). Figure 7: To avoid potential misunderstandings about the eastern extent of the contaminant plume near the north end of the landfill, the results from well SHM-10-06A should be replaced with the results from well SHM-10-06, or a footnote should be added to the figure for clarify the situation. Arsenic was reported with concentrations exceeding*

1,500-ug/l in the samples collected from well SHM-10-06, which was located less than 100-feet wet of well SHM-10-06A, where the maximum sample concentration was 94 ug/l.

Response: Comment noted. However no change to the figure is required. The section locations and nearby well concentrations are indicated in Figure 3.

**Email Message from Ginny Lombardo, USEPA dated 29 June 2011**

**Subject: MNA for North Impact Area and Draft Final SRI Report.**

I finally had the chance to follow-up with Bryan and others at EPA on the question of MNA as a remedial component for SHL. Although EPA recognizes that the geochemistry and uncertainties associated with the SHL system make it difficult to complete a full weight-of-evidence MNA assessment, EPA believes that the Army has presented adequate data and documentation in the SRI to select MNA, in conjunction with source control at the north end of the landfill, as components of the SHL remedy. As discussed, the source control remedy will not remedy the elevated As that has already come to be located in the NIA. As EPA has expressed in the past, we are willing to accept MNA as the remedy for the NIA and recognize that there will be uncertainties with attenuation rate and remedial timeframe. We are confident that EPA, DEP and Army can establish an LTM program that will provide for adequate monitoring of the NIA conditions over time to assess whether projections are being met over time. EPA agrees to accept the available data and data evaluation, as presented in the SRI, to select MNA (in conjunction with source control at the north end of the landfill) as part of the planned ROD Amendment. As has been raised several times, the most critical next step is establishing a revised LTM program. EPA requests that these LTM discussions begin as soon as possible so that consensus can be reached on appropriate well locations and protocols for selection of appropriate screen depths. EPA will not concur on a remedy that does not include MNA for addressing the contamination that has come to be located in the NIA (i.e., source control with just LTM will not be accepted).

In addition, I have completed review of the Draft Final SRI Report. I have the following comments:

1. In our GC 7, EPA expressed concern that column experiments were ongoing and questioned the availability of the data. Although the response to comment and Draft Final document includes additional column study results, Section 6.4.2.3 and 6.4.3, page 47, references other column studies that are still ongoing. Please clarify the objectives of these additional column studies and provide a schedule for submission of the results.

*Response:* Additional modelling data being provided as an attachment to the report.

2. In our GC 8, EPA raised a concern about capture on the northeastern side of the landfill and the data from SHM-10-06 and SHM-10-06A that Army used to support their position that the impacts are bounded between these 2 wells. We requested more data. The Army's response indicated that additional monitoring would be proposed in future monitoring plans. As discussed below, at the May 19, 2011 BCT meeting, Army/Sovereign referred to several planned additional sampling and investigation activities. EPA requests that re-sampling of these wells be incorporated into plans for re-sampling of SRI wells as soon as possible. Groundwater characteristics and capture in this area is critical to the evaluation of

the FFS. In addition, in the near future, the BCT will need to consider the issue of the timing of the installation of the slurry wall to address the discharge to Red Cove and how this will direct additional groundwater to the northeastern side of the landfill. It is critical to have a more thorough evaluation of the capture in this area, so we can adequately consider the fate of the additional groundwater that will be directed to this area once the slurry wall is installed.

Response: Such changes or enhancements to the current groundwater LTM network will be performed pending implementation of an updated remedy for SHL.

3. In response to SC 8, Army agreed to revise Figure 30. I did not see a revised Figure 30 in the Draft Final revisions submission.

Response: Corrected Figure will be provided.

4. In response to SC 16, Army agreed to provide an appendix with the PHREEQC2 and other modeling details. I did not see this in the Draft Final revisions submission.

Response: Additional modelling data will be provided as an attachment to the report.

5. In response to SC 22, Army agreed to revise Table 3. I did not see a revised Table 3 in the Draft Final revisions submission.

Response: The April 2011 Response to Comment mistakenly indicated that Table 3 and not Figure 2 would be revised. Figure 2 was reissued and provided to show all of the results collected for each of the analyzed wells. No changes were made or are proposed to Table 3.

Finally, at the May 19, 2011 BCT meeting, Army/Sovereign discussed the following planned efforts. EPA wants to ensure that we have an opportunity to review and comment on the plans for this work. Please update us on the status and schedule for these efforts:

6. During the discussion of characterization of the NIA, Sovereign stated that they planned to install a new transect (of boreholes or wells?) in the wetland area north of the P&T system. Sovereign also stated that they planned to get additional As solids data in the NIA.

Response: Such changes or enhancements to the current groundwater LTM network will be performed pending implementation of an updated remedy for SHL.



7. During the discussion on the model, Sovereign stated that the Corps was putting out a bid for gathering more model data and updating the model. The BCT discussed having a model meeting to discuss this further.

*Response: Additional groundwater modelling enhancements will be performed pending implementation of an updated remedy for SHL.*

8. During the discussion on DEP's concern regarding characterization of the eastern edge of the plume at Nonacoicus, Army stated that they planned to install a new transect near 10-08 to resolve this concern

*Response: Such changes or enhancements to the current groundwater LTM network will be performed pending implementation of an updated remedy for SHL.*

9. During the discussion on LTM, Army stated that they were having Sovereign look at what updates needed to be done and to address some short term needs.

*Response: Such changes or enhancements to the current groundwater LTM network will be performed pending implementation of an updated remedy for SHL.*

10. During the discussion on LTM, Sovereign stated that they planned to resample some of the SRI temporary wells this summer.

*Response: Such changes or enhancements to the current groundwater LTM network will be performed pending implementation of an updated remedy for SHL.*

**FINAL**



# **SHEPLEY'S HILL LANDFILL SUPPLEMENTAL GROUNDWATER AND LANDFILL CAP ASSESSMENT FOR LONG-TERM MONITORING AND MAINTENANCE – ADDENDUM REPORT**

**SHEPLEY'S HILL LANDFILL**

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**FORMER FORT DEVENS ARMY INSTALLATION, DEVENS, MA**

**AUGUST 2011**

**Prepared for:  
US Army Corp of Engineers  
New England District  
Concord, Massachusetts**

**Prepared by:  
Sovereign Consulting Inc.  
Contract No.: W912WJ-10-D-0003  
Delivery Order: 0002**



### **NOTICE**

The United States Department of Defense, Department of Army, funded wholly or in part the preparation of this document and work described herein under Contract No. W912WJ-10-D-0003 and Delivery Order 0002. Mention of trade names or commercial products does not constitute endorsement or recommendation for use.

**Shepley's Hill Landfill  
Supplemental Groundwater and Landfill Cap  
Assessment for Long-term Monitoring and Maintenance -  
Addendum Report**

**FINAL VERSION**

**Devens, Massachusetts**

**August 2011**

**CERTIFICATION:**

I hereby certify that the enclosed Report, shown and marked in this submittal, is that proposed to be incorporated with Contract Number W912WJ-10-D-0003 DO#0002. This Document was prepared in accordance with USACE Scope of Work and is hereby submitted for Government Approval.

**Reviewed By:**

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**Sovereign Project Manager**

**Date**

---

**Sovereign Quality Control Manager**

**Date**

**Received By:**

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**USACE Project Manager**

**Date**



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## ATTACHMENTS

Attachment A	Soil Boring Logs/Well Construction Logs
Attachment B	Geophysical Applications Report
Attachment C	Groundwater Sampling Logs
Attachment D	Soil Laboratory Reports (Disk)
Attachment E	Groundwater Monitoring Well Laboratory Reports (Disk)
Attachment F	Groundwater Profiling Laboratory Reports (Disk)
Attachment G	Landfill Gas Evaluation Memo
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## ABBREVIATIONS, ACRONYMS, AND SYMBOLS

ADR	Automatic Data Review
AMEC	AMEC Earth and Environmental, Inc.
AOC	Area of Concern
AR	Annual Report
ATP	Arsenic Treatment Plant
AW	Additional Work
BCT	BRAC Cleanup Team
bgs	below ground surface
BRAC	Base Realignment and Closure
CERCLA	Comprehensive Environmental Response, Compensation, and Liability Act
COD	Chemical Oxygen Demand
CSM	Conceptual Site Model
cys	cubic yards
DIC	Dissolved Inorganic Carbon
DO	Dissolved Oxygen
DOC	Dissolved Organic Carbon
DPT	Direct Push Technology
DQO	Data Quality Objective
ECC	Environmental Chemical Corporation
FFS	Focused Feasibility Study
FS	Feasibility Study
FSSR	Feasibility Study Screening Report
GPS	Global Positioning System
IDL	Instrument Detection Limit
HERA	Human and Ecological Risk Assessment
IC	Institutional Control
LTM	Long Term Monitoring
MA	Massachusetts
MassDEP	Massachusetts Department of Environmental Protection
MCL	Maximum Contaminant Level
MNA	Monitored Natural Attenuation
MNR	Monitored Natural Recovery
MSL	Mean Sea Level
ND	None Detectable
NIA	North Impact Area
ORP	Oxidation-Reduction Potential
pH	Standard potential of Hydrogen ion concentration
ppb	parts per billion
ppm	parts per million
PVC	polyvinyl chloride
RI	Remedial Investigation
ROD	Record of Decision
REDOX	Reduction and Oxidation

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RSE	Remediation System Evaluation
RTC	Response to Comments
SAP	Sampling and Analysis Plan
SAR	Supplemental Assessment Report (AMEC 2009)
SC	Specific Conductance
SHL	Shepley's Hill Landfill
SOW	Scope of Work
Sovereign	Sovereign Consulting Inc.
TAL	Target Analyte List
TDS	Total Dissolved Solids
Temp	Temperature
TOC	Total Organic Carbon
TSS	Total Suspended Solids
UFP-QAPP	Unified Federal Policy - Quality Assurance Project Plan
USACE-NAE	U.S. Army Corps of Engineers - New England District
USEPA	U.S. Environmental Protection Agency
USGS	U.S. Geological Survey
Workplan	SHL Supplemental Investigation Workplan Addendum data May 2010

## EXECUTIVE SUMMARY

The Shepley's Hill Landfill encompasses approximately 84 acres in the northeast corner of the main post of the former Fort Devens. The landfill was reportedly operating by the early 1940s, and evidence from test pits within the landfill suggests earlier usage, possibly as early as the mid-nineteenth century. The landfill contains a variety of waste materials, including incinerator ash, demolition debris, asbestos, sanitary wastes, spent shell casings, glass, and other wastes. As described previously (Harding ESE 2002), the maximum depth of the refuse occurs in the central portion of the landfill and is estimated to be about 40 feet bgs. The volume of waste in the landfill has been estimated at over 1,500,000 cys, of which approximately 160,000 cys (11%) is below the water table. The landfill was closed in five phases between 1987 and 1992-93

Since landfill closure, numerous studies have been conducted to evaluate contaminant conditions at the landfill. Data gaps identified by these investigations are outlined within Table 1. Because of the complex nature of the site conditions, the following areas were identified for further evaluation as documented in this addendum report:

- Delineation & Monitoring for North Impacted Area - Determine if arsenic impact in groundwater extends beyond the installed locations (SHM-10-01 through SHM-10-04, SHM-10-05A, and SHM-10-08 through SHM-10-10).
- North Impact Capture - Determine if the existing treatment system is capturing the arsenic, and that natural attenuation is an effective alternative;
- Landfill Gas Impact - Determine if methane intrusion into surrounding buildings is a concern or issue;
- East Impact Delineation and Capture - Obtain additional information on the migration of arsenic towards Plow Shop Pond; and
- Arsenic Source Strength - Obtain information to evaluate the strength and duration of the dissolved arsenic conditions. This assessment will be conducted by evaluating arsenic stability, redox boundary, the impact of the existing treatment system, and evaluate the arsenic impact via a fate and transport evaluation.

To facilitate this investigation, the following scope of work was implemented:

- Advancement of 21 borings using DPT and 7 borings using Rotasonic drilling methodologies. Temporary groundwater monitoring wells were constructed within 16 of 29 boreholes. During drilling operations, groundwater profile samples were collected at 10-foot sampling increments for field screening with an arsenic test kit and laboratory analysis. All groundwater samples were collected in accordance with the January 2010 USEPA Region I Low-Stress / Low-Flow groundwater sampling guidance document. During sampling collection, the purge water was monitored using a properly calibrated YSI meter and screened for DO, pH, Temp, Specific Conductivity, ORP, and color;

- Completion of a geophysical survey to identify bedrock surface elevations within the North Delineation and Monitoring Area along three transect lines;
- Analysis of designated soil, groundwater, and groundwater profiling samples for metals (aluminum, antimony, arsenic, barium, beryllium, cadmium, calcium, chromium, cobalt, copper, iron, lead, magnesium, manganese, mercury, nickel, potassium, selenium, silver, sodium, thallium, vanadium, and/or zinc), hardness, alkalinity, TSS, ammonia, nitrite, nitrate, COD, chloride, DIC, DOC, TOC, sulfide, and/or sulfate;
- Completion of an evaluation to determine whether dissolved methane gas in groundwater from the landfill presents a potentially unacceptable hazard to nearby structures;
- Completion of treatability bench testing on water samples obtained from monitoring wells SHM-10-14 and SHM-10-15;
- Running of column studies on soil and waste samples obtained at the site in order to evaluate arsenic source strength and reducing conditions at the landfill.

The findings of this investigation as summarized as follows:

- Delineation & Monitoring for North Impacted Area – The investigation included the advancement of soil borings, completion of groundwater vertical profiling, and construction and sampling of monitoring wells on the northern and southern side of Nonacoicus Brook. These boring and well locations are identified as SHM-10-01, SHM-10-02, SHM-10-03, SHM-10-04, SHM-10-05 (no well installed), SHM-10-05A, SHM-10-08, SHM-10-09 (no well installed), and SHM-10-10. Groundwater profiling conducted during the drilling program recorded dissolved arsenic concentrations varying from non-detect to 112-ug/l. Sampling and analysis of groundwater samples obtained from the monitoring wells reported concentrations of dissolved arsenic varying between 0.43 and 7.87-ug/l. Lastly, the geophysical survey indicated that bedrock slopes upward, thereby restricting the migration of the release. The results of this data define the down-gradient extent of the arsenic impact below the southern bank of Nonacoicus Brook. Groundwater flow from the north and northeast of the Brook flows and mixes with groundwater advancing north and northwest from the landfill area creates an oxidation/reduction front that effectively limits the northern extent of the arsenic at the mixing front.
- North Impacted Capture – Points SHM-10-06 and SHM-10-06A were installed to evaluate the capture and confinement of the arsenic plume on the north and northeastern side of the existing arsenic treatment plant. Groundwater profiling indicated evidence of dissolved arsenic ranging from 10 to 2,540-ug/l in well SHM-10-06, while decreased concentrations were detected in SHM-10-06A at concentrations of non-detect to 106-ug/l. Sampling and analysis of groundwater from the monitoring wells document concentrations decreasing between the two wells from 2,710 to 60.1-ug/l. This data was included in refined particle tracking modeling that indicates that the treatment system is reducing arsenic mass and capturing the bulk of arsenic mass on the northern and



northeastern side of the treatment plant and that the impacts are bounded between monitoring points SHM-10-06 and SHM-10-06A. Drilling operations indicated a shallower than previously extrapolated bedrock surface in this area. The shallower rock elevations were plotted and included in the refined particle track models that document a bedrock trough trending northward through the landfill and that the shallower rock ridge along the east side of the landfill appears to restrict arsenic migration in a northerly direction. These observations will be refined through long term monitoring.

- Landfill Gas Assessment - Modeling was conducted to determine if methane gas intrusion into an occupied building or structure was a concern. The results of this modeling using a dissolved methane concentration of 10-mg/l in the groundwater determined that this concentration would not pose an explosive hazard.
- East Plume Delineation and Capture - For this part of the investigation, a temporary monitoring well was advanced at the location identified as SHM-10-07. Groundwater profiling recorded dissolved arsenic concentrations varied between 58 and 1,350-ug/l, while groundwater sampling of this monitoring well confirmed dissolved arsenic concentrations of 818 and 918-ug/l. Drilling operations indicated a shallower than previously extrapolated bedrock surface in this area. The shallower rock elevations were plotted and included in the refined particle track model that document a bedrock trough trending northward through the landfill and that the shallower rock ridge along the east side of the landfill appears to restrict arsenic migration to a northerly direction.
- Arsenic Natural Attenuation/Source Strength and Reducing Environmental Evaluation - An evaluation of the collected information determined the following;
  - Presently the primary source of arsenic in groundwater appears to be aquifer sands rich in amorphous iron hydroxide solids, usually coated on sand grains as documented through microscopy. Other sources of arsenic include landfill waste, peat, and bedrock/till. The contribution of landfill waste has been reduced due to depletion of easily degradable carbon and recent capping of the landfill. While peat in some instances was found to contain arsenic, it is not clear if the peat contained the arsenic originally or whether arsenic accumulated in the peat by leaching of arsenic from overlying waste. Arsenic solubility is controlled by desorption from the iron solids and by reductive dissolution of the iron (III) solids created by biodegradation of peat and waste. A site specific distribution coefficient (Kd) was derived from the aquifer solids content and aqueous arsenic in contact with the solids, as 7.6. The distribution is useful for predicting ranges of arsenic concentrations that could be expected in local groundwater. This process does not however include dissolution of the iron solid, a process that could lead to higher arsenic concentrations.

- Arsenic groundwater distribution has been improved via a number of transects and depth profiles. The distribution of arsenic can be considered as (1) increasing with depth to just above the glacial till layer, (2) highest in the center of the landfill near SHM-10-14 and SHM-10-15, (3) slowly decreasing in concentration to the north of the landfill to the south side of the Nonacoicus Brook and wetlands, and (4) controlled in large degree by the bedrock surface as far as flow direction is concerned.
- A redox boundary appears to be located in the vicinity of SHM-10-10. The boundary consists of three features: (1) a bedrock surface that controls the flow of landfill impacted water to the Brook but also brings groundwater from the north and northeast of the Brook that mixes or dilutes the landfill flow from the south, (2) intrusion of non-impacted, more oxidized groundwater from the north side of the landfill, and (3) mixing of non-impacted with landfill water resulting in precipitation of arsenic that should not impact the water quality in the Brook or wetlands.
- Carbon inputs to the groundwater from biodegradation of waste or peat indicates that peat is probably a more important carbon source for maintaining reducing conditions than landfill waste at this time. The reducing conditions created by the peat preceded the landfill, but were exacerbated by the additional carbon source from the landfill waste. Peat formation is a result of reducing conditions, but also maintains reducing conditions by biodegradation and release of short chain carboxylic acids and methylated amines that will drive iron oxy hydroxide reduction and ammonia production (Bergmann et al, 1999) both byproducts that are widespread at the site.
- The time it takes to flush groundwater arsenic from beneath the landfill has been simulated from two column experiments. The studies suggest that soluble arsenic is removed (concentration less than laboratory detection methods) within 13 to 14 pore volumes of clean water. However, reducing conditions and soluble carbon still remain indicating reserve (non-soluble) arsenic that may be resolubilized. The time frame describing removal of soluble arsenic from the landfill aquifer and north impacted area is approximately 270 years based on this data assuming a flow velocity of 0.5 ft/day and the site travel distance.

The conceptual site model advanced for Shepley's Hill Landfill by others has been updated to include the following new information.

- Waste within the landfill has been further characterized with the recent installation of 5 borings drilled through the landfill to bedrock. Waste analysis revealed that with the exception of lead, zinc and copper most trace elements were at typical background levels. Arsenic in the waste or peat did not exceed 60 mg/kg. Initial leaching tests indicate that landfill waste potentially could deliver up to 500 ug/L arsenic to underlying groundwater. This leaching test is a sequential extraction test that estimates the entire pool of available arsenic, not the amount in equilibrium with the waste. Placement of the cap has likely eliminated leaching of arsenic and any other constituents from landfill

waste to underlying groundwater, although recent estimates suggest that only 11% of the landfill waste is in contact with groundwater or saturated.

- In comparison to the waste, underlying sands potentially leach up to 1,500 ug/L arsenic to groundwater. For example, if all of the arsenic entrained in the iron solids on the sand grains was release, then concentrations of 30,000 ug/L or higher of arsenic could be found in solution. Based on these results, underlying aquifer sands are the dominant source of arsenic at the landfill.
- The borings through the landfill revealed that thick peat layers are found underlying waste in the center of the landfill roughly bounded by SHL-99-29x, SHM-10-13, SHM-10-14, and SHM-10-15.
- The peat and the associated wetlands preceded the landfill based on historical mapping of the area. The peat is a significant source of carbon to the groundwater and caused locally reducing conditions prior to emplacement of waste. Therefore arsenic mobilization has been occurring historically prior to landfill development and will continue to occur as long as carbon degradation within the peat takes place.
- The north impacted area (NIA) also appears to have reducing conditions partially from the landfill influence and in part from naturally occurring wetlands occurring in the NIA.
- Arsenic in groundwater in the north impacted area appears to diminish substantially prior to discharge beneath the Brook and wetlands due to a partially observable and mapped redox boundary. The redox boundary occurs due to mixing or dilution with groundwater flow from the north side of the brook. Chemistry of water in DPT points close to the Brook show mixing with water from the north side indicating that the Brook is a discharge divide. Arsenic is not expected to impact the Brook and wetlands due to this redox boundary.
- Groundwater discharge at the north end appears to follow the particle track data presented by and refined by AMEC based on these investigations described herein. Arsenic impact to the MacPherson well is not anticipated based on the results of the investigation at the redox boundary.
- Newly acquired bedrock information indicated that bedrock is located at a shallower depth than originally projected within the area near Nonacoicus Brook. This information was incorporated within the hydrogeologic study and the particle track updated. The results indicated an increase in the groundwater flow velocity near the Brook, but continued to show that the system collected the arsenic impacted groundwater.
- An evaluation of methane determined that the dissolved concentration within groundwater does not present an explosive hazard.

- It is likely that reducing conditions prevalent in the landfill and peat have mobilized arsenic from the aquifer sands which is now entering the Cove via a different flow path than the predominant south-north flow pattern observed for most of the landfill. Similar to the arsenic flux north of the site, the impact to Red Cove likely preceded the placement of the landfill. The landfill and the corresponding additional dissolved carbon associated with the reducing conditions certainly would have exacerbated the flux prior to capping.

The results of the column and batch studies are complete and included:

- A column study to determine the time (estimated from pore volumes) for clean, oxidized water to restore the column to background conditions under conditions of moderate arsenic in pore water,
- A column study to determine the time for arsenic free, but reduced water to restore the column to background conditions under moderate arsenic pore water concentrations,
- A batch study to determine the rate at which organic carbon is degraded under anaerobic condition, and
- A column study to determine the rate of release of arsenic from aquifer sands under reducing conditions typical of the landfill environment.



## 1.0 INTRODUCTION

Information contained within this report is associated with the scope of work outlined under two separate contract proposals including:

- 15 April 2010 Supplemental Investigation Contract Proposal; and,
- 22 July 2010 Modification Proposal.

These work scopes were conducted to address data gaps outlined in the Shepley's Hill Landfill Supplemental Investigation Workplan Addendum dated May 2010, the Shepley's Hill Landfill Supplemental Investigation Workplan Addendum for Evaluation of the North Plume Monitored Natural Attenuation for the Impacted Area and Source Strength/Landfill Reducing Environmental Evaluation dated July 2010, and the Supplemental Groundwater and Landfill Cap Assessment for Long-term Monitoring and Maintenance dated June 2009. The location of the site is shown on **Figure 1**.

### 1.1 Purpose and Scope of Investigation

The purpose of this study is to address the following:

1. Delineation and Monitoring of the North Impacted Area - To delineate the north impacted area in all directions to depth in order to establish final delineated impact boundaries. Install additional monitoring wells to monitor arsenic impact migration and ensure that the arsenic impacts do not migrate further beyond the final delineated plume boundaries. The location of these monitoring points was outlined within the May 2010 Workplan Addendum;
2. North Impact Capture - To evaluate whether the existing treatment system is capturing arsenic, and evaluate and/or demonstrate that natural attenuation will be effective at remediating the North Impact Area within a timeframe that is reasonable given the groundwater chemistry of the site;
3. Landfill Gas Assessment - To evaluate potential landfill gas impacts in the area of the North Impacted Area in accordance with the EPA Guidance for Evaluating Landfill Gas Emissions from Closed or Abandoned Facilities to ensure that methane emanating from the landfill will not cause unacceptable risks in nearby structures;
4. East Impact Delineation and Capture - Install a groundwater monitoring well to evaluate arsenic groundwater impact to Plow Shop Pond sediments;
5. Arsenic Source Strength - To estimate the arsenic source strength and duration, including the quantity of arsenic that may be mobilized and the strength and duration of the source of the reducing conditions.



6. Source Strength / Landfill Reducing Environmental Evaluation – To estimate the duration of the landfill's ability to maintain reducing/methanogenic conditions.

The technical objective and approach of the data collection program is summarized in **Table 1** of this report. To achieve these objectives, the following scope of services was conducted:

1. Advancement of 11 borings using DPT and 7 borings using Rotasonic drilling methodologies. The DPT locations are identified as SHM-10-01 through SHM-10-06, SHM-10-05A, SHM-10-06A, and SHM-10-08 through SHM-10-10. The Rotasonic locations are identified as SHM-10-07, and SHM-10-11 through SHM-10-16. Each of the boring locations are illustrated on **Figure 2**, with copies of the boring logs provided as **Attachment A**;
2. Advancement of an additional 10 DPT points to evaluate reduction and oxidation (REDOX) conditions both horizontally and vertically along the boundaries of the Nonacoicus Brook. Representative soil samples were not obtained during the completion of this phase of the evaluation program, rather a detailed investigation was conducted of the water chemistry between the groundwater and surface water interface. The location of these points are shown on **Figure 3**, and labeled as SHM-10-17 through SHM-10-27;
3. Completion of a geophysical survey to identify bedrock surface elevations within the Northern Delineation and Monitoring Area along three transect lines. These transect lines are identified as A-A', B-B', and C-C' on **Figure 4**. A copy of the Seismic Refraction Survey Report prepared by Geophysical Applications, Inc. is included as **Attachment B** of this document;
4. Analysis of groundwater samples obtained during groundwater profiling for concentrations of total and/or dissolved metals (aluminum, antimony, arsenic, barium, beryllium, cadmium, calcium, chromium, cobalt, copper, iron, lead, magnesium, manganese, mercury, nickel, potassium, selenium, silver, sodium, thallium, vanadium, and/or zinc) and screened using an Arsenic Field Testing Kit. The samples were also analyzed for hardness, alkalinity, TSS, ammonia, nitrite, nitrate, COD, chloride, DIC, DOC, sulfide, and sulfate. During sampling, purged water was field screened for DO, pH, Temp, Specific Conductivity, ORP, and color. A tabulated summary of the groundwater profiling results is provided in **Table 2**;
5. Construction of temporary groundwater monitoring wells within 16 of the 29 completed boreholes. The well screening depth was based on the arsenic groundwater profiling and laboratory results. No temporary monitoring well was constructed within the point identified as SHM-10-09, since concentrations of arsenic were not present within the profile samples. However, an additional well, SHM-10-06A, was installed to better define the arsenic plume in the north capture zone area. In addition, monitoring wells were not installed within the points identified as SHM-10-17 through SHM-10-27 since they were being used for profiling of the redox conditions along the Nonacoicus Brook only;

6. Analysis of groundwater samples obtained from the temporary monitoring wells for total and/or dissolved metal (aluminum, antimony, arsenic, barium, beryllium, cadmium, calcium, chromium, cobalt, copper, iron, lead, magnesium, manganese, mercury, nickel, potassium, selenium, silver, sodium, thallium, vanadium, and/or zinc), hardness, alkalinity, TDS, TSS, ammonia, nitrite, nitrate, COD, TOC, chloride, sulfide, and sulfate. During sampling collection, water was field screened for DO, pH, Temp, Specific Conductivity, ORP, and color. A tabulated summary of the groundwater results is provided in **Table 3**;
7. Analysis of soil samples from the landfill borings (SHM-10-07, and SHM-10-11 through SHM-10-16) for concentrations of TAL Metals (aluminum, antimony, arsenic, barium, beryllium, cadmium, calcium, chromium, cobalt, copper, iron, lead, magnesium, manganese, mercury, nickel, potassium, selenium, silver, sodium, thallium, vanadium, and/or zinc) and TOC. A tabulated summary of the soil results is provided in **Table 4**.
8. Completion of a treatability bench testing on water samples obtained from monitoring wells SHM-10-14 and SHM-10-15. Water collected from the site was run through a column containing iron with the effluent water analyzed for residual arsenic concentrations. Further information on this study is provided in **Section 6.2.3.2** of this report.
9. Running of column study on samples obtained at the site. These column studies were conducted to evaluate Arsenic Source Strength and Reducing conditions.

## **1.2 Goals of Investigation**

The goals of this investigation are to address the summarized data gaps noted on **Table 1** of this report. These goals include:

1. Delineation and Monitoring of the North Impacted Area – Confirm that arsenic does not extend beyond the installed locations;
2. North Impact Capture – Confirm that the existing treatment system is capturing arsenic, and that natural attenuation is an effective alternative;
3. Landfill Gas Assessment – Confirm that methane intrusion into surrounding buildings is not a concern or issue;
4. East Impact Delineation and Capture – Obtain additional information on the migration of arsenic towards Plow Shop Pond;
5. Arsenic Source Strength – Obtain information to evaluate the strength and duration of the dissolved arsenic conditions. This assessment will be conducted by evaluating the plume stability, redox boundary, the impact of the existing treatment system, and evaluate the arsenic plume via a fate and transport evaluation.

## 2.0 SITE HISTORY AND BACKGROUND

Shepley's Hill Landfill encompasses approximately 84 acres in the northeast corner of the main post of the former Fort Devens. The landfill is bordered to the northeast by Plow Shop Pond, to the west by Shepley's Hill, to the south by recent commercial development, and to the east by land formerly containing a railroad roundhouse. Nonacoicus Brook, which drains the pond, lies to the north of the landfill. The landfill includes three Areas of Contamination (AOCs) investigated under CERCLA: AOC 4, the sanitary landfill incinerator; AOC 5, sanitary landfill No. 1; and AOC 18, the asbestos cell. The landfill was reportedly operating by the early 1940s, and evidence from test pits within the landfill suggests earlier usage, possibly as early as the mid-nineteenth century. The landfill contains a variety of waste materials, including incinerator ash, demolition debris, asbestos, sanitary wastes, spent shell casings, glass, and other wastes. As described previously (Harding ESE, 2002), the maximum depth of the refuse occurs in the central portion of the landfill and is estimated to be about 40 feet below ground surface (bgs). The volume of waste in the landfill has been estimated at over  $1.5 \times 10^6$  cys, of which approximately  $1.6 \times 10^5$  cys (11%) is below the water table. The saturated wastes may be emplaced in a wetland reducing environment; at least two areas previously mapped as wetlands appear to have been filled (Harding ESE, 2002).

Subsequent to closure of the landfill (1987-1993), remedial investigations (RIs) completed under CERCLA evaluated soil, sediment, surface water, and groundwater conditions at and in the immediate vicinity of the landfill. The results confirmed the presence of various contaminants, particularly certain inorganics and volatile organic compounds (VOCs), in groundwater, sediments, and surface water at or adjacent to Shepley's Hill Landfill. A Feasibility Study (FS) and Record of Decision (ROD) resulted in a remedy that required long term monitoring and maintenance of the existing landfill cap and groundwater monitoring. The ROD (USEPA, 1995) included a contingency provision, which required that a groundwater extraction system be installed if groundwater contaminant concentrations, primarily arsenic, did not meet risk-based performance standards over time. Due to continued elevated contaminant concentrations, the Army installed and started full time operation of a groundwater extraction and treatment system in March 2006 to address groundwater contamination emanating from the northern portion of the landfill.

### 2.1 Regulatory Context

Fort Devens was placed on the National Priorities List (NPL) in November 1989 due to contamination of groundwater with arsenic (As), cadmium (Cd), chromium (Cr), lead (Pb), and mercury (Hg). The EPA and Army signed a Federal Facilities Agreement (FFA) on May 13, 1991 (amended March 26, 1996). The ROD outlined the remediation objectives for the Shepley Hill Landfill (USEPA, 1995). It requires the Army to monitor groundwater, maintain the landfill, and prepare annual reports. It also requires that the Army review the effectiveness of the remedy every five years. The goal of that remedy, which relied heavily on the previously installed landfill cap, was to attain groundwater clean-up goals by 2008 thereby reducing exposure risks. In addition, the ROD states that if the landfill cap was found not to meet the prescribed risk reduction performance criteria, the Army was to use a contingency remedy that consisted of groundwater extraction and treatment. That remedy has been constructed and



began operation in September 2005, and has operated full time since March 2006. The table below summarizes remediation target levels for Shepley's Hill Landfill Operable Unit groundwater, as defined in the ROD.

Chemical of Concern	Remediation Target Level (ug/l)	Selection Basis
Arsenic	10*	MCL
Chromium	100	MCL
1,2-Dichlorobenzene	600	MCL
1,4-Dichlorobenzene	5	MMCL
1,2-Dichloroethane	5	MCL
Lead	15	Treatment Technology Action Level
Manganese	291	Background**
Nickel	100	MCL
Sodium	20,000	Health Advisory
Aluminum	6,870	Background**
Iron	9,100	Background**

ug/l – micrograms per liter, approximately equivalent to parts per billion (ppb)

MCL – Maximum Contaminant Level; MMCL – Massachusetts MCL

\*Note – The MCL for arsenic prior to January 23, 2006 was 50-ug/l. The EDS (CH2M Hill 2005) indicated “It is expected that they (ROD cleanup goals) will change to be responsive to this new (10-ug/l) Standard.”

\*\* The estimation of background concentration is presented in Section 4 of the RI Addendum Report (ABB-ES, 1993).

The ROD grouped monitoring wells at Shepley's Hill Landfill into two groups. Well Group 1 consists of wells, primarily at the north end of the landfill, where cleanup levels have been attained historically. Well Group 2 consists of wells where historically cleanup levels have not been attained. However, as discussed further in the next section, the Group 1 and 2 well designations were determined to no longer be relevant for the combined capped landfill and Contingency Remedy in 2007.

## 2.2 Remedial Actions to Date

The landfill was closed in five phases between 1987 and 1992-93 in accordance with Massachusetts regulations set forth in 310 CMR 19.000. The Massachusetts Department of Environmental Protection (MassDEP) approved the closure plan in 1985. Closure consisted of installing a 30-mil polyvinyl chloride (PVC) membrane cap, covered with soil and vegetation and incorporating gas vents. Closure also included installation of monitoring wells to evaluate groundwater quality around the landfill and construction of drainage swales to control surface water runoff. MassDEP issued a Landfill Capping Compliance Letter approving the closure in February 1996.

The Army maintains and monitors the landfill. Activities include:

- mowing the vegetation;
- monitoring emissions from gas vents;
- monitoring vapor levels in soil gas probes;
- operating a pump and treat system; and
- monitoring of groundwater.

### 3.0 FIELD INVESTIGATION

The following services were conducted to evaluate conditions associated with the North Impact Area Delineation, North Plume Capture, East Plume, and to provide information of the Arsenic Source Strength and Reducing Conditions.

#### 3.1 Access Arrangements and Conservation Commission

Upon finalizing the proposed exploration locations with the USACE and input from stakeholders, Sovereign personnel obtained contact information of each of the property owners. The prepared letters were submitted to the USACE who assigned a representative to obtain approval from each owner prior to accessing each property. Work was not completed at a proposed exploration point until approval was received from the property owner.

Sovereign then performed a wetland delineation that included routine assessments of vegetation, hydrology, and soil conditions along previously defined geophysical survey transects (A-A', B-B', and C-C') in the area north of Nonacoicus Brook proposed monitoring well locations, and proposed access points to work areas (Figure 4). Sovereign also completed a riverfront (Nonacoicus Brook) delineation which included field identification and flagging of the 'top of bank' for riverfront areas, where applicable, to locate the inner and outer riverfront areas/riparian corridors. Wetland delineation procedures followed the "routine method" outlined in the Corps 1987 Wetlands Delineation Manual, as modified by U.S. Army Corps of Engineers Interim Regional Supplement to the Corps of Engineers Wetland Delineation Manual: North-central and Northeast Region (2009). As discussed in the North-central and Northeast Regional Supplement, Ayer, Massachusetts is located in the Land Resource Region – R, Northeastern Forests. The standards and regulations established in the Massachusetts Wetlands Protection Act Regulations (310 CMR 10.00) were reviewed prior to the site delineation. The methodologies described within the Massachusetts Wetland Protection Act differ slightly from the USACE methodology. As such, the procedure for wetland delineation described in the Massachusetts document Delineating Bordering Vegetated Wetlands also was utilized during the May 2010 field investigation. Both the USACE and Massachusetts method delineations established the same wetland line (i.e. the USACE and Massachusetts lines did not diverge); therefore, it was not necessary to flag/delineate two separate wetland lines. The results of this evaluation were issued in a report titled "Wetland Delineation Report" dated 13 May 2010. An updated boring location plan was provided to the Ayer Conservation Commission to detail the location of additional exploration points which were proposed as a result of a modification to the original scope of work. This 30 July 2010 letter report and plan were provided to the Conservation Commission on 5 August 2010.



### 3.2 Geophysical Survey

Bedrock can have a strong influence on groundwater flow patterns and in aquifers with contaminants at depth in the saturated overburden, the flow changes that occur near depth to the bedrock surface can influence the direction of contaminant migration. Further, variations in bedrock topography (i.e. the presence of troughs and ridges that expand or contract over a distance), can affect the localized groundwater flow velocity in the overlying overburden aquifer as a unit of saturated aquifer migrates across and through those topographical changes. Therefore, a geophysical survey to map the bedrock surface within the North Impact Area Delineation area was conducted to document depth to bedrock within this area and determine if additional information could be gathered pertaining to the mechanisms controlling groundwater flow patterns. The principal objective of the geophysical survey was to determine the depth to and the elevation of the bedrock surface in the vicinity of Nonacoicus Brook, downgradient of the landfill. Available information suggests the presence of a bedrock trough beneath the northern toe of the landfill and Nonacoicus Brook. The trough is oriented north to south beneath the landfill toe, and gradually turns west until generally aligned east to west beneath Nonacoicus Brook. The geophysical survey included seismic refraction imaging along lines designated A-A', B-B', and C-C' as depicted on Figure 4.

As part of this investigation, the May 2010 Workplan Addendum outlined the placement of three transect lines to be located and used to conduct a seismic refraction geophysical bedrock elevation survey (Lines A-A', B-B', and C-C'). To conduct this assessment, the GPS coordinates of SHM-10-02, SHM-10-03, SHM-10-04, SHM-10-08, and points near the end of each transect line were determined, and the point located and marked in the field with wooden stakes. Each of the transect lines was surveyed, with grubbing operations conducted for survey line-of-sight and to implement the geophysical survey. In several locations, the transect lines and exploration point were offset or adjusted because of adverse conditions (wet soils or standing water).

The geophysical survey along each traverse was conducted in 250-foot long segments, with geophones placed at 10-foot increments. A Betsy Gun or 450-pound accelerated weight-drop device was used as the energy source. A copy of the Seismic Refraction Survey Report prepared by Geophysical Applications, Inc. is included as **Attachment B** of this document. The results of the survey indicate that bedrock undulates between elevations 145-feet to 167-feet along transaction A-A', 113-feet to 180-feet along transaction B-B', and 142-feet to 176-feet along transaction C-C'.

### 3.3 Subsurface Exploration

The drilling services outlined under this section of the report were conducted in two separate phases. These services were conducted to evaluate conditions within the North Impact Area Delineation, North Capture, and the East Plume Delineation Areas. The drilling procedures used for each of these two areas are outlined in the following subsections. All drilling and sampling management was conducted as required by the site specific documents which include the HASP, DAP, FSP, and QAPP.

The borings completed under this investigation are shown on **Figure 2** and **Figure 3**. The locations of the proposed exploration points were used to evaluate the following:

1. SHM-10-01 is located to evaluate the western limit of the plume in the area of West Main Street;
2. SHM-10-02 and -03 are located to evaluate the western limit of the plume in the area of Nonacoicus Brook and the bedrock valley;
3. SHM-10-04 is located to evaluate the northern limit of the plume in the area of Nonacoicus Brook;
4. SHM-10-05A (and 05) is located to evaluate the eastern limit of the plume in the area of West Main Street;
5. SHM-10-06 and SHM-10-06A were used to evaluate contaminant capture of the treatment system;
6. SHM-10-07 was used to evaluate the limits of the plume in the area of Red Cove;
7. SHM-10-08 through -10 were used to evaluate the limit of the plume in the area of Nonacoicus Brook;
8. SHM-10-11 through -15 were used to evaluate contaminant conditions and characterize groundwater chemistry within the landfill;
9. SHM-10-16 was used to evaluate contaminant conditions downgradient of the landfill;
10. SHM-10-17 through SHM-10-27 were used to evaluate Redox conditions along the southern side of Nonacoicus Brook.

Copies of the test boring logs/monitoring well construction reports are attached as **Attachment A**. No logs were prepared for the points identified as SHM-10-17 through SHM-10-27 since these points were used to evaluate groundwater Redox conditions, and soil samples were not collected as part of the drilling procedures.

### 3.3.1 Direct Push Technology (DPT)

A DPT drilling method was used to advance the proposed exploration points located within the North Impact Area Delineation and the North Plume Capture Areas. During this phase of the investigation the DPT investigation was conducted in two separate mobilizations. The initial phase involved advancing DPT groundwater sampling rods continuously, with vertical groundwater sampling conducted at 10 feet intervals to assess groundwater chemistry and arsenic concentrations within the overburden aquifer as discussed in **Section 3.6.3.2** of this report. The second phase of the DPT investigation included continuous soil sampling to evaluate the subsurface soil geology (no soil samples were saved or analyzed), and to allow for the construction of temporary 1.5" Poly Vinyl Chloride (PVC) monitoring wells within select locations. In general, soil conditions consisted of fine to coarse grained sand deposits overlying a varying layer of glacial till within each location, with each location terminated at a refusal conditions (bedrock or presumed bedrock). The exploration points conducted using this drilling method include SHM-10-01 through SHM-10-06, SHM-10-05A, SHM-10-06, and SHM-10-08 through SHM-10-10. These points were used to characterize groundwater chemistry at downgradient points from the landfill.

### 3.3.2 Rotosonic Drilling Method

Rotosonic drilling methods were used to conduct drilling operations at the exploration points identified as SHM-10-07, and SHM-10-11 through SHM-10-16 within the East Plume Area and Landfill. Continuous soil samples were collected at each location, with select samples obtained during the drilling operations submitted for laboratory analysis or used for the column study analysis. Groundwater profiling was also conducted during the drilling program, with samples obtained at 10-foot sampling increments upon reaching the groundwater table and extending vertically to the bedrock interface. A five to ten foot sample of the underlying bedrock was obtained at each of the completed borings. To complete each location, a 2-inch diameter temporary monitoring well was constructed within the completed borehole. Further information on the sampling analyses is provided in Section 3.6 of the report. Point SHM-10-07 was used to evaluate groundwater chemistry near Red Cove, while the other points were used to evaluate landfill MNA and SS conditions. In general, soil conditions consisted of sand with varying percentages of silt, gravel, and rock fragments, with areas of waste materials and peat. Refusal conditions were encountered, presumably at bedrock or presumed bedrock, at each of the completed boreholes, with glacial till encountered above the refusal conditions in several locations. Prior to drilling the locations situated within the landfill, the overlying soils were excavated to expose the landfill liner, the liner was cut and air monitoring conducted in accordance with the SOP attached to the FSP.

### 3.3.3 Redox Evaluation

During the Redox evaluation program, a DPT drilling method was used to advance the proposed exploration points located to the south side of Nonacoicus Brook. To conduct this evaluation program, a DPT groundwater sampling rod was advanced through the underlying soils, with vertical groundwater samples collected at 10 feet intervals to assess groundwater chemistry and arsenic concentrations within the overburden aquifer as discussed in a later section of this report. Soil samples were not collected during drilling operations, or groundwater monitoring wells constructed, since this was not part of the goal of the drilling program. The primary purpose of this drilling program was to evaluate groundwater redox conditions and the potential limits of the release along and near Nonacoicus Brook. Each of these points was terminated at refusal conditions. The exploration points conducted under this phase of the program were identified as SHM-10-17 through SHM-10-27.

## 3.4 Temporary Monitoring Well Installation

As described in the previous section, temporary monitoring wells (Refer to **Figure 2** and **Figure 3**) were installed to evaluate groundwater chemistry within the North Impact Area, Delineation area, North Plume Capture area, East Plume near Red Cove, and Landfill MNA/SS Conditions. The locations of these points were plotted and mapped based on Global Positioning System coordinates. Vertical profiling of arsenic concentrations and field parameters for groundwater was conducted during drilling operations at each of the points to determine the construction screening depth for the temporary monitoring wells. Temporary groundwater monitoring wells were constructed within each of the completed boreholes, with the exception of SHM-10-09, and SHM-10-17 through SHM-10-27. The construction of a well at location SHM-10-09 was



eliminated since no evidence of arsenic was detected within the groundwater profiling samples. Additionally, monitoring wells were not constructed within SHM-10-17 through SHM-10-27 since these points were used to profile redox conditions along Nonacoicus Brook.

At each well location, the well point screening depth was based upon the arsenic profiling results (see **Table 5**). In general, each well was constructed with a 10-foot to 20-foot long PVC screen located at the maximum depth explored or at a depth corresponding with the maximum arsenic concentration. Filter sand was placed around the PVC screen and extended 2 to 3 feet above the well point screen. Next, a two foot thick bentonite seal was installed, followed by grouting the remainder of the void to within two feet of grade. At ground surface a protective casing (stand pipe or flush mounted gate box) was installed to complete each location. With the exception of well SHM-10-07, and SHM-10-11 through SHM-10-16 (2-inch PVC material), each was constructed using 1.5 inch diameter PVC material. A summary of the temporary monitoring well construction information is summarized on the boring logs which are attached as **Attachment A** to this report. Sovereign personnel developed each of the wells several days after construction in accordance with EPA Well Development procedures.

### 3.5 Media Sampling

During this investigation select groundwater and/or soil samples were collected and submitted for laboratory analysis. The limits of the testing or field screening program are outlined under the following sub-sections. Refer to **Tables 2** through **Table 5** for soil, groundwater profiling, and groundwater monitoring results. The locations of these sampling points are outlined within **Figures 2** through **Figure 5** of this document. All sampling operations were completed using the protocols and procedures outlined within the FSP, DAP, and USP-QAPP.

#### 3.5.1 Field Screening

Groundwater samples obtained during the sampling operations were field screened or analyzed as detailed in the subsections below:

##### 3.5.1.1 Arsenic Test Kit

Upon reaching the groundwater table, profiling samples were obtained at 10-foot sampling increments at both DPT and roto sonic drilling locations. At each profiling interval, groundwater was purged using either a stainless steel bladder pump or a peristaltic/inertial pump and select monitoring parameters recorded (**Section 3.6.1.2**). Next, representative samples were obtained and screened using an Industrial Test Systems Quick As - arsenic field test kit. These field testing results were used to provide preliminary information on the concentration of arsenic within the groundwater samples, and assist in the placement of the monitoring well screening depth. To confirm and obtain accurate information of the actual arsenic concentrations, a split sample was submitted for laboratory analysis. A comparison of the field testing results is detailed in **Table 5**. The field arsenic testing was conducted on the dissolved samples only. Prior to conducting the drilling program, a correlation study was conducted on several of the onsite monitoring wells RSK-12, RSK-24A, RSK-27, and RSK-32. The results of the testing program indicated the following:

Location	Laboratory Concentration	Arsenic Test Kit
RSK-12	736-ug/l	> 500-ug/l
RSK-27	425-ug/l	Approx 500-ug/l
RSK-32	285-ug/l	250 to 300-ug/l
RSK-24A	0.79-ug/l	5-ug/l

### 3.5.1.2 Sampling Parameters

During groundwater profiling and monitoring well sampling, the samples were passed through a YSI meter with a flow-through cell, which was properly calibrated at the beginning of each day and post-calibrated at the end of the day. The YSI was used to monitor, dissolved oxygen, pH, temperature, specific conductivity, and oxygen reduction potential. A separate turbidity meter was used to monitor turbidity. Samples were collected upon achievement of field parameter stability, if the event field parameters did not stabilize within 2 hours, samples were collected at the 2 hour time mark. Summaries of the results are provided in **Table 2** and **Table 3**, and the sampling monitoring logs are attached as **Attachment C**.

### 3.5.2 Soil Sampling

During the rotosonic and DPT drilling programs, representative soil samples were collected using a continuous sampling approach. Each sample was reviewed, classified and logged by the site geologist. Only soil samples collected during the rotosonic drilling events were stored, with representative soil samples designated for laboratory analysis or the column study. In general, the underlying soils consisted of sand with varying percentages of silt, gravel, and rock fragments. Refusal conditions were encountered, presumably at bedrock at each of the completed boreholes, with glacial till encountered above the refusal conditions in several locations. A detailed summary of the soil conditions is provided on the Boring Logs which are attached as **Attachment A** to this report.

Three soil samples obtained from SHM-10-07 at sampling depths of 29-feet, 41-feet, and 53-feet were analyzed for TAL Metals and TOC. In addition, 86 soil samples obtained from SHM-10-11 through SHM-10-16 were analyzed for concentrations of TAL Metals (aluminum, antimony, arsenic, barium, beryllium, cadmium, calcium, chromium, cobalt, copper, iron, lead, magnesium, manganese, mercury, nickel, potassium, selenium, sodium, thallium, vanadium, and zinc) and TOC. Each soil sample was analyzed following the appropriate analytical methods listed in worksheets 15-3 and 15-4 of the approved UFP-QAPP. As part of this sampling program, QA/QC procedures included the use of duplicate samples, matrix spikes, matrix spike duplicates, and rinsate blanks. The orientation and results of the testing is summarized in **Table 4**, with the laboratory report attached as **Attachment D**. None of the soil samples obtained during the DPT drilling were submitted for laboratory analysis. No soil samples were collected during the completion of the redox profiling sampling program (SHM-10-17 through SHM-10-27).



Soil cores from borings SHM-10-07 and SHM-10-11 through SHM-10-15 were also sampled to obtain representative strata within each boring to aid in the MNA/SS evaluation. The focus of the sampling was to profile TOC, DOC, DIC, Eh, pH, Conductivity, Turbidity, Total and Dissolved arsenic and iron in the landfill since arsenic mobilization is primarily due to enhanced reducing conditions from the landfill. As long as strongly reducing conditions exist, arsenic will continue to enter groundwater. The samples collected from the borings were selected for analysis via the following methodology:

- 1.) Collection of discrete samples from the waste, peat, and wetlands deposits that constitutes the likely layers in the landfill profile,
- 2.) Collection of aquifer sands overlying bedrock based on recognizable strata,
- 3.) Collection of the upper 5 ft of weathered and/or bedrock, and
- 4.) All cores were logged in the field. Based on core logging, samples from each important strata were collected

Where soil cores encountered landfill waste and/or bedrock, waste samples were analyzed for:

- Total metal(loid)s (TAL)
- TOC
- X-ray Diffraction (XRD) for common mineralogy
- Sequential Chemical Extraction to identify major solid phase partitioning of arsenic, and
- Thin-section/scanning electron microscopy for identification of arsenic and metal bearing phases.

### 3.5.3 Groundwater Sampling

Groundwater samples were obtained during the profiling operations and monitoring well sampling program (2 events spaced approximately 2-3 months apart) were used to evaluate groundwater contaminant and chemistry conditions. The results of the testing program are summarized within **Tables 2** and **Table 3**, with the laboratory reports attached as **Attachment E** and **Attachment F** to this report. Copies of the field sampling logs are attached as **Attachment C**. The locations of each sampling point are detailed in **Figures 2** and **Figure 3**. As part of this sampling program, QA/QC procedures included the use of duplicate samples, matrix spikes, matrix spike duplicates, and rinsate blanks. All groundwater samples were collected in accordance with the January 2010 USEPA Region I Low-Stress / Low-Flow groundwater sampling guidance document.

New wells and select existing wells were also sampled to provide at least 6 transects for geochemical analysis. The data was analyzed to identify major geochemical changes in the north end of plume and along several transects emanating from beneath the landfill and extending into the north end of the plume. For the flow path analysis, the following well transects were analyzed (**Figure 2** and **Figure 3**):

- a. **Transect A-A'**: Landfill South to North: SHM-10-11 , SHM-10-12, SHM-10-14, SHM-10-15, SHM-10-16, SHM-10-18, and SHM-10-24
- b. **Transect B-B'**: East of center of landfill South to North: SHM-10-11, SHM-10-07, SHM-10-06A, SHM-10-16, SHM-10-18, and SHM-10-24
- c. **Transect C-C'**: West to East at Wetland Boundary, Wells SHM-10-22, SHM-10-10, SHM-10-19, SHM-10-17, SHM-10-23, SHM-10-25, and SHM-10-27
- d. **Transect D-D'**: West to East at Wetland Boundary, Wells SHM-10-22, SHM-10-10, SHM-10-19, SHM-10-18, SHM-10-24, and SHM-10-25
- e. **Transect E-E'**: West to East on North side of Brook Wells SHM-10-08, SHM-10-02, SHM-10-03, and SHM-10-04.
- f. **Transect F-F'**: South to North across Wetland, Wells SHM-10-08, SHM-10-02, SHM-10-03, and SHM-10-04

#### 3.5.3.1 Groundwater Profiling

Upon reaching the groundwater table, profiling samples were obtained at 10-foot sampling increments. At each profiling interval, water was purged through a YSI flow through cell and monitored for DO, pH, temp, specific conductivity, and ORP. Turbidity was monitored with a separate instrument. Next, representative samples were obtained and screened using an arsenic field test kit. A summary of the monitoring parameters and arsenic test kit results is provided in **Table 5**. In addition split samples at each sampling interval were laboratory analyzed for total and/or dissolved metals (arsenic, calcium, iron, magnesium, manganese, potassium, and/or sodium), alkalinity, ammonia, nitrite, COD, chloride, nitrate, and sulfate following the appropriate analytical methods listed in worksheets 15-1 and 15-2 of the approved UFP-QAPP. The groundwater samples were collected in accordance with the January 2010 USEPA Region I Low-Stress / Low-Flow groundwater sampling guidance document. A tabulation of the results is detailed in **Table 2**, while copies of the laboratory reports are provided as **Attachment F**.

#### 3.5.3.2 Temporary Monitoring Well Sampling

Temporary groundwater monitoring wells were constructed within SHM-10-01 through SHM-10-04, SHM-10-05A, SHM-10-06, SHM-10-06A, SHM-10-07, SHM-10-08, and SHM-10-10 through SHM-10-16. At each of these points, the construction depth of the well point screening was based upon the arsenic profiling results. Several days after installation, each monitoring well was purged and developed in preparation for the initial groundwater sampling event. During the two groundwater sampling events (separated by 2-3 months), the purge water was monitored for DO, pH, temp, specific conductivity, and ORP using a properly calibrated YSI meter. Turbidity was monitored with a separate instrument. Samples were collected after the field parameters stabilized or after 2-hours of purge if stabilization was not encountered. The collected samples were placed in the appropriate container, logged on a chain-of-custody, and analyzed for total and/or dissolved metals (aluminum, antimony, arsenic, barium, beryllium, cadmium, calcium, chromium, cobalt, copper, iron, lead, magnesium, manganese, mercury, nickel, potassium, selenium, sodium, thallium, vanadium, and/or zinc), hardness, alkalinity, TDS, TSS, ammonia, nitrite, nitrate, DIC, DOC, COD, TOC, chloride, sulfide, and/or sulfate following the appropriate analytical methods listed in worksheet 15-1 and 15-2 of the approved

UFP-QAPP. The groundwater samples were collected in accordance with the January 2010 USEPA Region I Low-Stress / Low-Flow groundwater sampling guidance document [EQASOP-GW001, Revision Number 3]. A tabulation of the laboratory results is detailed in **Table 3**, the field sampling parameters in **Table 5**, and the laboratory reports are provided as **Attachment E**.

### **3.6 Quality Assurance / Quality Control Procedures**

Field QC samples that were prepared and submitted to the laboratory for analyses during performance of this field effort consisted of equipment blanks (for all analyses), duplicate samples (for all analyses), and matrix spike/matrix spike duplicate samples (for all analyses). A summary of the QC samples is presented in **Table 2** through **Table 5**. The frequency and method of collection of field QC samples are described in the UFP-QAPP.

Decontamination of equipment used during the investigation program was conducted as follows:

- All down-hole drilling equipment was decontaminated prior to initial use and between each borehole. Non-dedicated groundwater sampling devices (i.e., pumps, etc.) were decontaminated prior to initial use and between collection of each sample to prevent the possible introduction of contaminants into successive samples. Equipment was decontaminated at the sample location, or at a pre-designated, controlled location. All equipment was decontaminated before leaving the site.
- Decontamination of drilling equipment included drill bits, drill-string tools, drill rods, tremie pipes, clamps, hand tools, steel cable, along with pump drop-lines and pumps. These items were cleaned, by the subcontractor, using a steam pressure washer.
- Equipment decontaminated included the water level and water quality meters, pumps and pump equipment, and miscellaneous tools. All items were cleaned using the method detailed within the Sampling Equipment Decontamination SOP which is part of the FSP.
- Heavily soiled equipment was washed a second time using an aqueous non-phosphate detergent solution and using a portable, high presser steam cleaning equipment.
- All non-dedicated equipment was decontaminated in accordance with the procedures presented in the Sampling Equipment Decontamination SOP which are part of the FSP.

## **4.0 SCREENING AND LABORATORY SAMPLING RESULTS**

The results of the field sampling and analysis are outlined within the following sub-sections. A discussion and evaluation of these results are covered under later section of this report. **Tables 2** through **Table 5** provide a summary of the results, and **Figure 2** through **Figure 3** for the location of the sampling points.



## 4.1 Field Screening

### 4.1.1 Arsenic Test Kit

As stated previously, an Industrial Test Systems Quick As - arsenic test kit was employed to field screen the collected groundwater profiling samples for concentrations of arsenic. In addition, a split sample was submitted to the analytical laboratory for arsenic testing. The arsenic field test kit was confined to a calibration range of less than 5-ug/l to a maximum of 500-ug/l. In general, a review of the results noted that the test kits provide a slight overestimate of the arsenic concentration. In some cases, sample dilution was used to evaluate concentrations over the 500-ug/l. A review of the results confirms that the temporary well screen construction depths were situated in zones of maximum arsenic impact. A tabulation of the arsenic test kit results against the laboratory results is provided in **Table 5** to this report.

### 4.1.2 Sampling Parameters

During groundwater sampling (profiling and monitoring well), the purge water was monitored for turbidity, dissolved oxygen, pH, temperature, specific conductivity, and oxygen reduction potential using properly calibrated field equipment. A summary of the results at the collection of the samples is detailed in **Table 2** and **Table 3**, while a copy of the monitoring log is attached as **Attachment C**.

## 4.2 Soil Sample Analytical Results

To characterize subsurface soil samples obtained during the exploration program, representative samples were collected and submitted for laboratory analysis. These samples were prepared in accordance with the testing methodology and analyzed for TAL Metals (aluminum, antimony, arsenic, barium, beryllium, cadmium, calcium, chromium, cobalt, copper, iron, lead, magnesium, manganese, mercury, nickel, potassium, selenium, sodium, thallium, vanadium, and zinc) and TOC. A summary of the concentrations ranges is recorded as follows:

Compound	Concentration in mg/Kg		Compound	Concentration in mg/Kg	
	Min	Max		Min	Max
Aluminum	1,400	30,000	Antimony	ND (< 0.17)	11
Arsenic	1	62	Barium	5	200
Beryllium	< 0.09	2	Cadmium	ND (< 0.03)	220
Calcium	250	25,000	Chromium	2	69
Cobalt	1	21	Copper	1	310
Iron	950	140,000	Lead	2	1,200
Magnesium	430	21,000	Manganese	22	3,000
Mercury	< 0.002	2	Nickel	3	101
Potassium	160	11,000	Selenium	ND (< 0.11)	3
Silver	< 0.03	14	Sodium	< 22	3,200
Thallium	< 0.23	< 2.19	Vanadium	2	49
Zinc	8	13,000	TOC	< 0.01 %	25%



Copies of the laboratory reports are attached as **Attachment D** and a complete summary of the soil testing results are tabulated in **Table 4**. **Figure 2** and **Figure 3** provide a depiction of the location of the sampling points.

### 4.3 Groundwater Sample Results

#### 4.3.1 Temporary Monitoring Wells

Following the construction and purging of the groundwater monitoring wells, two separate groundwater sampling and analytical events were conducted on the date and at the locations detailed on **Table 3**. Groundwater samples were collected from the wells using the procedures outlined in the FSP and USF-QAPP, and analyzed for total and/or dissolved metals (aluminum, antimony, arsenic, barium, beryllium, cadmium, calcium, chromium, cobalt, copper, iron, lead, magnesium, manganese, mercury, nickel, potassium, selenium, sodium, thallium, vanadium, and/or zinc), hardness, alkalinity, TDS, TSS, ammonia, nitrite, nitrate, DIC, DOC, COD, TOC, chloride, sulfide, and/or sulfate following the appropriate analytical methods listed in worksheet 15-1 and 15-2 of the approved UFP-QAPP. In general, concentration ranges were noted as follows and represent conditions at each of the well point screening depths of the analyzed monitoring wells:

Compound	Total Analysis (ug/L)		Dissolved Analysis (ug/L)	
	Min	Max	Min	Max
Aluminum	27.6	3,870	< 3.82	35.8
Antimony	0.19	1.93	0.17	2.99
Arsenic	0.59	7,930	0.14	8,110
Barium	40.3	160	36.5	154
Beryllium	< 0.118	0.07	0.07	< 0.59
Cadmium	< 0.236	< 0.59	< 0.236	< 0.59
Calcium	14,200	182,000	2,230	195,000
Chromium	0.38	15.9	< 0.186	0.73
Cobalt	0.84	28.6	0.73	29.3
Copper	0.64	6.88	0.34	2.06
Iron	508	149,000	16.9	145,000
Lead	0.07	4.72	ND (< 0.05)	2.08
Magnesium	1,660	23,600	163	127,000
Manganese	9.54	27,400	6.78	25,800
Mercury	< 0.012	0.1218	< 0.012	0.1268
Nickel	1.16	23.5	0.27	22.2
Potassium	1,770	18,800	841	101,000
Selenium	0.54	0.74	< 0.406	0.7
Silver	< 0.085	< 0.85	< 0.085	< 0.85
Sodium	7,090	536,000	1,400	536,000
Thallium	0.05	< 0.31	0.05	< 0.31
Vanadium	0.31	1.85	0.08	0.22
Zinc	3.49	54.6	3.91	37.7

Compound	Concentration in mg/L		Compound	Concentration in mg/L	
	Min	Max		Min	Max
Hardness	41	490	Alkalinity	4.3*	500*
TDS	110	1,900	TSS	ND (< 5)	640
Ammonia	ND (< 0.017)	9.7	Nitrite	ND (< 0.002)	0.5
COD	ND (< 7)	62	Chloride	1.3	1,100
Nitrate	0.008	3.8	Sulfate	< 0.12	87
Sulfide	ND (< 0.1)	ND (< 0.1)	TOC	0.64	4.8
DOC	< 1	62	DIC	< 8	150

\* Alkalinity units are mg CaCO<sub>3</sub>/L

Copies of the laboratory reports are attached as **Attachment E** and a complete summary of the testing results are provided in **Table 3**. The locations of the sampling points are shown in **Figure 2** and **Figure 3**.

#### 4.3.2 Profiling

Samples obtained during groundwater profiling were prepared in the appropriate laboratory container, logged on a chain-of-custody, and analyzed for total and/or dissolved metals (arsenic, calcium, iron, magnesium, manganese, potassium, sodium), alkalinity, ammonia, nitrite, COD, chloride, nitrate, and sulfate following the appropriate analytical methods listed in worksheets 15-1 and 15-2 of the approved UFP-QAPP. The concentration ranges were noted as follows:

Compound	Sampling Point	Concentrations in ug/L					
		Test Kit [Dissolved]		Dissolved		Total	
		Min	Max	Min	Max	Min	Max
Arsenic	GP-10-01	ND (< 5)	5	0.3	0.97	0.48	18.9
	GP-10-02	ND (< 5)	5	ND (< 0.226)	8.68	0.41	84.6
	GP-10-03	ND (< 5)	ND (< 5)	ND (< 0.452)	3.85	0.89	42.1
	GP-10-04	ND (< 5)	20	0.15	15.1	1.22	214
	GP-10-05	ND (< 5)	150	0.31	112	1.02	130
	GP-10-05A	ND (< 5)	ND (< 5)	0.33	5.09	0.93	911
	GP-10-06	5	> 500	10	2,540	17.2	2,660
	GP-10-06A	ND (< 5)	60	ND (< 1.13)	106	0.59	1,090
	GP-10-07	ND (< 5)	> 500	58	1,350	283	1,240
	GP-10-08	ND (< 5)	ND (< 5)	0.31	1.06	2.07	19.8
	GP-10-09	ND (< 5)	ND (< 5)	0.15	0.94	0.45	183
	GP-10-10	ND (< 5)	ND (< 5)	0.27	2.47	0.34	13.7
	GP-10-11	< 5	150	19.8	396	230	760
	GP-10-12	30	> 500	38.9	3,880	--	4320
	GP-10-13	< 5	> 500	12.2	1,060	120	176

Compound	Sampling Point	Concentrations in ug/L					
		Test Kit [Dissolved]		Dissolved		Total	
		Min	Max	Min	Max	Min	Max
Arsenic	GP-10-14	5	> 500	14.4	15,100	39.1	17,300
	GP-10-15	70	> 500	278	16,600	—	17,200
	GP-10-16	< 5	100	1.89	445	19.3	333
	GP-10-17	< 5	500	0.25	1,860	0.58	1,950
	GP-10-18	< 5	80	0.73	390	0.93	373
	GP-10-19	< 5	100	0.35	810	0.53	886
	GP-10-20	< 5	50	0.066	429	1.6	446
	GP-10-21	< 5	60	0.31	349	1.48	322
	GP-10-22	< 5	< 5	0.37	14.5	0.51	15.8
	GP-10-23	< 5	> 500	0.38	1,100	0.52	1,160
	GP-10-24	< 5	250	0.39	615	1.52	629
	GP-10-25	< 5	5	0.4	34.9	10.9	44
	GP-10-26	< 5	< 5	0.18	1.96	0.6	6.48
	GP-10-27	< 5	> 500	0.38	1,040	1.11	1,100

The GP and SHM notation refer to the same locations. Refer to **Figure 2** and **Figure 3** for the location of these points using the SHM notation.

Dissolved Compound	Concentration in ug/L		Dissolved Compound	Concentration in ug/L	
	Min	Max		Min	Max
Aluminum	4.17	345	Antimony	< 0.12	2.39
Barium	5.73	244	Beryllium	< 0.059	< 0.295
Cadmium	0.08	< 0.59	Calcium	2,100	288,000
Chromium	0.2	2.66	Cobalt	0.31	45.2
Copper	0.25	4.32	Iron	57.9	122,000
Lead	< 0.01	0.59	Magnesium	218	38,700
Manganese	21.1	30,700	Mercury	< 0.012	0.1389
Nickel	1.34	25	Potassium	422	25,400
Selenium	< 0.406	0.79	Silver	< 0.085	< 0.34
Sodium	639	598,000	Thallium	< 0.031	0.21
Vanadium	0.1	2.23	Zinc	1.81	44.4
Hardness	210	210	Alkalinity	9 mg CaCO <sub>3</sub> /L	530 mg CaCO <sub>3</sub> /L
TSS	< 5	55,000	Chloride	0.43	1,200
Ammonia	0.0166	17.3	Nitrite	ND (< 0.002)	0.025
Nitrate	0.009	5.8	Sulfide	< 0.1	< 0.1
Sulfate	ND (< 0.12)	97	COD	ND (< 7)	170
DOC	< 1	15	DIC	6.4	170

Copies of the laboratory reports are attached as **Attachment F** and a complete summary of the testing results are provided in **Table 2**. The locations of the sampling points are shown in **Figure 2** and **Figure 3**. Geological profiles depicting the concentration gradients of the results are attached as **Figures 6** through **Figure 28**. These profiles show the vertical groundwater profiling results of dissolved arsenic, dissolved iron, dissolved manganese, oxidation reduction



potential (Eh), and dissolved organic carbon. An evaluation of these profiles is presented in **Section 6.0** of this report.

#### **4.4 Landfill Gas Evaluation**

For this evaluation, AMEC evaluated whether dissolved methane gas in groundwater from the landfill presents a potentially unacceptable hazard to nearby structures. Methane is not toxic at concentrations up to the lower explosive limit (LEL) and is an asphyxiant at higher concentrations. The primary concern is thus the possibility of methane gas explosion within structures. The results of this investigation determined dissolved methane conditions did not pose an explosive hazard within 10-feet of a building using a dissolved methane concentration of 10-mg/l. A copy of the Landfill Gas Evaluation Report prepared by AMEC is attached as **Attachment G**.

#### **4.5 Data Validation**

Sovereign contracted AMEC to conduct a data validation of analytical data collected during the field investigation program. AMEC's data validation and data quality review methodology complied with the validation procedures specified in the QAPP. In accordance with the specifications of QAPP Worksheet #35, all laboratory data was processed through the ADR software and the ADR reports were reviewed by an AMEC chemist. A Data Validation Report was prepared for each laboratory sample delivery group indicating any data limitations.

The review of soil and ground water sampling results were evaluated for the usability of the data and to determine any limitations on their use in drawing conclusions about the extent of contamination at the Shepley's Hill Landfill. Based on the data validation and data quality assessment, the analytical data set completeness was calculated as 100 percent. No data was rejected.

A number of analytical and/or sampling biases were applied to the data set. These were the result of imprecision between laboratory and field duplicates, low and high matrix spike recoveries, low or high post digestion spike recoveries, high serial dilution relative percent differences, exceeded holding times, and results reported between the LOQ and LOD. Overall, results were qualified as estimated (J or UJ). These data are considered usable and of acceptable quality. Additional biases were applied due to detections in associated method, calibration and equipment results. Results that had concentrations less than 10-times the blank concentrations were U qualified because of potential contamination.

Overall, the data set satisfies completeness and quality objectives and data can be used for their intended purposes with confidence. Copies of the Data Validation package are provided as **Attachment H** to this report.



## 5.0 EVALUATION/UPDATE HYDROGEOLOGIC CONDITIONS

This hydrogeologic assessment integrates data collected during 2010 including geophysical survey transects in the Nonacoicus Brook area, lithologic logs and refusal depths from borings constructed within and downgradient of the landfill footprint, and water levels collected from both existing and new monitoring wells.

### 5.1 Bedrock Surface

Based largely on the results of the geophysical survey, it is evident that the buried bedrock surface, and consequently the saturated thickness of the permeable overburden aquifer, is considerably shallower than previously interpreted in the Nonacoicus Brook area (see **Figure 29**) by as much as 50%. Boring refusal depths around Nonacoicus Brook confirm these results. It should be noted that there are some discrepancies with the presumed bedrock depths encountered during DPT investigations due to the two-step process of the DPT work. In many cases, the initial vertical profiling DPT work was completed with narrow diameter drilling tools which may be able to penetrate into glacial till and/or saprolitic rock. Secondary DPT work to install the temporary wells was completed using larger diameter tools necessary to install the wells. In some instances, the depth to refusal for the second phase of drilling was shallower than the first. In general, refusal and presumed bedrock depth evidence is weighted to the depths noted by the smaller diameter vertical profiling results. Further, the broad east-west trending bedrock 'trough' thought to be present under the brook corridor instead consists of both a narrow east-west trending 'tributary' directly under the brook axis and a north-northwest trending tributary which extends north of the brook. The reduction in overall saturated thickness due to this structure requires that horizontal groundwater velocities are higher than previously interpreted and modeled in this area as there is substantially less aquifer through which it can flow. Based on the assessment of hydraulic gradients discussed below, it is most likely the deep arsenic plume is confined to the east-west trending trough directly under the brook axis and not the north-northwest trending trough. This is also supported by the absence of arsenic in SHM-10-04 located directly within this trough.

Within and around the landfill, boring refusal depths are both shallower and deeper, however, they generally confirm the prior interpretation of a north-south trending bedrock trough just east of Shepley's Hill. Immediately west of Red Cove at SHM-10-07 and in the area east of the extraction wells at SHM-10-06, bedrock was shallower than previously understood, further confirming the presence of a north-south trending ridge generally coinciding with the eastern edge of the landfill cap.

As groundwater flow patterns at the site are strongly influenced by variations in saturated thickness, these data have significant implications with respect to preferential pathways within the overburden aquifer. Consequently, this information has been integrated into the latest groundwater model variants to provide updated predictions of contaminant flow paths as discussed below.

## 5.2 Lithologic Features

In terms of lithologic variations within the overburden that might also define preferential pathways, the new borings are consistent with previous observations that local overburden is dominantly well sorted sands with little stratification. Gravelly zones were present in a few of the borings in and around Nonacoicus Brook (SHM-10-01, SHM-10-03, SHM-10-09, and SHM-10-10), consistent with where gradients decrease and hydraulic conductivity is hypothesized to increase. The sole occurrence of a silt lens was in SHM-10-02 midway within the 60' of overburden. Within the landfill footprint fairly thick occurrences of peat were found in SHM-10-13 and SHM-10-14, consistent with their location in the historic wetland. This unit may have hydraulic implications and potentially could result in perched or semi-confined conditions locally. Lastly, the basal till unit is further confirmed to vary widely in terms of its thickness and is in places laterally discontinuous.

## 5.3 Water Levels

Static water levels were collected from all new monitoring wells between July and October. These data were integrated with the regularly scheduled fall synoptic survey of existing wells conducted under the Long Term Maintenance and Monitoring Plan (LTMMP) to produce a current water table elevation map (**Figure 30**) extending to the Nonacoicus Brook area. While this may not represent a true synoptic snapshot of the water table, it is evident that Fall 2010 water levels are uniformly lower than for Fall 2009 (and long term averages) particularly around the extraction wells, a condition likely related to the late summer drought experienced across the region. As a consequence, horizontal hydraulic gradients are generally 'flatter' or lower than under more typical seasonal conditions, ranging from 0.003 to 0.012 ft/ft over the majority of the landfill (corresponding to groundwater transport velocities of 0.15 to 1.7 ft/day). In contrast, the gradient along Nonacoicus Brook is considerably flatter, on the order 0.0015 ft/ft. Within the northern half of the landfill groundwater flow direction, as inferred from water table contours, is predominantly northward, while in the southern half flow direction is more north-northeast. It should be noted that water levels in the N5 cluster are higher than those in the three new wells immediately surrounding it (and existing well SHP-99-29X) though water levels in those wells appear internally consistent.

A number of vertical well pairs in the area downgradient of the extraction wells exhibit water level differences of 1 to 3 feet including SHM-99-31, SHM-05-34, SHM-05-39, SHM-05-49, and the N1 cluster. This difference is presumably related to the 'deflated' water table resulting from drought conditions. These strong downward gradients are interpreted to reflect increased recharge to the shallow aquifer from the pond, and the portion of Nonacoicus Brook nearest the pond, relative to typical seasonal conditions.

Water levels from new wells both south and north of Nonacoicus Brook suggest the horizontal gradient, though not very steep, is uniformly westward. Consequently, the projected arsenic plume trajectory based on field data alone is along the axis of the brook, consistent with previous groundwater flow path modeling predictions.

## 5.4 Particle Track Prediction

In order to update the numerical groundwater flow model and flow path predictions using the particle tracking technique, the revised bedrock surface interpretation shown in **Figure 29** was incorporated into the current model (SHL007). The groundwater flow model was revised subsequent to the 2010 Supplemental Investigations, principally through adjustment of the interpreted bedrock surface. The development, calibration and refinement of the revised model (SHL008) was reported in the *AOC 72 Remedial Investigation Report* (AMEC, 2011) and the 2009 Annual Report (ECC, 2010). The latest revisions were focused on the bedrock surface, integrating data from drive points, borings, and geophysical studies undertaken as part of the SAR. This revised model is used to explore a range of hydraulic control remedial alternatives in this FFS. The model in its present state is considered adequate to support early-stage comparison of remedial alternatives for the FFS, but will be further refined to support the Remedial Design. Subsequently, the impact of this structural change on calibration of the model was evaluated. It can be shown that not only does this new variant adequately match long-term average water levels (see **Table 6** and, **Figure 31**) but calibration was slightly improved relative to preexisting data.

Using the revised model (SHL008), forward particle tracking was conducted to both update the prediction of current captures zones (**Figure 32**) and simulate the trajectory of current Arsenic exceedances in the aquifer, including those in new wells constructed in 2010 (**Figure 33**). Relative to the previous model predictions documented in the 2009 Annual Report (ECC, 2010) the capture zone under peak operating rate (49 gpm) is slightly larger, extending farther east some 50-60 feet closer to the landfill boundary. This is likely the direct consequence of the reduction in average saturated thickness due to bedrock being shallower than previously interpreted.

As depicted in **Figure 33**, patterns of flow and velocity relationships have changed somewhat relative to previous predictions. Predicted groundwater transport velocities within the landfill average just over 0.6 feet/day and are largely identical to the preceding SHL007 model. In the area immediately downgradient of the landfill toe, velocities average just under 0.5 feet/day, as the magnitude of horizontal hydraulic gradient declines slightly. Within the Nonacoicus Brook corridor, gradient is much flatter and consequently velocities rapidly decline to less than 0.1 feet/day as the deeper groundwater flow becomes entrained with the westward flowing stream. The most significant difference between previous predictions and the new SHL008 model is that particle tracks representing detections all discharge upgradient of the 'bend' in the brook, and no longer travel farther west before discharging into Nonacoicus Brook or the Nashua River. This again is a direct consequence of the reduction in average saturated thickness due to bedrock being significantly shallower than previously interpreted. Further, the quantity of water predicted to discharge along the brook is increased, as would be expected with less aquifer available through which to flow horizontally.



## 6.0 MNA/SS LANDFILL REDUCING CONDITIONS EVALUATION

The purpose of this section is to present collected data and to summarize the technical findings concerning (1) Shepley's Hill Landfill groundwater characterization, (2) the landfill source strength (SS) and reducing conditions, and (3) effectiveness of monitored natural attenuation (MNA). This section also addresses data gaps as outlined in the AMEC 2010 Supplemental Groundwater Investigation Workplan Volumes 1 and 2, Sovereign 2010 Supplemental Investigation Workplan Volume 1 and 2, and the AMEC 2009 Supplemental Groundwater and Landfill Cap Assessment. The data and data interpretation presented here also serves to supplement information required for the Sovereign 2010 Focused Feasibility Study.

While source strength/landfill reducing conditions, site characterization, and evaluation of data for possible remedial alternatives appear as separate topics, they are linked in the overall conceptual site model and development of criteria for selecting an appropriate remedy for the landfill.

### 6.1 Objectives

The specific objectives are identified in Table 1 of the Sovereign Workplan (May 2010) and include:

- **Objective 1 - Natural Attenuation for the North Impacted Area** - Once capture (hydraulic control from the ATP) is demonstrated, establish that natural attenuation will be effective at remediating the North Impacted Area) within a timeframe that is reasonable given the circumstances of the site.
- **Objective 2 - Source Strength/Landfill Reducing Environment Evaluation** - Estimate the duration of the landfill's ability to maintain reducing/methanogenic conditions.

The results presented here are used to determine if attenuation is effective for remediation of the arsenic plume north of the arsenic treatment plant (ATP) capture zone within a timeframe that is reasonable given the complexities of the site due to the landfill induced reducing conditions. Evaluation of attenuation involves identifying the current distribution of arsenic in local groundwater and identifying the fate of arsenic as it moves from the landfill along the identified flow paths to its ultimate fate some distance from the landfill. In the present case this requires evaluation of the arsenic in the flow path as it approaches the Nonacoicus Brook and associated wetlands to the north of the landfill.

The study also addressed data collected to date that is required to determine the time it will take for the aquifer to return to normal (pre-landfill) if reducing and/or anaerobic conditions created by the landfill and underlying peat and wetlands were to cease. Pre-landfill in this context simply suggests the condition of the aquifer prior to landfill emplacement. While the landfill presumably leached arsenic and created its own reducing conditions, some degree of anaerobic conditions existed prior to the landfill due to the existence of the wetlands and peat over which the landfill was placed. The attempt to determine the pre-landfill conditions and the time it takes for restoration to occur to bring these conditions back is referred to as Source



Strength/Landfill Reducing Environment Evaluation. The landfill evaluation was approached by recognizing that arsenic release from beneath the landfill is linked to conditions within the landfill that add to reducing and methanogenic conditions including the presence of a peat layer within the former wetlands. Both arsenic and carbon cycling was evaluated in order to determine the landfill impact and the length of time required for arsenic or carbon depletion to occur.

In the present case, the landfill impact to reducing conditions and subsequent mobilization of arsenic is confounded by the presence of underlying wetlands and peat layers existing beneath and within the landfill footprint. The data collected as part of this study demonstrated that the underlying wetlands and peat layers generate their own reducing conditions with or without the landfill.

## 6.2 Review of Data Collection Efforts

In the summer of 2010 the following field work and types of samples were collected. A description of the data gaps, use of samples and resulting data is described in the 2010 Workplan Addendum and summarized below:

<b>Data Gap</b>	<b>Data Collection Objectives</b>	<b>Type(s) of Samples Collected</b>
Arsenic Distribution in Landfill and North Impacted Area	Fate and Transport Transect Analysis	2 rounds of groundwater sampling Landfill groundwater profiles DPT samples
Redox Boundary/MNA	Comparative water geochemistry	DPT samples North placed wells and water samples
Landfill Profiling: Solids and Water profiles	Landfill borings for solids and water	5 new borings and landfill wells
Arsenic Source and Fate	Solids and water geochemistry Column studies	Core samples from 6 borings Water profiles from new borings Select core for flushing and release studies
Carbon Source and Fate	Solids and water geochemistry Column studies	Core samples from 6 borings Water profiles from new borings Select core samples for flushing and release studies
Waste Distribution and Characterization	Landfill borings for solids	Core samples by lithology for 6 new borings

### 6.2.1 Laboratory Bench and Column Studies

Several bench and column studies were initially proposed and are listed below. These studies include:

- A column study to determine the time (estimated from pore volumes) for clean water to restore the column to background conditions under conditions of high arsenic in pore water,
- A column study to determine the time for clean water to restore the column to background conditions under moderate arsenic pore water concentrations,
- A batch study to determine the rate at which organic carbon is degraded under anaerobic conditions
- A batch study to determine the distribution coefficient ( $K_d$ ) of arsenic sorption to native aquifer sands, and
- A column study to determine the rate of release of arsenic from aquifer sands under reducing conditions typical of the landfill environment.

The initial list of bench studies was altered during the course of the investigation based on the data collected and were amended to the studies described below:

- Two column studies were conducted. The first was designed to test the number of pore volumes required to flush arsenic free from the sand under the influence of oxidized water infiltration.
- A second column study was conducted that also examined the number of pore volumes required to flush arsenic from a core sample but under reducing conditions instead. The same column was then allowed to run with more infiltration of reducing water in order to determine how much arsenic would be re-mobilized from the sand under continued reducing conditions. This study is essentially similar to the one designed to look at rate of release of arsenic under reducing conditions.
- The initial results and usefulness of the carbon degradation study is in question since only minute amounts of gas have been collected to date. This lack of degradation is now thought to be due to the negative effect of freezing on the microbial population. Therefore, the study was terminated since it would not provide any further information concerning carbon degradation rates.
- The  $K_d$  study was not done since the discussion with BCT and USACE indicated that a  $K_d$  developed from one site sample was probably insufficient to provide any meaningful data.
- All laboratory data can be found in **Attachment I** (Report of Findings, PRIMA Environmental).

#### 6.2.1.1 Column Study

The high TOC arsenic flushing test under oxidizing conditions is described here along with the flushing of arsenic and remobilization column study under reducing conditions. (Refer to the PRIMA Environmental: Report of Findings, Shepley's Hill Landfill 2011, **Attachment I** for all column data).

The high arsenic column flushing test was conducted in duplicate using 2 inch diameter clear PVC pipe approximately 24 inches long. The columns were filled with approximately 3 kg of landfill soil from a moderate to relatively high (about 1,200 ug/L) arsenic containing portion of the landfill area and packed to a density similar to the native field density (see **Attachment I** for details). Next synthetic water (water that was made in the laboratory and based on composites of non-impacted well water from the site, refer to **Attachment I** for the composition) similar to up-gradient native groundwater was passed through the column in an up flow direction at a rate of about 1 pore volume per day. Effluent was collected in Tedlar bags in 12 hour increments (for example, 0-12 hours, 12-24 hrs, etc) for the first 3 pore volumes, after which it was collected in 24 hour increments. Influent water and effluent samples for the first 2.5 pore volumes, were analyzed for arsenic (total dissolved), total dissolved iron, DO, DOC, ORP, and pH. Additional samples in additional pore volumes were analyzed for the same constituents.

The study design is very similar to that conducted by the USGS at the Saco Landfill in Maine. The column parameters are summarized in **Attachment I**.

The second column test was conducted in exactly the same manner as above with a few important differences:

- The column was pre-flushed with reducing water made by passing tap water through zero-valent iron and then into the column.
- The reduced water was allowed to flush pore water arsenic out of the column until <5 ug/L As could be detected.
- At this point reducing water was allowed to flow through the column at about a rate of 0.3 ft/day. Samples were collected every 3 to 4 days to examine the rate at which arsenic could be re-released or mobilized from the solids entrained in the sands.

Modeling of the column data and some of the transect data was also completed to understand the significance of geochemical changes due to the landfill conditions and at the redox boundary at the north end of the impacted area. Chemical analysis and speciation in the transects following groundwater flow was modeled using MINTEQA2 (USEPA), Geochemist's Workbench and PHREEQC2 which allowed a well by well comparison of key geochemical changes such as iron and arsenic solubility and precipitation as well as changes in dissolved oxygen, sulfate and Eh. Column data was analyzed using PHREEQC2 (USGS, 1999) which can be used to assess the changes in arsenic concentration due to geochemical conditions versus those due only to advection-dispersion. In this exercise, the flushing results were compared to model results where only advection and dispersion were considered since arsenic was removed not by adsorption or attenuation but by displacement with water containing no arsenic. The modeling input and output is also presented in **Attachment I**.



### 6.3 Site Characterization and Arsenic Distribution

Historic and recent data collected for examining arsenic distribution at the landfill includes water samples from numerous wells located adjacent to and down-gradient from the landfill, cores collected from borings, sediment samples and surface water samples. What is known presently and confirmed by the results of the newest work is presented herein:

- The landfill and underlying peat increase arsenic solubility due to biodegradation of carbonaceous material, oxygen depletion, creation of reducing conditions, and the reductive dissolution of arsenic containing iron solids;
- The landfill is not the main source of arsenic or dissolved organic carbon. Most arsenic appears to be associated with iron coated sands below the waste;
- The landfill cap is effectively decreasing the interaction of meteoric water with landfill waste;
- Only a portion of the waste is in contact with groundwater. Based on new estimates (Sovereign 2010) approximately 11% of the waste is thought to be saturated;
- Groundwater beneath the landfill has been characterized in terms of flow direction and velocity. Groundwater flow and direction has been modeled. In addition dissolved and suspended analytes in the groundwater flow path have been identified and quantified;
- Arsenic is likely precipitating beneath the wetlands at Nonacoicus Brook. The Brook appears to represent the northern most edge of the contaminated groundwater plume from the landfill. This area is also the primary redox boundary which occurs near or at the Brook/wetlands area north of the landfill; and,
- The redox boundary has been generally identified and the fate of arsenic at the Brook/wetlands investigated.

#### 6.3.1 Arsenic Distribution in Landfill and North Impacted Area

The vertical and horizontal distribution of arsenic and other analytes within and north of the landfill in the north impacted area are presented as a series of geological transects constructed using the water chemistry profiles compiled from Sovereign temporary well installation and groundwater profiling conducted in 2010 and described below.

The transect locations are depicted in **Figure 2** and **Figure 3** and the arsenic distribution in each transect in **Figure 6** to **Figure 11**. Other analytes in the same transects are shown in **Figure 12** to **Figure 28**. Please note that only wells with depth profiles are shown in this exercise. Each transect is discussed below.



#### 6.3.1.1 Geological Transect A-A' and Groundwater Profile Analysis

This transect is a south to north view of arsenic with depth from the south end of the landfill (SHM-10-11), through the center of the landfill (SHM-10-12,, SHM-10-14 and SHM-10-15) and then north to the Brook and wetlands (SHM-10-16, and SHM-10-18 and SHM-10-24) (**Figure 2, Figure 3, Figure 12, Figure 17, Figure 21 and Figure 26** show other analytes along this transect). The transect represents a two dimensional slice through the apparent center of the highest arsenic area and then follows arsenic north as the concentrations gradually diminish. The highest arsenic concentrations are found in groundwater beneath wells SHM-10-14 and SHM-10-15 where arsenic exceeds 14,000-ug/L. The arsenic follows the dipping bedrock surface to the north and arsenic in general is found to be highest at depth above the till layer, in all wells except SHM-10-12 where high arsenic is encountered at 44 ft bgs. Proceeding north, there is a thinner profile of high arsenic through SHM-10-16 (about 500 ug/L) and then much lower arsenic at the Brook/wetlands boundary (<400 ug/L). This north end distribution is discussed further in the C, D and E Transects.

The arsenic distribution along the transects is noteworthy for several reasons:

- The highest arsenic concentrations are frequently found at depth. This could be from a source of arsenic that is at the same depth of the arsenic found in the groundwater, or due to a source of arsenic in the underlying aquifer that is not associated with the landfill. . While several theories have been hypothesized for the existing distribution of arsenic, the data presently cannot confirm or deny these depositional hypotheses. Presently, it has been estimated based on drilling observations and mass calculations that only 11% of the waste is in contact with groundwater. Therefore the landfill may not be a significant source of arsenic presently but may have been one earlier in its history. The distribution of arsenic at Shepley's Hill is also similar to that found at the Winthrop Landfill in Maine. Keimowitz et al. (2005). At that site, the authors point to several lines of evidence as to why the Winthrop Landfill was not a source of arsenic. These include lack of enrichment of arsenic in hot spots beneath the landfill and in soil immediately below the waste, the fact that capping the landfill has not reduced arsenic concentrations in groundwater to any observable degree, and the fact that waste was not enriched in arsenic relative to native soil or rock, similar to Shepley's Hill.
- Some locations in the center of the landfill have very high arsenic concentrations (>14,000 ug/L) at depth but then immediately above the glacial till layer, arsenic concentrations in groundwater decrease dramatically to less than 400-ug/L. This may be due to infiltrating non-impacted groundwater entering beneath the landfill as recharge. At SHM-10-12 and SHM-10-15, groundwater at about 60 ft was partially oxygenated (6-mg/L) and contained arsenic at about 300-ug/L. This could be the original infiltrating landfill leachate boundary or recharging groundwater. Given the high DO contents, the latter seems more plausible as dissolved organic carbon would likely have caused the original oxygen in this layer to be consumed. Recent work by Gannett Fleming (2011) indicates that this lower concentration of arsenic in bedrock and till originates from oxidation reactions in the surrounding bedrock which then feeds the aquifer sands a continuous source of arsenic.

- The bedrock and till do not appear to be a major source of arsenic. Under oxidizing conditions as noted above, arsenic solubility will likely be controlled by sulfide oxidation (eg pyrite) which could lead to arsenic concentrations up to 400-ug/L as noted in the USEPA well on Shepley's Hill. While the concentration from bedrock weathering reactions, this process may be the original source of arsenic responsible for the arsenic enrichment in the aquifer sands prior to reducing conditions.
- Also as discussed with the BCT, it is understood that establishing a background number for SHL groundwater arsenic will be determined based on a monitoring program that is instituted as part of the final remedy as well studies performed by others including but not limited to the USGS, EPA and MassDEP. The USGS (USGS Special Report 2011-5013), EPA and MassDEP have and are performing studies to determine the background arsenic concentration in the regional groundwater. These studies have demonstrated that arsenic concentrations vary depending on whether the groundwater is oxidizing or reducing. Under oxidizing conditions arsenic will typically be controlled by sorption to hydrous ferric oxide (HFO) and by the weathering of arsenic occluded within pyrite or true arsenopyrite minerals. Under these conditions typical groundwater concentrations may range from <10 ug/L (Appelo, 2006) to 1,500 ug/L (Vermooten and Gunnink, 2007) depending on pH and bicarbonate concentrations. Near SHL, an EPA well has been found to contain about 400 ug/L in the bedrock which contains arsenopyrite. Other numerous regional studies indicate that concentrations up to 2,000 ug/L in groundwater is possible from bedrock arsenic mineral weathering (Peters and Blum, 2003, Gilpin and Ayotte, 2006, Peters, 2008, Ryan et al., 2011 (in press), Lipfert et al., 2006, and Lipfert et al., 2007).
- Under reducing conditions, dissolution of HFO containing arsenic appears to be the most important control on arsenic concentrations. Ultimately the amount of arsenic found in groundwater in aquifers of this type will depend on the total solid phase arsenic in HFO, the extent of reducing conditions and the amount of dissolved sulfide which can precipitate soluble arsenic as well. Dissolution of HFO containing arsenic can result in ppm (>1,000 ug/L) levels of arsenic in solution (Appelo, 2006). A recent USGS (2011) report for arsenic in wells in bedrock units of central Massachusetts indicates background arsenic concentrations exceeding 1,500 ug/L. Given these fluctuations in background groundwater arsenic concentrations, a determination of the background to be used in the areas outside of the SHL will be based on a monitoring program that is instituted as part of the final remedy, and as agreed upon with USEPA and MassDEP.
- Based on the above, it seems most probable that the arsenic distribution pattern is due to a native source of arsenic in the underlying sands and then infiltration of groundwater with lower arsenic concentrations emanating from and along the bedrock surface. This is similar to distributions speculated by Harding ESE in the 2002 Supplemental Groundwater Investigation.
- Any interpretation should be qualified to recognize that the cap placed on the landfill has and will prevent further meteoric water infiltration which may have altered the original arsenic distribution pattern.

- The effect of the ATP could also be altering the arsenic distribution by pulling in non-impacted water.

#### 6.3.1.2 Geological Transect B-B' and Groundwater Profile Analysis

This transect (**Figure 7**) begins at the south end of the landfill then proceeds east from transect A-A' before again converging at SHM-10-16 to the north and then to the Brook and wetlands (see also **Figure 2**, **Figure 3**, **Figure 7**, **Figure 13**, **Figure 18**, and **Figure 22** for other analytes on this transect). This transect presents the conditions on the eastern side of the landfill in contrast to the A-A' transect. The arsenic concentration is 396 ug/L at SHM-10-11 at the south end of the landfill, and then increases to 1,200 ug/L at SHM-10-07. SHM-10-07 is roughly east of and cross-gradient from the SHM-10-13, SHM-10-14, and SHM-10-15 cluster in the elevated arsenic concentrations. Wells north of SHM-10-07 have lower arsenic concentrations ranging from about 100 ug/L to 700 ug/L. Placing the A-A' transect in context with this transect suggests that arsenic is relatively low at the south end of the landfill (<400 ug/L), increases in the 29X, N-5, SHM-10-14 and 15 cluster (>14,000 ug/L), thins rapidly to the east through SHM-10-13 and SHM-10-07 (<1,200 ug/L) and then proceeds in a somewhat narrow flow path to the north. As with transect A-A', arsenic concentrations are generally higher at depth and the distribution generally follows the bedrock contour. As before, bedrock and till do not appear to be reduced but rather well oxygenated (DO = 5 and 9 mg/L at SHM-10-15 and SHM-10-13, respectively).

#### 6.3.1.3 Geological Transect C-C' / D-D' and Groundwater Profile Analysis

Transect C-C' is at the north end of the site at the Brook/wetlands boundary (**Figure 2**, **Figure 3**, **Figure 8**, **Figure 14**, **Figure 19**, **Figure 23** and **Figure 27**). This transect is located at the edge of the partially observed redox boundary and should be discussed with transect D-D' for clarity. Transect C-C' includes, from east to west, wells SHM-10-18, SHM-10-20, SHM-10-26 and SHM-10-01. Transect D-D' (**Figure 2**, **Figure 3**, **Figure 9**, **Figure 15**, and **Figure 28**) is similar to C-C' but steps slightly south and includes wells, from east to west, SHM-10-27, SHM-10-25, SHM-10-23, SHM-10-24, SHM-10-17, SHM-10-21, and SHM-10-22. The two transects run roughly parallel to each other and allow a comparison of groundwater chemistry at the edge of the wetlands to chemistry further south in the landfill flow path.

In C-C' (from east to west) the arsenic concentration is < 500 ug/L at SHM-10-18 and SHM-10-20 and then decreases to non-detectable at SHM-10-26 and SHM-10-01. Therefore in DPT profiling points immediately on the perimeter of the brook and wetlands, arsenic is quite low, especially to the west of SHM-10-18.

Comparing the C-C' wells to those in D-D' which extends even further east than C-C' it can be seen that arsenic concentrations in wells SHM-10-17, SHM-10-23 and SHM-10-27 is much higher or between 1,000 and 2,000 ug/L. Moving to the west of these points, arsenic again diminishes to less than 400 ug/L. Thus a redox boundary appears to occur to the north and west of the landfill, but not necessarily to the east, although in general the concentrations observed in these northern DPT points are much less than in the landfill.



The other notable characteristic of the transect analysis is that the bedrock surface also appears to control arsenic distribution. As noted in the C-C' transect, the highest arsenic groundwater appears to be flowing through a structural bedrock topographical trough beneath the wetlands. The newest bedrock elevation map (**Figure 29**) from AMEC (December 2010) confirms this structural trough. The bedrock elevation data is discussed further below.

#### 6.3.1.4 Geological Transect E-E' and Groundwater Profile Analysis

Transect E-E' shows the west to east configuration of wells SHM-10-08, SHM-10-02, SHM-10-03, SHM-10-04 on the north side of the Brook. As noted no elevated arsenic occurs on this north side of the Brook (**Figure 3** and **Figure 10**).

#### 6.3.1.5 Geological Transect F-F' and Groundwater Profile Analysis

Transect F-F' is a east to west view from well SHM-10-03 on the north side of the Brook to the wells on the southern edge of the Brook (**Figure 3**, **Figure 11**, **Figure 16**, and **Figure 20**) wells SHM-10-27, SHM-10-25, SHM-10-23, SHM-10-24, SHM-10-17, SHM-10-19 and SHM-10-10. We note that the transect does not consider any arsenic concentrations that might be found east of this transect. Based on **Figure 30**, this transect runs perpendicular to the groundwater contouring pattern. In transect, F-F', arsenic impact to wells on the north side of the Brook (see also E-E') does not occur. On the south side of the Brook, well SHM-10-10 has less than 5-ug/L while SHM-10-17 has soluble arsenic at depth approaching 1,900-ug/L. The transect illustrates the landfill impact up to SHM-10-17 and east, but arsenic diminishes north at SHM-10-18 and west at SHM-10-10. The key to understanding the arsenic distribution in this transect relies on three important considerations: (1) the bedrock contour and resulting groundwater flow direction, (2) the change in arsenic chemistry near the south side of the Brook, and (3) the change in cation/anion chemistry in the wells along the Brook and wetlands. Bedrock contours (AMEC, December 2010) are shown in **Figure 29**. This updated bedrock delineation map (**Figure 29**) assists in explaining the important features for water quality data observed at both the north and south sides of the Brook. The bedrock elevation is at a low in the middle to north end of the landfill (120 to 140 ft msl). Water flow is then confined to a resulting structural trough bounded on the east by increasing bedrock elevation of 140 to 160 msl and to the west by bedrock elevations of 160 msl or higher likely from the Shepley's Hill bedrock surface. Bedrock remains at about 140 msl up to and through the wetlands, but still rises to the east, confining groundwater flow to a north and west direction. At approximately the location of the Brook, bedrock rises again to the north to 140 to 160 ft msl, near the location of the SHM-10-08, SHM-10-02, SHM-10-03 and SHM-10-04 wells. Bedrock slopes to the west to a 120 ft msl contour.

#### 6.3.1.6 Geological Transect Evaluation

The general elevation of the northern most wells indicates that the bedrock surface is about 20 ft higher on the north side of the wetlands (at the location of the wells) and Brook than the southern side which indicates that groundwater flow is counter to flow from the landfill. This groundwater flow from the north provides the redox barrier that both oxidizes and precipitates arsenic at SHM-10-18 as it discharges into/below the wetlands.



The bedrock figure shows that on the north side of the Brook, bedrock slopes downward to the Brook, and to the west. In addition there is another structural trough on the north side of the Brook where water would also enter counter to the flow from the south side of the Brook. Where new data were not available the previous interpretation of the bedrock surface was retained, as is the case with the areas east and west of the geophysical survey transects. It is noted that bedrock outcrops are plotted on the USGS bedrock map to the north of Nonacoicus Brook, just beyond the short segment of 220' contour. Further, the eastern extent of Transect B-B' supports this systematic shallowing of the bedrock surface in a northeasterly direction. These observations preclude the possibility of a deepening trough between the end of Transect B-B' and the mapped outcrops.

The water quality of the wells on the south side of the Brook (i.e. SHM-10-10 and other DPT locations) reveals an impact from water entering counter to the flow from the landfill. It is this water flow (from the north and east) that provides the redox boundary on the south side and west of the Brook. To examine the impact of non-landfill impacted water on water quality at the south side a comparison of well water chemistry from SHM-10-08, SHM-10-02, SHM-10-03, and SHM-10-04 can be made with SHM-10-10 and select DPT points.

Arsenic concentration decreases dramatically to the north of SHM-10-17 (1,800 ug/L) at SHM-10-18 (<400 ug/L) and west at SHM-10-19 (<800 ug/L) and SHM-10-10 (<5 ug/L). The decrease is presumed to be from mixing with water from the north side of the Brook and from the westerly flow of the Brook and wetlands. The zone of mixing is considered the redox zone or boundary, where more non-impacted water mixes with water from the landfill emanating through SHM-10-17 and SHM-10-18 resulting in iron oxidation and adsorption of arsenic. The zone exhibits reduced arsenic by 61% to 83% over a distance of about 20 meters. Arsenic in detectable quantities is therefore unlikely to ever occur in the wetlands or the Brook at this location.

To determine the extent of changes in the water chemistry from intrusion of oxidized, relatively arsenic-free water from the north, simple mixing calculations were performed to determine how much clean water is intruding and creating the redox boundary at the south side of the Brook and wetlands.

Cation and anion chemistry from the landfill may be characterized by SHM-10-14 or SHM-10-15. If this water is mixed with the water from the north side of the landfill, then predicted mixing scenarios are summarized in the following table (Data from sampling of screened wells in September 2010):

The table suggests that mixing ranges from 25 to 75% at the redox boundary depending on the analyte (conservative/non-conservative) used. Regardless of the percent mixing, it is clear that as landfill-impacted groundwater mixes with non-impacted groundwater, clear chemical changes are occurring.

Analyte	Landfill Well SHM-10-14 (mg/L)	Ave of North Side Wells 08,02,03,04 (mg/L)	25:75 Mixing North Side Water/Landfill Water (mg/L)	50:50 Mixing (mg/L)	75:25 Mixing North Side Water/Landfill Water (mg/L)	Water Chemistry at SHM-10-10 (Observed) (mg/L)
Ca	55	170	84	113	141	95
Mg	4	20	8	12	16	14
Na	15	40	21	28	34	26
K	17	5	14	11	8	4
Cl	6	100	30	53	77	20

### 6.3.2 Geochemical Changes Along Flow Path

Other redox sensitive or redox-driven analytes can be compared to the arsenic distribution detailed above in order to illustrate the underlying geochemistry associated with arsenic mobility and fate at the site. This is also illustrated through a series of transects presented in **Figures 6** through **Figure 28**. The transects are discussed per analyte and how each is distributed compared to arsenic.

#### 6.3.2.1 Iron and Manganese

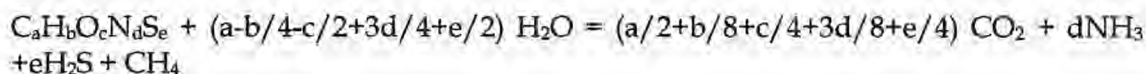
The iron and manganese (**Figures 12** to **Figure 19**) concentrations in the groundwater profiles depicted in each transect are similar to the arsenic distribution (see **Figures 6** through **Figure 11**) described above. In general, iron is found highest at depth (except at the top of the bedrock surface where it is very low (less than 0.5 mg/L)). Additionally, iron and manganese concentrations tend to diminish slightly with distance from the landfill. For example concentrations of dissolved iron range from 44 mg/L to 110 mg/L in the elevated arsenic area and decrease to 30 mg/L at the redox boundary. Manganese decline from north to south does not occur to the same extent as iron. This process has been noted in other landfill induced groundwater regimes presumably due to the ease with which manganese is reduced. Thus manganese will persist until very well oxidized conditions are again encountered.

#### 6.3.2.2 Redox Potential (Eh)

The measured redox potential (Eh) does not always correlate to the presence of redox sensitive species such as iron, manganese, sulfate etc. However at the landfill Eh is a reasonable indicator of conditions where elevated iron, manganese or ammonia should exist and correlates reasonably with where these constituents should be found. The observed Eh does not however identify where the highest concentrations of redox sensitive species exist (see **Figures 21** through **Figure 25**). It should be noted that ORP is not a particularly sensitive parameter. The electrode response to mixed redox couples is unknown. If redox was calculated from known redox chemistry in the borings a different result may have been obtained. As it is, most of the redox measurements appear to be buffered by the Fe (II)/Fe (III) couple and possibly the sulfate/sulfide couple.

### 6.3.2.3 Carbon Degradation

Carbon degradation species (ammonia, DOC, alkalinity). The distribution of carbon related species requires some background information as to their geochemical formation. Under anaerobic conditions such as observed at the landfill, carbon bearing molecules degrade in a very general sense via:



This degradation scheme serves to show that under anaerobic conditions, ammonia, carbon dioxide and methane are produced, all detectable at the landfill. Further reactions proceed including:

- Carbonic acid formation:  $CO_2 + H_2O = H_2CO_3^* = H^+ + HCO_3^-$
- Metal sulfide precipitation:  $H_2S = 2H^+ + S^{2-} = (Metal)S_{(solid)}$

These reactions result in the overall addition of the following analytes to landfill leachate and groundwater:

- Soluble species = residual carbon (DOC), bicarbonate, ammonium, and some sulfide
- Gaseous species = methane, carbon dioxide, and ammonia

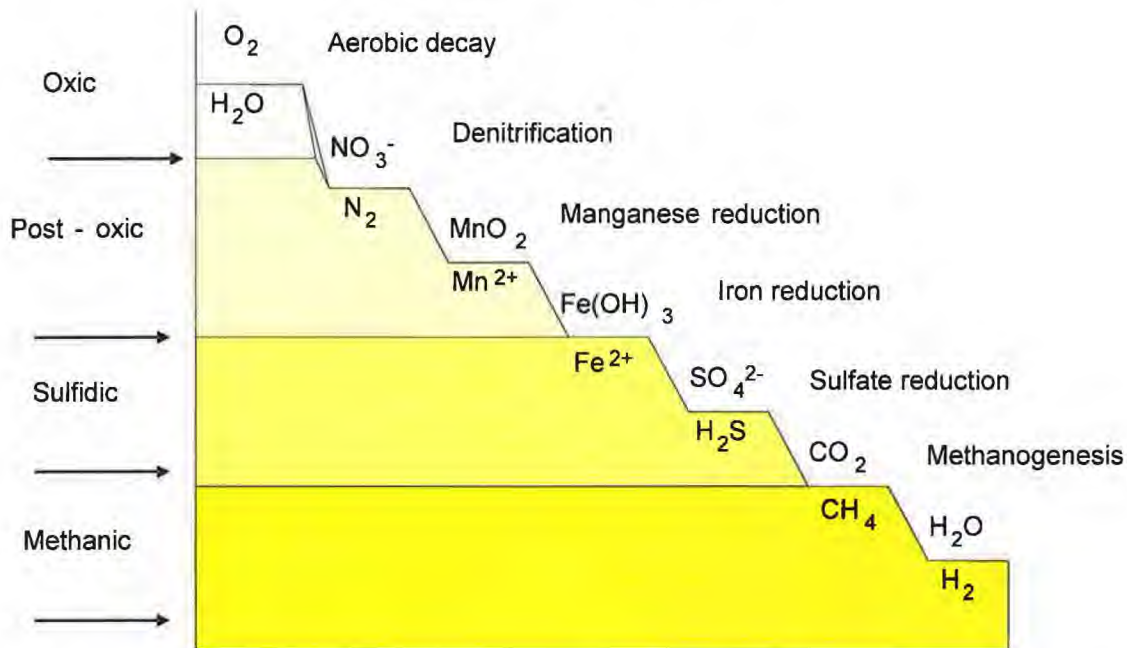
This overall reaction scheme is similar to the individual reaction examples listed below which occur as oxygen is consumed in an organic rich environment such as the peat and landfill waste. The reactions that occur as redox becomes more negative are illustrated below.

Reducing Stage: from oxidizing to more reducing	Chemical Reactions
Aerobic Respiration	$CH_2O + O_2 \rightarrow CO_2 + H_2O$
Denitrification	$5CH_2O + 4NO_3^- + 4H^+ \rightarrow 5CO_2 + 2N_2 + 7H_2O$
Manganic Reduction	$CH_2O + 2MnO_2 + 4H^+ \rightarrow CO_2 + 2Mn^{2+} + 3H_2O$
Ferric Reduction	$CH_2O + 4Fe(OH)_3 + 8H^+ \rightarrow CO_2 + 4Fe^{2+} + 11H_2O$
Sulphatic Reduction	$2CH_2O + SO_4^{2-} + H^+ \rightarrow 2CO_2 + HS^- + 2H_2O$

Based on the landfill geochemistry the redox ladder presented below illustrates where the landfill and underlying groundwater are presently poised and the order with which reactions have occurred.



## The Redox ladder



Based on these basic principles and comparing them to the chemistry observed at the site, several observations regarding redox species in the landfill and north of the landfill are presented below:

- The landfill is highly reducing and methanogenic. Methane production is widespread in the landfill. Ammonia is present throughout groundwater sampled from the landfill wells and to the north indicating the influence of the landfill and the strongly reducing conditions. Ammonia and alkalinity are good indicators of the extent of landfill-reducing conditions throughout the area.
- The transects show elevated DOC (**Figure 26** through **Figure 28**) that does not necessarily parallel the other redox sensitive species. This may be due to the microbial conversion of groundwater carbon to other species such as methane or carbon dioxide. The DOC may also act as an on-going source of reducing conditions. This is addressed in the next **Section 6.3.3**. Both transect and profile data for the various wells show elevated bicarbonate concentrations due to carbon dioxide production. These concentrations are highest in the center of the landfill and lower on the perimeter of the landfill.
- Bicarbonate is a good indicator of landfill influence and extent of intrusion into local groundwater. As explained earlier and in the redox diagrams, anaerobic biodegradation produces carbon dioxide which in turn dissolves in water and forms bicarbonate (and carbonate if pH is high enough). The high bicarbonate water produced from the landfill waste (and peat) intrudes upon native groundwater and changes the water quality from calcium chloride type water to calcium-iron-bicarbonate type water. This process is



described in a series of figures (**Figures 34 to Figure 40**) that show groundwater quality changes from the south of the landfill to the north of the landfill, discussed below.

To illustrate the use of bicarbonate as an indicator of landfill influence, the changes in bicarbonate concentrations are shown along a group of wells within the landfill and outside of the landfill. The well locations start in the south landfill at SHM-10-11 then to SHM-10-12 to SHM-10-13 with a cluster of wells in the center at SHM-10-15 and SHM-10-14 then north out of the landfill to SHM-10-16 and further north to SHM-10-04 across the Brook (**Figures 34 to Figure 40**). In **Figure 35**, the cation and anion balance is shown for SHM-10-11 that is illustrative of a partially landfill impacted groundwater. (i.e., shows chemical characteristics of landfill leachate such as elevated bicarbonate). At this location bicarbonate is the dominant anion (due to carbon dioxide production during carbon degradation) but measurable amounts of both chloride and sulfate are still found. This may be compared to groundwater sampled from SHM-10-04 (**Figure 34**) which is north of the landfill and across the Brook and wetlands and is thought to represent local, non-landfill (or peat) impacted groundwater. As noted anion chemistry in this well is nearly equally distributed among bicarbonate, sulfate and chloride. Thus the landfill/peat will enrich local groundwater in bicarbonate compared to other anions.

The bicarbonate enrichment expected from landfill carbon degradation processes is seen in the wells in the center of the landfill for SHM-10-12, SHM-10-13, SHM-10-14, and SHM-10-15 (**Figure 36 through Figure 39**). In these wells, bicarbonate is clearly the dominant anion with only small amounts of chloride and no detectable sulfate (due to sulfate reduction). This anion distribution is characteristic of the landfill influence. Moving north to SHM-10-16 outside of the landfill (**Figure 40**), bicarbonate still dominates, but chloride has increased and small amounts of sulfate are also noted, indicating some mixing with other groundwater or surface water recharge.

### 6.3.3 Summary of Arsenic Fate and Transport in Landfill and North Impact Area from Transect Analysis

This section summarizes the data collected for the north impacted area.

#### 6.3.3.1 Fate of Arsenic and Carbon in Landfill and North Area

The geochemical analysis of groundwater profile and transect data are summarized as follows:

- Arsenic concentrations are found to be highest beneath the area roughly defined by N-5, SHL-99-29X, SHM-10-12, SHM-10-14 and SHM-10-15. Observed arsenic concentrations range from 1,000-ug/L to about 17,000-ug/L.
- Sampling of groundwater from monitoring wells to the north of the landfill including SHM-10-16, SHM-10-17, SHM-10-18 and SHM-10-10 reveal that arsenic concentrations are diminished compared to the landfill concentrations. Arsenic in the wells ranges from <5-ug/L (SHM-10-10) to about 1,900-ug/L (SHM-10-17) indicating a gradual but identifiable decrease in arsenic with distance from the landfill.

- Monitoring well water chemistry from the east side of the landfill also shows that arsenic decreases in this direction. Wells SHM-10-06A and SHM-10-07 on the east side of the landfill have arsenic ranging from <200 ug/L to about 1,400 ug/L.
- The transect analysis illustrates that the arsenic concentrations usually increase with depth from the groundwater surface. There is, however, a noticeable and measureable change in arsenic and dissolved oxygen just above the till and bedrock surface. Here dissolved oxygen is high (up to 9 mg/L DO) and arsenic <300 to 400 ug/L.
- These transects clearly delineate the extent of arsenic with depth, within the landfill and to the north at the Brook/wetlands.
- The other redox sensitive analytes, iron and manganese, and the carbon degradation related analytes (especially bicarbonate) also define the extent to which degradation of landfill waste and peat have impacted native groundwater. Aside from manganese and possibly dissolved organic carbon (DOC), the redox species generally mirror the distribution of arsenic.
- The resulting picture from the transect analysis demonstrates that landfill waste and peat degradation have caused reducing conditions which in turn have mobilized arsenic through reduction of iron (III) solids and subsequent release of arsenic. The main area of arsenic mobilization is directly below the landfill in the area where the former wetlands were found underlain with peat. The organic carbon degradation here has resulted in a predictable series of redox changes identified through methane, carbon dioxide and ammonia production. These analytes are found throughout the flow paths examined. These analytes are found in diminishing concentrations as the north end of the site is encountered at the Brook and wetlands presumably due to intrusion of clean non-landfill impacted groundwater and groundwater recharge.

#### 6.3.3.2 Summary of Redox Boundary Data in North Area

In this document, the term "redox boundary" is used to define significant and measureable changes in groundwater geochemistry that occur at the edges of the landfill impacted groundwater. These changes may occur for several reasons:

- Flow of landfill-impacted water that intrudes into non-impacted groundwater downgradient of the landfill (i.e. the downgradient extent of the impacted groundwater migration)
- Mixing of landfill-impacted water with non-impacted water beneath the Brook and wetlands, and
- Dilution of landfill impacted water by infiltrating non-impacted water along the sides of the plume outside of the landfill footprint where infiltrating meteoric water is not restricted due to capping.

The redox boundary has been roughly defined by Transects C-C', D-D', E-E', and F-F'. The extent and significance of the redox boundary can be described as follows:

- The general elevation of the northern most wells indicates that the bedrock surface is about 20 ft higher on the north side of the wetlands (at the location of the wells) and Brook than the southern side which indicates that groundwater flow is likely in the opposite direction to flow from the landfill. This provides a redox boundary due to the generally better water quality from the north compared to that emanating from the landfill.
- The bedrock contours also show that on the north side of the Brook, bedrock slopes downward to the Brook, and to the west. In addition there is another structural trough on the north side of the Brook where water would also enter in the opposite direction to the flow from the south side of the Brook. This counter flow should also create an effective redox boundary.
- The groundwater on the north side of the brook that is intruding, diluting or mixing into the landfill impacted water on the south side of the brook contains on average 40 mg/L of sodium. The wells in the landfill contain on average 15 mg/L of sodium. This is due to the intrusion of the iron-bicarbonate water created from the landfill carbon degradation process and subsequent replacement of calcium and sodium in the native groundwater. The wells at the north end of the impacted area at the south side of the Brook and wetlands contain on average 15 mg/L of sodium. This indicates that mixing of water from the north side of the Brook which is high in sodium is occurring. Using a simple mixing model, approximately 50% mixing between the two waters has occurred. This same analysis can be done with calcium, bicarbonate, sulfate or chloride with similar results. Some analyses suggest up to 75% mixing with water from the north.
- The subsequent mixing with this water diminishes arsenic to low levels. Mixing also results in redox changes that will oxidize iron (II) to iron (III) with subsequent adsorption of soluble arsenic. This redox boundary has been clearly delineated to the west of SHM-10-17 near DEP-08-03 and to the north at SHM-10-18. To the west SHM-10-19 and SHM-10-10 show marked decreases in Eh, DO, iron and arsenic and to the north SHM-10-18 shows only 17% (300 ug/L) of the arsenic encountered at SHM-10-17 (1,800 ug/L). This reduction is consistent with the change in sodium, chloride and other general chemistry parameters found at SHM-10-18 or SHM-10-10 which indicate mixing with non-impacted water. To the east, the redox boundary was not as clearly defined since access was not obtained for several key locations. However, based on earlier DPT work to the east, the extent of landfill intrusion into the Brook/wetlands may not occur past SHX-01-14X.
- Due to the observed geochemical changes in some parts of the north end, arsenic exceeding 400-ug/L will likely not enter the wetlands/Brook underflow. Since rapid oxidation is expected in the wetlands, detectable arsenic entering the base-flow is unlikely.
- Since the data was collected at the lowest flow stage of the wetlands and Brook it is expected that during other flow stages the impact from the landfill will be even less as the percentage of mixing and oxidation will increase as peak flows are approached.
- The redox boundary can be better identified using a groundwater monitoring network established from the well water chemistry completed in this SAR. Wells placed to the



north of the landfill, to the west along the brook and east along the brook can, over time allow changes in arsenic geochemistry to be observed along the groundwater flow path in this area of the site which can be used to refine the redox boundary observations

- The existing data support the conceptual model of arsenic laden groundwater migrating along and above the bedrock surface at depth through the documented bedrock topographic trough that proceeds north from the landfill and turns westward along Nonacoicus Brook. Based on the depth of impacts and as depicted on the Transects, arsenic laden groundwater does not appear to discharge to the brook or wetlands as the arsenic impacts are located deeper than the brook and wetlands.

### 6.3.4 Column Results and Modeling of Monitoring Natural Attenuation

#### 6.3.4.1 Column Results

The first column study was designed to address the question of how long would it take for the landfill aquifer to recover to pre-landfill conditions if un-impacted oxidized water were to enter and flush the arsenic and carbon out of the column pore water.

The data for the initial column flushing study is presented in Prima Environmental: Report of Findings, Shepley's Hill Landfill 2011 (**Attachment I**). As noted from the data the column is washed free of arsenic (to less than 5 ug/L) in 8 to 9 pore volumes in one column and 13 pore volumes in the column duplicate (**Figure 41**). **Figure 42** and **Figure 43**, show that while arsenic diminished rapidly, the column is still maintaining reducing conditions ( $Eh < -25$  mv) and carbon is still elevated at 3 mg/L.

Using the initial arsenic flushing rate from this study an estimate of the time it takes for the aquifer to be flushed free of arsenic can be made. Since the groundwater velocity ranged from approximately 0.5 to 1 ft/day and the migration of 1 pore volume of groundwater through the landfill would take approximately 13.5 years, then 13 pore volumes represents about 176 years of flushing and roughly 269 years to the brook at an initial arsenic concentration of 1,200 ug/L.

The above example can be considered a best case scenario since the column effluent was still reducing at the end of the study, containing roughly half the dissolved organic carbon (about 3 mg/L) indicating reducing conditions will persist beyond the initial flushing of the pore water entrained arsenic.

In a second column study a different scenario was tested. The details included:

- Flushing of a section of core containing high solid phase arsenic (35 mg/kg) with oxidized water to remove all pore water arsenic (initial concentration 1,450 ug/L).
- Once the core was flushed free of soluble arsenic, introduce reduced water and flush at a slow rate (1 pore volume per 4 days or less than 0.5 ft/day)
- Examine effluent to determine how fast arsenic is re-released from the remaining solid phase pool (presumably HFO and other solids)



This test is especially relevant since several proposed remedial strategies focus on removing arsenic from groundwater while allowing reducing conditions to persist. Therefore the test simulates the potential for re-release of arsenic from aquifer solids downgradient either from the ATP or a reactive barrier. Under both situations arsenic will be removed allowing for the pore water arsenic to decrease, but reducing conditions will still prevail.

The results from the study are summarized as follows:

- Influent water: Bicarbonate alkalinity = 210 mg/L, Arsenic (total dissolved) < 5 ug/L, Calcium = 92 mg/L, Cl = 12 mg/L, DOC = 62 mg/L, Mg = 9 mg/L, K = 42 mg/L, Fe (II) < 0.01 mg/L, Na = 75 mg/L, DO = 2 mg/L, pH = 6.8.
- Arsenic in column 1 (experiment was duplicated) began at <5 ug/L. After 12 pore volumes arsenic in the column 1 effluent was 210 ug/L. In column 2, arsenic was 190 ug/L after 9 pore volumes (See **Figure 1**).
- The arsenic in the effluent in both columns was low (<70 ug/L) through the first 9 pore volumes extracted at a rate of 0.5 ft/day.
- At pore volumes 10 and 11, arsenic began to increase presumably due to dissolution of HFO in the sands.
- The slow dissolution pattern suggest that HFO dissolution and arsenic release is initially rate limited and will take time before significant amounts of arsenic are released to solution. After 15 weeks arsenic appeared to level off between 300 and 400 ug/L.

#### 6.3.4.2 Geochemical Modeling and Mixing

The data from the above flushing exercise was modeled with PHREEQC2 which is a US Geological Survey computer code that can be used for modeling column data and other water quality exercises. The model parameters were used to address the time of flushing for the center of the landfill where arsenic concentrations approach 15,000-ug/L. The results are shown also in **Figure 44**. As noted, arsenic rapidly diminishes in the first few pore volumes and then diminishes to about 200-ug/L at 12 to 14 pore volumes. Thus flushing the center of the plume may take approximately 50 to 100 years longer than found in the moderate arsenic column flushing data.

Another geochemical exercise was conducted. The purpose of this exercise was to determine (1) the primary solid phase controlling arsenic solubility, and (2) determine the distribution coefficient of arsenic per a site specific analysis. These are needed to understand what the primary source of arsenic is in groundwater and what concentrations can be expected in groundwater based on the presence of the source. In the first case, it is assumed that iron solids control arsenic solubility by adsorption of arsenic onto the surface of amorphous hydrous ferric oxide (HFO) or ferrihydrite. This assumption has been based on previous site work and literature that demonstrates the control that HFO has on arsenic solubility and mobilization under reducing conditions. While this control on arsenic solubility is probable in the Shepley's Hill Landfill, there may also be other controls on arsenic solubility such as oxidation of arsenopyrite in bedrock and till and dissolution of pyrites or sulfides containing arsenic. Recent

mineralogical investigation of some of the core samples has been examined by RJ Lee Group (**Attachment L**, Mineralogy and SEM Results). It was noted that in-situ formed framboidal pyrites were prevalent in many of the samples even in some of the waste. Thus there is at least some evidence that other iron minerals may be present. Due to this, if all solid phase iron and arsenic concentrations in the soil/aquifer solids from the borings is examined by plotting Fe versus As there should be considerable variability as noted in **Figure 45**. This suggests that iron solids (as HFO) contain different amounts of arsenic and/or there are several sinks for iron which can alter the arsenic to iron ratio expected from arsenic in HFO alone.

Since water samples were collected every 10 ft, it was possible to assign an aqueous arsenic value at the same depth where the solid arsenic content was measured in all the boring samples. By plotting the aqueous phase arsenic against the solid phase it would be possible to define a site specific distribution coefficient or Kd for arsenic. Since Kd:

$$\text{Arsenic (solid)} = \text{Kd} * \text{Arsenic (solution)}$$
$$\text{Kd} = \text{Arsenic (solid phase)} / \text{Arsenic (solution phase)} - \text{liters/kilogram}$$

This exercise was carried out and plotted in **Figure 46**. The plot is generally linear with a Kd (slope) of 7.62 and an R squared of 0.76. Since the plot is generally linear and the parameters well correlated a site specific Kd of 7.62 can be used in subsequent geochemical analyses. Care should be exercised in the use of the Kd since the correlation is dominated the cluster of samples at the low end of the plot. This site specific Kd, which covers a large range of concentrations, may also be in fact a series of 2 or more slightly different plots or lines representing different mechanisms of arsenic retention.

#### 6.4 Reducing Conditions in Landfill

One of the most difficult processes to quantify at the landfill is the source strength. Source strength is defined as the mass of potentially reactive arsenic emanating from the landfill or the aquifer minerals or both. Landfills are notoriously difficult to characterize due to severe variability in types of material disposed and irregular placement of refuse. In the case of Shepley's Hill Landfill, this is made more difficult due to the relatively new cap placed over the landfill. The cap alters the original delivery of arsenic and carbon to the underlying groundwater by cutting off the infiltration of meteoric water and results in a new or different distribution of arsenic and carbon in the groundwater. Due to these complications it is not likely that the landfill can be characterized vertically and aurally with any degree of confidence. As such, the borings completed in the landfill were advanced in several distinct locations based on previous site investigations that would yield important information about the potential arsenic contents within the landfill and also the carbon distribution at key locations within the landfill. Waste characteristics within the landfill borings is described first followed by a discussion of the carbon as a source of reducing conditions.

#### 6.4.1 Waste Distribution and Characterization

Waste was encountered in all of the borings advanced in the landfill, with the exception of SHM-10-13. Here a layer of ash and sand from approximately 6 feet to 10 feet below grade and again at approximately 22 to 24 feet (mixed with sand) below grade was encountered overlying a large thick section of peat. **Table 7** summarizes the occurrence of waste and the type of waste and the major trace element analyses encountered.

The table illustrates that the waste metal content is highly variable but with the exception of a few samples not necessarily enriched in metals with respect to normal soil background ranges (see yellow highlighted values which represent enriched samples). The shaded values represent enrichment with respect to normal soil ranges. As noted, lead appears to be enriched most commonly in the waste samples, a not unexpected result given the composition of municipal waste. Arsenic in the waste varies from 0.8 to 60 mg/kg with the highest contents found in a single ash sample and in peat. The distribution of important trace elements in the waste and underlying sands are shown (and discussed) in the following soil boring profiles.

**Figure 47** displays the trace metal content of the SHM-10-11 landfill boring strata. Several important observations can be derived. First, there are 4 distinct zones in the profile. The first zone is a layer of waste of mainly paper, plastic, and some metal scraps that occurs to about 12 ft bgs. This zone is elevated in lead, zinc, and copper. The second zone occurs below the first and also includes paper waste but wood fragments as well (13-23 feet). The waste in this zone is mainly chromium, copper and zinc enriched and at levels lower than the first zone. The third zone (24 to 60 feet) is the underlying aquifer sand that has very low (less than 20 mg/kg) metal contents. Finally, at the bottom of the boring (> 60-feet) glacial till and weathered bedrock is encountered from 55 to 70 ft. Here chromium, zinc, nickel and lead increase again due to the native mineralization of the bedrock and till in the area.

Another observation from the profile is the sharp break in concentration of metals from the waste layers to the underlying sands. There is no gradual decrease in metals with depth suggesting that enrichment of the underlying solids from waste leaching has not occurred. As noted previously this is similar to the distribution of arsenic and metals at the Winthrop landfill where waste is not considered a source of arsenic or metals to underlying groundwater (Keimowitz et al. 2005).

**Figure 48** shows the same trend for boring SHM-10-12. A simpler trend is observed in this profile, with only the upper waste enriched in lead, copper and zinc (10-feet) and lower strata (10 to 60 feet) showing no significant variation in trace metal content. Again the sharp break in concentration is observed.

**Figure 49** shows the profile for SHM-10-13. This profile also has 4 distinct zones. Waste occurs to approximately 25 to 30 feet bgs which is elevated in lead, chromium, and copper. Below this waste, sand is encountered with no obvious elevated metals, and just underlying the first sand zone is another sand layer with elevated nickel, chromium, and copper (40-45 feet). The reason for the elevated metals in this part of the profile is not fully known. Sands



occurring from 50 to 70 ft are relatively low in metals concentrations (<20 mg/kg) until till is encountered and metals (lead, copper, and arsenic) increase as noted earlier.

**Figure 50** is the metal profile for SHM-10-14. This profile shows a waste zone occurring to about 25 feet bgs followed by a thin clean sand layer and then a 14 ft thick layer of peat. The waste contains some lead and zinc while the peat is slightly elevated in arsenic and zinc. Below the peat layer is low metal containing sand from 44 to 60 ft bgs. At 60 ft till and weathered bedrock are encountered which explains the increase in arsenic and zinc from 70 to 83 ft.

**Figure 51** is the final profile for landfill boring SHM-10-15. The profile shows elevated lead, zinc, and copper in the waste layer (5-25 feet) and as observed in the other borings, relatively clean sand followed by increases in metals at the till/bedrock interface.

**Figure 52 and Figure 54** display the carbon and arsenic contents of the aquifer solids from three of the landfill borings. Initial analysis of the data suggests little correlation between TOC and arsenic. Unlike arsenic distribution, TOC outlines the waste and peat profiles very well and the decreases, presumably to background with depth. In all cases TOC decreases rapidly below the waste and or peat layer.

A summary of the waste characteristics and depth profiling shows that:

- Most trace metals are confined to the upper part of the profile defined by the landfill waste boundary. No enrichment of underlying sands has been found indicating leaching has not resulted in measurable changes to the solid phase metal content in the aquifer.
- Most of the waste is enriched in metals typically found in municipal landfill: lead, copper, zinc, chromium, and nickel.
- Arsenic in waste samples was found to be 31 mg/kg. Only in the peat underlying SHM-10-14 did arsenic reach levels approaching 60 mg/kg.
- Two borings appeared to have waste and or peat in contact with groundwater. These were borings SHM-10-14 and SHM-10-15.
- The effect of the cap will likely have a great effect on preventing possible migration of metals from the waste into groundwater. Future analysis of wells should reveal marked declines in any soluble metals such as nickel and zinc.

#### 6.4.2 Landfill and Peat / Wetlands as Arsenic and Carbon Source

This section discusses the relative importance of the landfill waste and peat as sources of arsenic and carbon.

#### 6.4.2.1 Geochemical Analysis: Arsenic Source

Additional calculations were made using the arsenic contents from the waste and underlying sands to determine the relative importance of waste or aquifer sands as a source of arsenic to groundwater. This was attempted by calculating the relative mass of arsenic in waste and the mass of arsenic in aquifer sands. The results are summarized as follows:

Material	Average As Content (mg/kg)	Depth of Material (ft)	Arsenic Inventory in Landfill Due to Waste or Sand (kg) assumes 90 acre landfill and Bulk Density of 1.6
Waste	10.9	23.2	27,598 kg
Sand	14.2	35.6	68,710 kg

The table shows that the aquifer sands had a slightly higher average arsenic content compared to waste (14.2 mg/kg compared to 10.9 mg/kg). The depth of waste versus aquifer sands was obtained from the boring logs and collection of samples from each stratum at borings SHM-10-11, SHM-10-12, SHM-10 SHM-10-13, SHM-10-14, and SHM-10-15. While the waste was considered to be 23 ft deep on average, most of the waste was bisected by sand layers or daily cover. A correction of 4 ft of sand cover per 20 ft of waste was made. The calculations indicate that the aquifer sand contains about 2.5x the amount of arsenic as the waste, confirming the significance of this (aquifer sand) source to the overall groundwater quality.

The data show on a mass basis there is more arsenic inventory in the underlying aquifer sands than in the waste. Hence as an on-going source of arsenic, the aquifer sand is a more important source. On a mass basis the waste contains about 27,600 kg of arsenic compared to 68,800 kg in the aquifer sand. If the amount of saturated waste is further taken into account, only 7,000 kg of arsenic in the waste is possibly in contact with groundwater. It is not known with certainty how much if any waste based arsenic has leached into the groundwater, this calculation simply describes the condition of the landfill as it now occurs. Capping and pumping have likely altered the distribution of arsenic from the previous uncapped condition.

Early reports by Harding ESE, AMEC and Gannett Fleming and more recently by Sovereign have revealed: (1) the primary source of arsenic now mobilized in groundwater originates from the aquifer sands. Other sources such as landfill waste and bedrock may contribute to dissolved arsenic but are not the primary source. Aquifer sands are rich in hydrous ferric oxide (HFO) which hosts surface adsorbed arsenic; (2) arsenic solubility is controlled by reducing conditions imposed by both landfill waste and pre-existing peat deposits within the wetlands over which waste was emplaced; (3) reducing (and anaerobic) conditions force reduction of Fe (III) to Fe (II) resulting in dissolution of HFO and concurrent release of sorbed arsenic; (4) This process has resulted in arsenic concentrations in groundwater that range up to 16,000 ug/L. The importance of HFO in controlling arsenic solubility is a widely accepted process and has been demonstrated to occur at other landfills.

Another evaluation of the waste and aquifer sand is presented. Reported here are the results of the Sequential Extraction which have been used to determine how much arsenic could be potentially released and leached into groundwater from the different potential source samples. The Table below describes the results received to date.

Sample ID		Arsenic in Sample (Total) (mg/kg)	Arsenic in Phosphate Extract (mg/L)	Potential Leachable Arsenic (ug/L)
SHM-10-12	Waste at 5-ft	12	0.14	140
	Sand at 42-ft	29	0.39	390
	Sand at 65-ft	34	0.48	480
SHM-10-13	Waste at 23-ft	31	0.51	510
	Sand at 83-ft	23	0.39	390
SHM-10-14	Waste at 10-ft	18	0.28	280
	Waste at 15-ft	12	0.08	8
	Waste at 20-ft	18	0.21	21
	Waste at 27-ft	3.8	< 0.052	< 52
	Sand at 70-ft	35	0.55	550
	Sand at 75-ft	51	1.24	1,240
SHM-10-15	Waste at 18-ft	25	0.083	83
Method Blank		NA	< 0.052	< 52

Preliminary analysis reveals that waste samples potentially could leach from <53 ug/L arsenic to 510 ug/L arsenic. The underlying aquifer sands by comparison could leach up to 1,240 ug/L. This leachable quantity is not however an indication of the amount of arsenic that could be released in the sand samples by reducing conditions. For example if all of the arsenic entrained in the iron solids on the sand grains was released, then concentrations of 30,000-ug/L or higher could be found in solution (i.e., 15-mg As/g sand dissolving into 0.5-mL of pore water). This range of concentration has been reported in SHM-10-14. This simple analysis suggests again that the waste, like the bedrock, is not the most significant source of arsenic to the underlying groundwater under reducing conditions. The sands rich in surface precipitated iron and arsenic are the main source of arsenic. The cap will prevent further migration of potentially soluble arsenic from the landfill waste to the underlying soils in most locations.

#### 6.4.2.2 Landfill and Peat / Wetlands as Carbon Source

For evaluating reducing conditions or carbon source strength, a well by well comparison was completed in order to assess the relative contributions of landfill waste to peat as a source of reducing conditions. From the previous discussion, reducing conditions evolve from a set of geochemical reactions that begin when carbon degradation utilizes, then expends all available oxygen. At this point other oxygen sources such as nitrate and sulfate are utilized that further drive the redox potential down (more negative). Once these are expended, anaerobic metabolism proceeds and carbon dioxide, methane and ammonia are produced. A simple way to assess the relative "reducing strength" of the landfill waste and peat is to examine the total carbon produced by the geochemical conditions within the landfill waste or peat. To do this the following protocol was used:



- The landfill borings recently completed were segregated by whether waste or peat or both were encountered in the borings. This led to the following classes:
  - SHM-10-13 contains almost **exclusively peat**, with only a trace of ash well above the water table. No other organic waste was found in the boring;
  - SHM-10-14 contains **peat and waste**;
  - SHM-10-15 and SHM-10-12 **contain waste** but no peat.
- The carbon balance encountered in the well water at each of these locations was examined to determine which location contributed more carbon to the system.
- The analysis provides a limited but useful comparison of peat vs. waste vs. peat plus waste as far as carbon and reducing conditions are concerned.

The analysis yielded the following results:

Location	DIC (mg/l)	DOC (mg/l)	Total Carbon Input (DIC + DOC)
SHM-10-11 (waste)	62	3.3	65.5
SHM-10-12 (ash/waste)	110	4.1	114.1
SHM-10-13 (peat)	140	5.6	145.6
SHM-10-14 (peat/waste)	120	8.7	128.7
SHM-10-15 (waste)	82	4	86

The results show that the two wells drilled into the peat, SHM-10-13 and SHM-10-14 have the greatest carbon input of 129 and 146 mg/L, respectively. The two wells drilled into waste only, SHM-10-15 and SHM-10-11 have the lowest carbon input of 65.5 and 86 mg/L, respectively. The boring through the ash layer is intermediate with 114 mg/L of total carbon.

This limited analysis suggests that the peat layer, with or without waste above it supplies more carbon input to the groundwater than ash or waste alone by almost a factor of two. This also suggests that the peat layer and associated wetlands have been acting as a carbon source long before the landfill existed. This carbon source resulted from and contributes to locally reducing conditions that would have mobilized arsenic long before the existence of the landfill. The landfill impact to reducing conditions has no doubt decreased through time due in part to exhaustion of easily degradable carbon sources and to the placement off the cap on the landfill. Thus this analysis can only be valid for the present time. The exercise conducted above is substantiated by the scientific literature. The emplacement of landfill waste clearly has created its own carbon metabolism, degradation and anaerobic reducing conditions. Municipal landfills are known to behave in this manner and there is no dispute that the landfill comes with its own set of impacts to underlying groundwater. SHL is considered an older landfill (>20 years). By literature standards (El Fadel et al., 2001) leachate from these landfills have lower COD (<1,000 mg/L), BOD (<50 mg/L), ammonia (<30 mg/L), TDS (<1,000 mg/L) and other constituents compared to newer landfills. SHL groundwater falls within these ranges even with dilution considered. Since SHL has been capped, most of the waste (89 %) is no longer in contact with

groundwater. Over time, the landfill's role in maintaining reducing conditions will diminish and cease.

The wetlands and peat appear, from historic USGS maps, to encompass about 70% of the northern half of the landfill and possibly half of the southern part of the landfill. These wetland areas formed shortly after or during the retreat of glaciers during the last Ice Age and typically date 13,000 yrs before present (BP). Formation of wetlands, and underlying peat, results in a number of important biogeochemical changes (Mitsch and Gosselink, 2007):

- Inundation of water into the surface soils in the wetlands results in anaerobic conditions. Low diffusion rates of oxygen under saturated conditions will result in anaerobic conditions typically within 12 weeks.
- Lack of oxygen leads to nitrate reduction, then iron reduction and sulfate reduction, and finally methanogenesis.

These biogeochemical changes will result in production of soluble iron as Fe (II), hydrogen sulfide which can off-gas and/or precipitate as a metal sulfide, production of ammonia and methane. Measured methane rates (Mitsch and Wu, 1995) have been found to range from 0.1 to 500 mg C m<sup>-2</sup> d<sup>-1</sup>. Global carbon emission rates from methane from peat are 150 mg C m<sup>-2</sup> d<sup>-1</sup> (Matthews and Fung, 1987).

Literature reviews and textbooks on wetlands and peat make it abundantly clear that the formation and maintenance of wetland and peat always result in anaerobic conditions and resulting biogeochemical conditions that will mobilize arsenic as explained in the SAR. To illustrate this we point to a paper (Ravenscroft et al., 2001) in which peat occurs extensively beneath arsenic affected areas of southwestern Bangladesh. The peat is thought to be Holocene aged, about 5,000 yr BP. In wells where peat was not encountered arsenic levels rarely exceeded 100 ug/L. In wells drilled through peat deposits, arsenic concentrations increased to over 1,000 ug/L. It is important to note that peat was encountered at various depths up to 60 meters below ground surface. The findings can be summarized as follows: The concentration of arsenic was not exceptional in much of the study area and the occurrence of reducing conditions was not enough to explain the degree and extent of arsenic pollution. High arsenic levels were attributed to biodegradation of buried peat deposits which drives the reductive dissolution of FeOOH supplying high amounts of arsenic to groundwater. The correlation of peat deposits to high arsenic has also been noted by others (Smedley and Kinniburgh, 2002). Arsenic mobilization by peat is also described by Bauer et al., (2008), Rothwell et al., (2008), in wetlands by Kalbitz and Wennrich (1997) and in an urban pond by Durant et al. (2004). The importance of peat and wetlands in mobilizing arsenic due to carbon and reducing conditions is well established.

The fact that wetlands and peat underlie a significant portion of the landfill can only mean that additional sources of carbon and arsenic were introduced to an already dynamic anaerobic system via the landfill emplacement. Estimates of dissolved carbon from either landfill or wetland sources as noted in the SAR suggests that peat and wetlands have increased total carbon by 50 to 75% of that delivered by the landfill suggesting that removal of the landfill would only reduce the carbon input by 25 to 50%. Thus the peat and wetland areas are a major

source of carbon and reducing conditions. With the landfill aging, the peat and buried wetlands will continue to act as a carbon source and hence maintain reducing conditions into the future. Additional information on the role of peat as a carbon source and its use as an analogue for the long-term behavior of landfills can be found in a review paper by Bozkurt et al., (2001).

#### 6.4.2.3 Bench Scale / Column Testing

As noted previously freezing of the soils may have negatively impacted the microbial populations and prevented degradation from occurring to a measurable degree. This study has, unfortunately, been discontinued.

#### 6.4.3 Duration of Reducing Conditions

To date only estimates of the life cycle of reducing conditions can be made. Carbon will persist in the aquifer due to 3 types of carbon processes. The first is the degradation rate of the peat or waste alone. Coupled with this is the fact that the cap may provide a barrier to water infiltration effectively ending the delivery of carbon from much of the waste. This seems to be true in the southern half of the landfill where the waste is 10 to 15 feet above the water table such as at SHM-10-11 and SHM-10-12. At SHM-10-14 and SHM-10-15 peat and some waste are still in contact with groundwater. The release rates of carbon are being studied in the laboratory (results pending).

The second carbon source is the persistent TOC measured in the aquifer sand solid phase that likely migrated geologically from the peat into the underlying sand. Concentrations up to 4% TOC have been found in the center of the landfill around borings SHM-10-13, SHM-10-14 and SHM-10-15 at depth of 45 ft or more, although 0.1 to 0.5% TOC are more common. This carbon will slowly biodegrade (via an anaerobic pathway) and maintain reducing conditions.

The last type of carbon to consider is the dissolved organic carbon (DOC) that is still persistent in all the wells measured even into the wells at the edge of the Brook/wetlands. This carbon will also degrade to further maintain reducing conditions and/or flush out over time.

The literature has some anaerobic biodegradation rates, mostly from laboratory studies. For example degradation of waste and peat can vary from 0.01 mg d<sup>-1</sup> to 1 mg d<sup>-1</sup>. Assuming the lowest value has some meaning for the present case, 5% of the carbon in the peat will degrade in roughly 13,000 years (or 1,300 years at 0.1mg/d<sup>-1</sup>).

Column studies completed to date that describe arsenic flushing also have tracked carbon flushing. The results of carbon flushing from the column study through 13 pore volumes show a 59% reduction in carbon with a long apparent tail associated with the removal. The 13 pore volumes are equivalent to removing carbon from an initial concentration of 6.3 mg/L to 2.6 mg/L. Keimowitz et al. (2005) found a similar slow removal of carbon from the landfill due to sorption of carbon to the mineral phase in the aquifer sediment. Using a distribution coefficient model they estimated that carbon flushing would require at least twice as much time to diminish as arsenic which would allow for continued release of arsenic from HFO. As applied to Shepley's Hill this suggests that up to 500 years would be required to remove carbon from



the landfill groundwater. Recall, however, that unlike Winthrop, Shepley's Hill has a thick layer of peat and underlying wetlands that will continue to deliver carbon to groundwater.

## **7.0 Bench Scale PRB Zero Valent Iron Test**

Bench testing of zero valent iron for arsenic removal at the site is discussed below.

### **7.1 Purpose**

The potential use of a permeable reactive barrier (PRB) composed of zero-valent iron (ZVI) for in-situ arsenic removal at the Shepley's Hill Landfill has generated considerable interest due to the relatively low cost and potential high efficiency of the method. A similar system has been explored and published for a former municipal landfill in Maine, published by Nicolaidis et al. 2003 Water Research. In that study, reduced water (Eh <-50 mv) high in dissolved arsenic (550 ug/L) and iron (8 mg/L) was effectively treated to <1 ug/L with retention times as low as 10 minutes. While the sites are similar, the Shepley's Hill Landfill has higher dissolved arsenic (4 mg/L) and iron (60 mg/L) and some different geochemical properties. Thus a lab bench test was performed to confirm the viability of the use of ZVI as part of a PRB at this site. The specific goals of the test were to:

- Test removal capacity of ZVI on unamended site groundwater
- Compare the removal efficiency of two types of ZVI Aggregates: ETI CC-1004 and CC-1200, both manufactured by Connelly-GPM, Inc.

### **7.2 Methods and Materials**

Testing included flow of site groundwater through columns prepared with Iron Aggregates ETI CC-1004 and CC-1200 and silica sand. Two tests were run with different conditions. Test methods are given below.

- Column configuration 18 inches long x 2 inches diameter (clear schedule 80 PVC)
- Up flow into bed from a variable speed peristaltic pump (GeoPump 2)
- Each column was fully packed with the following:
  - Column 1 contained 100% Iron Aggregate ETI CC-1004.
  - Column 2 contained 100% Iron ETI CC -1200 which due to the fine dust like particles led to "concrete like" mass and was not further evaluated.
  - Column 3 contained approximately 50% Iron Aggregate ETI CC-1004 by volume and 50% silica sand by volume.
  - Column 4 contained 25% Iron Aggregate CC-1200 by volume and 75% silica sand by volume.
  - Column 5 contained 100% silica sand.

- Site groundwater (SHM-10-14 and SHM-10-15) used in the column tests were collected directly into three 5-gallon carboys using a peristaltic pump while minimizing headspace in the carboys.
- Influent and effluent groundwater were analyzed for:
  - pH (by direct-read instrument YSI-556)
  - ORP (by direct-read instrument YSI-556)
  - DO (by direct-read instrument YSI-556)
  - dissolved and total As (by USEPA Method 200.7)
  - dissolved and total Iron (by USEPA Method 200.7)
  - dissolved and total Mn (by USEPA Method 200.7)
  - dissolved organic carbon (by Standard Method 5310)
  - sulfate (by USEPA Method 375.4)
  - alkalinity (by Standard Method 2320B)
- Laboratory analysis was conducted by Accutest Laboratories in Dayton, NJ.

#### Test 1

- Test 1 was run through Column 1, Column 3, and Column 5.
- Test 1 was conducted using 5 gallons groundwater of obtained from site monitoring well SHM-10-15.
- Test 1 was run for a 3.0 hour period. All columns were run simultaneously using common influent water.
- Groundwater was run through each column at approximately 30 mL/min for a retention time of approximately 9 minutes.
- Lab analytical samples were collected at t=0.25 hrs, 1.25 hrs, and 2.0 hrs. Analytical results from Test 1 are provided in **Attachment J**.

#### Test 2

- Test 2 was run through Column 1, Column 3, Column 4, and Column 5.
- Test 2 was conducted using 10 gallons of obtained from site monitoring well SHM-10-12.
- Test 2 was run for a 5.0 hour period. All columns were run simultaneously using common influent water.
- Groundwater was run through each column at approximately 30 mL/min for a retention time of approximately 9 minutes.
- Lab analytical samples were collected at t=0.5 hrs, 1.2 hrs, 2.9 hrs, and 4.3 hrs. Analytical results from Test 2 are provided in **Attachment J**.

## 7.3 Methods and Materials

### 7.3.1 Test 1

#### 7.3.1.1 Field Results

Attempts to pass groundwater through a column with 100% Iron Aggregate CC-1200 and with 50% Iron Aggregate CC-1200 and 50% silica sand were unsuccessful due to excessive back pressure formed by the iron material when saturated.

Influent groundwater pH increased by approximately 0.5 SU after passing through Column 1 and Column 3. There was no change as it passed through Column 5.

Influent groundwater ORP decreased by over 60 mV after passing through Column 1 and Column 3. There was no change in the ORP as it passed through Column 5.

#### 7.3.1.2 Laboratory Analytical Results

Influent water contained dissolved and total arsenic concentrations of 1,560-ug/L and 4,560-ug/L, respectively. Additionally, influent water contained dissolved and total iron concentrations of 21,700-ug/L and 47,000-ug/L, respectively. Sulfate was not detected in the influent water.

Both dissolved and total arsenic concentrations in groundwater decrease of >99.9% after passing through Column 1. Dissolved arsenic concentrations decreased an average of 99.7% and total arsenic concentrations decreased an average of 98.3% decrease after passing through Column 3. Dissolved arsenic concentrations showed an average of 4.1% and total arsenic concentrations decreased an average of 34.2% after passing through Column 5.

Dissolved Iron concentrations in groundwater decreased an average of 66.7% and total Iron concentrations decreased an average 5.6% after passing through Column 1, though dissolved and total iron increased over the course of the test. Dissolved iron concentrations in groundwater increased 134% and total iron concentrations increased an average 127% after passing through Column 3. Dissolved iron concentrations in groundwater decreased 16.1% and total iron concentrations decreased an average 28.5% after passing through Column 5.

Sulfate was present at concentrations of 87.6 mg/L, 38.3 mg/L, and 11.4 mg/L after passing through Column 1, Column 3, and Column 5, respectively.



## 7.3.2 Test 2

### 7.3.2.1 Field Results

Influent groundwater pH increased by approximately 1.0 SU after passing through Column 1, Column 3, and Column 4. There was an increase of approximately 0.2 SU as it passed through Column 5.

Influent groundwater ORP decreased by over 100 mV after passing through Column 1, Column 3, and Column 4. There was no change in the ORP as it passed through Column 5.

#### 7.3.1.1 Laboratory Analytical Results

Influent water showed averaged dissolved and total arsenic concentrations of 708-ug/L and 2,810-ug/L, respectively. Additionally, it showed average dissolved and total iron concentrations of 53,950-ug/L and 78,600-ug/L, respectively. Sulfate was not detected in the influent water.

Both dissolved and total arsenic concentrations in groundwater decreased by 99.9% after passing through Column 1. Dissolved arsenic concentrations on average decreased 98.8% and total arsenic concentrations decreased an average of 90.9% decrease after passing through Column 3. Dissolved arsenic concentrations decreased 97.7% and total arsenic concentrations decreased an average of 92.9% after passing through Column 4. Dissolved arsenic concentrations increased 28.6% and total arsenic concentrations decreased an average of 35.0% after passing through Column 5.

Dissolved iron concentrations in groundwater increased 114% and total iron concentrations increased an average 165% after passing through Column 1. Dissolved iron concentrations in groundwater increased an average of 192% and total iron concentrations increased an average of 284% after passing through Column 3. Dissolved iron concentrations in groundwater increased an average of 162% and total iron concentrations increased an average of 135% after passing through Column 4. Dissolved iron concentrations in groundwater increased an average of 7.2% and total iron concentrations decreased an average of 10.1% after passing through Column 5.

Sulfate was present at concentrations of 16.9 mg/L and 33.6 mg/L after passing through Column 1 and Column 4, respectively. Sulfate was not detected after passing through Column 3 or Column 5.

## **7.4 Conclusions**

Both Iron Aggregate ETI CC-1004 and CC-1200 were effective in decreasing arsenic concentrations in site groundwater through the bench scale testing. Iron Aggregate ETI CC-1004 was easier to handle during the test and may be preferable for implementation in the field.

Increases in dissolved and total iron after passing through the iron aggregate suggest that during field implementation a solids filter may be desirable for water that passes through the iron aggregate. This is supported by the decrease in total arsenic seen in both tests after passing through the column packed with silica sand only.

Changes in parameters pH, ORP, and sulfate after passing through iron-packed columns suggest that the iron aggregate is having the intended effect of creating an environment conducive to arsenic removal.

## **8.0 CONTAMINANT CHARACTERISTICS**

This section describes and summarizes the contaminants of concern and the site specific fate and transport patterns.

### **8.1 Sources and Releases**

The primary contaminant of concern is arsenic. The sources of arsenic have been described previously and include (1) bedrock, (2) glacial till, (3) aquifer sands overlying bedrock and underlying waste or peat, (4) landfill waste, and (5) peat. While the exact magnitudes of the various types of sources at and beneath the landfill are unknown, the relative importance of the possible sources (as they now exist) is known based on recent waste and peat characterization studies. The relative importance of the arsenic sources is as follows: aquifer sands > landfill waste = peat > bedrock = glacial till. Due to the cap place on the landfill, leachate from the landfill waste is expected to be minimal except where waste is in direct contact with the groundwater. Current estimates suggest that only 11% of the landfill waste is now in contact with groundwater. Based on recent groundwater profiling in this area, metals and arsenic entering groundwater from the waste appears to be minimal and primarily in the center of the landfill. Arsenic is released into groundwater from the sources by naturally occurring and landfill-induced reducing conditions caused by carbon degradation and oxygen depletion that lead to the anaerobic conditions. Portions of the landfill also overlay pre-existing, buried peat deposits that induced reducing conditions prior to emplacement of the landfill over the peat and associated wetlands. Therefore, the peat within the landfill footprint caused arsenic mobilization to both the North end of the site at Nonacoicus Brook and east to Red Cove prior to the placement of waste. This natural process will persist even if the landfill waste were to be removed. Recent estimates indicate that peat degradation and reducing conditions could persist far into the future

## 8.2 Nature and Extent of Contaminant

Potential sources of arsenic in groundwater include (1) bedrock, (2) till, (3) aquifer sand overlying bedrock and underlying waste or peat, (4) landfill waste, and (5) peat (see Section 6.4, Sovereign, 2011 for discussion of arsenic content in different materials). In terms of mass available for mobilization, the primary source of arsenic in groundwater appears to be the aquifer sand rich in amorphous iron hydroxide solids, usually coated on sand grains as documented through microscopy. While the exact magnitudes of the various types of sources at and beneath the landfill are unknown, the relative importance of the possible sources is known based on recent waste and peat characterization studies. The relative importance of the arsenic sources decreases in the order: aquifer sand > landfill waste = peat > bedrock = till. Due to the cap placed on the landfill, leachate from the landfill waste is expected to be minimized except where waste is in direct contact with the groundwater. Based on recent groundwater profiling in this area, metals and arsenic entering groundwater from the waste appears to be minimal and primarily in the center of the landfill. Arsenic is released into groundwater from the sources by naturally occurring and landfill-induced reducing conditions caused by carbon degradation and oxygen depletion that lead to anaerobic conditions. Portions of the landfill overly pre-existing, buried peat deposits that induced reducing conditions prior to emplacement of the landfill over the peat and associated wetlands. Therefore, the peat within the landfill footprint caused arsenic mobilization to the north end of the site toward Nonacoicus Brook as well as east toward Plow Shop Pond prior to the placement of waste. This natural process will persist even if the landfill waste were to be removed. Recent estimates indicate that peat degradation and reducing conditions could persist for hundreds to thousands of years.

Arsenic solubility is controlled by desorption from the iron solids and by reductive dissolution of the iron (III) solids created by biodegradation of peat and waste. The distribution coefficient of 7.6 L/kg indicates that for example, if 30 mg/kg arsenic is found in the aquifer sand then 3,947 ug/L could be found in the aquifer groundwater. The distribution coefficient is useful for predicting ranges of arsenic concentrations that could be expected in local groundwater. It is important to note that this process does not, however, include dissolution of the iron solid, a process that could lead to higher arsenic concentrations. Use of the  $K_d$  should consider that the correlation is dominated by the cluster of samples at the low end of the plot. This site specific  $K_d$ , which covers a large range of concentrations, may also be in fact a series of two or more slightly different plots or lines representing different mechanisms of arsenic retention.

Prior to emplacement of the landfill, much of the local groundwater flow emanating from and through the peat within the landfill footprint discharged to Red Cove. As waste was emplaced in the landfill and the landfill was capped, local groundwater gradients changed and much of the groundwater flow was directed in a more northern direction.

To date, peat has not been encountered north of the landfill. However, due to the presence of wetlands, areas of buried peat deposits would not be unexpected. Recent well sampling north of the landfill indicates that in-situ carbon degradation and landfill leachate have resulted in reducing conditions. This has been confirmed by the low dissolved oxygen, elevated dissolved methane concentrations, elevated dissolved carbon, elevated ammonia concentrations, and



elevated arsenic and iron concentrations. Thus both naturally occurring conditions and landfill influence have and will continue to mobilize arsenic in that area.

Nonacoicus Brook is a groundwater discharge divide. Recent sampling shows there is no arsenic in the monitoring wells directly north of the wetlands confirming no impact from the landfill. The bedrock delineation and general elevation of the northern most wells indicates that the bedrock surface is much higher on the north side of the wetlands and brook than the southern side which indicates that groundwater flow is roughly opposite in direction to flow from the landfill. This flow of groundwater from the north effectively creates a redox boundary that should precipitate arsenic into iron solids as the water becomes more oxidizing. The impact on water quality is somewhat predictive. Based on the mixing estimates in the SAR (Sovereign, 2011) and the observed changes in arsenic from the DPT points placed in the north end, arsenic in detectable quantities are unlikely to ever occur in the wetlands or the brook.

### 8.3 Contaminant Fate and Transport

Fate and transport of arsenic is related both to the source of arsenic and the presence of degradable carbon species in the aquifer.

Arsenic fate and transport at the north end of the site has been determined in some locations. The groundwater on the north side of the Brook that is intruding into the landfill impacted water on the southern side of the Brook contains on average 50 mg/L of sodium. The wells in the landfill contain on average 15 mg/L of sodium. This is due to the intrusion of the iron-bicarbonate water created from the landfill carbon degradation process and subsequent replacement of calcium and sodium in the native groundwater. The wells at the north end of the impacted area at the south side of the Brook and wetlands contain on average 26 mg/L of sodium. This indicates that mixing of water from the north side of the Brook which is high in sodium is occurring. Using a simple mixing model, approximately 47% mixing between the two waters has occurred. This same analysis can be done with calcium, bicarbonate, sulfate or chloride with similar results. Depending on the analyte used in the mixing calculation, some water appears to be mixing with water from the north by as much as 75%

The subsequent mixing with this water diminishes arsenic to low levels. Mixing also results in redox changes that will oxidize iron (II) to iron (III) with subsequent adsorption of soluble arsenic. Due to the marked geochemical changes in the north end, arsenic exceeding 400-ug/L will not enter the wetlands/Brook underflow. Since rapid oxidation is expected in the wetlands, detectable arsenic entering the base-flow is unlikely. A proposed monitoring well network will be used to further examine the geochemical changes in the north end impacted area.

Analysis of reducing conditions created by landfill waste or peat suggests that the peat layer, with or without waste above it supplies more carbon input to the groundwater than ash or waste alone by almost a factor of two. This also suggests that the peat layer and associated wetlands have been acting as a carbon source long before the landfill existed. This carbon source would also have led to locally reducing conditions that would have mobilized arsenic before the existence of the landfill.

## 9.0 CONCEPTUAL SITE MODEL

The data gathered during the above noted and previously referenced investigations were used to continually update and refine the CSM as it has been presented herein. Presently, the conceptual site model has been updated to include the following new information.

- Waste within the landfill has been further characterized with the recent installation of 5 borings drilled through the landfill to bedrock. Waste analysis revealed that with the exception of lead, zinc and copper most trace elements were at typical background levels. Arsenic does not appear to have leached significantly from the waste into groundwater due to the lack of typical leaching patterns or enrichment in subsurface soils. Arsenic in waste was also not dissimilar to arsenic observed locally or regionally in soils or rock. Arsenic in the waste or peat did not exceed 60 mg/kg. Leaching tests indicate that landfill waste potentially could deliver up to 500 ug/L arsenic to underlying groundwater. However, placement of the cap has likely eliminated possible leaching of arsenic and any other constituents from landfill waste to underlying groundwater.
- In comparison to the waste, the underlying sand potentially leaches up to 1,500 ug/L arsenic to groundwater. In addition reductive dissolution of arsenic containing amorphous iron solids could release as much as 30,000 ug/L of arsenic. Based on these results, the aquifer sand is the dominant source of arsenic at the landfill.
- The borings through the landfill revealed that thick peat layers are found underlying waste in the center of the landfill roughly bounded by SHL-99-29x, SHM-10-13, SHM-10-14 and SHM-10-15.
- The peat and the associated wetlands preceded the landfill. The peat is a significant source of carbon to the groundwater and caused locally reducing conditions prior to emplacement of waste. Therefore arsenic mobilization has been occurring historically prior to landfill development and will continue to occur as long as carbon degradation within the peat takes place.
- Anaerobic degradation within the aquifer in the northern impacted area is occurring with or without landfill influence. This occurs likely from natural organic matter and possibly peat since this area was at least in part a former wetland. These conditions have allowed arsenic to be mobilized within the northern impacted area aquifer sands and will likely persist for centuries.
- The importance of peat as a source of reducing conditions and arsenic mobilization has been addressed. Calculation of carbon inputs to groundwater at the site demonstrates that peat could supply up to twice as much carbon to underlying groundwater compared to waste alone. This may or may not have been the case throughout the landfill history. Early in the landfill history waste might have been the more important carbon source but as easily degradable material was consumed, the landfill input

diminished compared to that of the underlying peat. The carbon dating studies conducted by Gannett Fleming (2009 Memo, USEPA) on methane sources from the landfill seem to indicate that methane emanating from the landfill was biogenic (produced by biodegradation) and that the carbon source was likely entirely from historic or old carbon such as the peat. However analytical problems discussed in the report prevent any further use of the data.

- Literature reviews and textbooks on wetlands and peat make it abundantly clear that the formation and maintenance of wetlands and peat always result in anaerobic conditions and resulting biogeochemical conditions that will mobilize arsenic as explained in the SAR. High arsenic levels are attributed to biodegradation of buried peat deposits which drives the reductive dissolution of FeOOH supplying high amounts of arsenic to groundwater. The correlation of peat deposits to high arsenic has also been noted by others (Ravenscroft, et al., 2001; Smedley and Kinniburgh, 2002).
- Arsenic in groundwater in the north impacted area appears to diminish substantially prior to discharge into Nonacoicus Brook and wetlands due to the underlying oxygenated zone. The redox boundary occurs due to intrusion or mixing of non-impacted groundwater entering the Brook and wetlands from the north and north east of the Brook in the opposite direction of the flow from the landfill. Chemistry of water in several DPT points close to the brook show mixing or dilution with water from the north side indicating that the brook is a discharge divide. Arsenic is not expected to impact the brook and wetlands due to this redox boundary. The area to the east of the new DPT points has only been partially characterized.
- The placement of the landfill cap increased arsenic flux to the north. Operation of the pump and treat system subsequently caused a significant reduction in arsenic concentrations in wells SHP-05-41B and SHM-93-22B as the additional arsenic flux was mitigated.
- Groundwater discharge at the north end appears to follow the particle track data presented by AMEC. Arsenic impact to the MacPherson well is not anticipated based on the results of the investigation at the redox boundary.
- Newly acquired bedrock information indicated that bedrock was located at a shallow depth than originally projected within the area near Nonacoicus Brook. This information was incorporated within the hydrogeologic study and the particle track updated. The results indicated an increase in the groundwater flow velocity near the brook, but continued to show that the system is collecting the arsenic impacted groundwater.
- An evaluation of methane determined that the dissolved concentration within groundwater does not present an explosive hazard.



- Arsenic entering Red Cove is likely from reducing conditions prevalent in the landfill and peat. The reducing conditions have mobilized arsenic from the aquifer sand which is now entering the Red Cove via a different flow path than the predominant south-north flow pattern observed for most of the landfill. It is also possible that the arsenic and iron floc impact to Red Cove preceded the placement of the landfill due to the same reducing conditions created by the historic wetlands and peat. The landfill and its reducing conditions would then have exacerbated the flux

## 10.0 FINDINGS AND CONCLUSIONS

The findings of this investigation as summarized as follows:

- North Impact Area Delineation & Monitoring - The investigation included the advancement of soil borings, completion of groundwater vertical profiling, and construction and sampling of monitoring wells on the northern and southern side of Nonacoicus Brook. These boring and well locations are identified as SHM-10-01, SHM-10-02, SHM-10-03, SHM-10-04, SHM-10-05 (no well installed), SHM-10-05A, SHM-10-08, SHM-10-09 (no well installed), and SHM-10-10. Groundwater profiling conducted during the drilling program recorded dissolved arsenic concentrations varying from non-detect to 112-ug/l. Sampling and analysis of groundwater samples obtained from the monitoring wells reported concentrations of dissolved arsenic varying between 0.43 and 7.87-ug/L. Lastly, the geophysical survey indicated that bedrock slopes upward, thereby restricting the migration of the arsenic. The results of these data define the down-gradient extent of the arsenic impact below the vicinity of the southern bank of Nonacoicus Brook. Groundwater flow from the north and northeast of the Brook flows and mixes with groundwater advancing north and northwest from the landfill area creates an oxidation/reduction front that effectively limits the northern extent of the arsenic at the mixing front.
- North Plume Capture - Points SHM-10-06 and SHM-10-06A were installed to evaluate the capture and confinement of the arsenic plume on the north and northeastern side of the existing arsenic treatment plant. Groundwater profiling indicated evidence of dissolved arsenic ranging from 10 to 2,540-ug/L in well SHM-10-06, while decreased concentrations were detected in SHM-10-06A at concentrations of non-detect to 106-ug/L. Sampling and analysis of groundwater from the monitoring wells document concentrations decreasing between the two wells from 2,710 to 60.1-ug/L. These data were included in refined particle tracking modeling that indicates that the treatment system is reducing arsenic mass and capturing the bulk of arsenic mass on the northern and northeastern side of the treatment plant and that the impacts are bounded between monitoring points SHM-10-06 and SHM-10-06A. Drilling operations indicated a shallower than previously extrapolated bedrock surface in this area. The shallower rock elevations were plotted and included in the refined particle track models that document a bedrock trough trending northward through the landfill and that the shallower rock ridge along the east side of the landfill appears to restrict arsenic migration in a northerly direction.

- Landfill Gas Impact -Modeling was conducted to determine if methane gas intrusion into an occupied building or structure was a concern. The results of this modeling used a dissolve methane concentration of 10-mg/L in the groundwater and determined that this concentration would not pose an explosive hazard.
- East Plume Delineation and Capture – A temporary monitoring well was advanced at the location identified as SHM-10-07. Groundwater profiling recorded dissolved arsenic concentrations varying between 58 and 1,350-ug/L, while groundwater sampling of this monitoring well confirmed dissolved arsenic concentrations of 818 and 918-ug/L. Drilling operations indicated a shallower than previously extrapolated bedrock surface in this area. The shallower rock elevations were plotted and included in the refined particle track models that document a bedrock trough trending northward through the landfill and that the shallower rock ridge along the east side of the landfill appears to restrict arsenic migration to a northerly direction.
- Arsenic MNA/Source Strength and Reducing Environmental Evaluation – An evaluation of the collected information determined the following;
  - The primary source of arsenic in groundwater appears to be aquifer sands rich in amorphous iron hydroxide solids, usually coated on sand grains as documented through microscopy. Other sources of arsenic may include landfill waste, peat, and bedrock/till. The possible contribution of landfill waste has been reduced due to depletion of easily degradable carbon and recent capping of the landfill. While peat in some instances was found to contain arsenic, it is not clear if the peat contained the arsenic originally or whether arsenic accumulated in the peat by leaching of arsenic from overlying waste.
  - Arsenic solubility is controlled by desorption from the iron solids and by reductive dissolution of the iron (III) solids created by biodegradation of peat and waste. A site specific distribution coefficient (Kd) was derived from the aquifer solids content and aqueous arsenic in contact with the solids. The equilibrium distribution coefficient of 7.6. The distribution is useful for predicting ranges of arsenic concentrations that could be expected in local groundwater. This process does not however include dissolution of the iron solid, a process that could lead to higher arsenic concentrations.
  - Arsenic groundwater distribution has been elucidated via a number of transects and depth profiles. The distribution of arsenic can be considered as (1) increasing with depth to just above the glacial till layer, (2) highest in the center of the landfill near SHM-10-14 and SHM-10-15, (3) slowly decreasing in concentration to the north of the landfill to the south side of the Brook and wetlands, and (4) controlled in large degree by the bedrock surface as far as flow direction is concerned.
  - The redox boundary appears to be located in the vicinity of SHM-10-10. The boundary consists of three features: (1) a bedrock surface that controls the flow of landfill impacted water to the Brook but also brings groundwater from the north and northeast of the Brook that counters the landfill flow, (2) intrusion of clean more

oxidized groundwater from the north side of the landfill, and (3) mixing of clean water resulting in precipitation of arsenic that does not impact the water quality in the Brook or wetlands. The area east of SH-10-17 along the brook and wetlands has not been completely delineated.

- Carbon inputs to the groundwater from biodegradation of waste or peat indicates that peat is likely more important for maintaining reducing conditions than landfill waste. The reducing conditions created by the peat preceded the landfill, but were exacerbated by the additional carbon source from the landfill waste. Peat formation is a result of reducing conditions, but also maintains reducing conditions by biodegradation and release of short chain carboxylic acids and methylated amines that will drive iron oxy hydroxide reduction and ammonia production (Bergmann et al, 1999) both byproducts that are widespread at the site.
- The time to return the aquifer to “pre-landfill” conditions has been simulated from columns experiments. The time frame describing removal of soluble arsenic from the landfill aquifer and north impacted area is approximately 270 years based on this data.
- Peat within the landfill footprint caused arsenic mobilization to the north end of the site toward Nonacoicus Brook as well as east toward Plow Shop Pond prior to the placement of waste. In addition, wetlands and presumably peat occurring in the NIA are also a source of natural reducing conditions that will persist even if the landfill waste were to be removed. Recent estimates indicate that peat degradation and reducing conditions could persist for hundreds to thousands of years.

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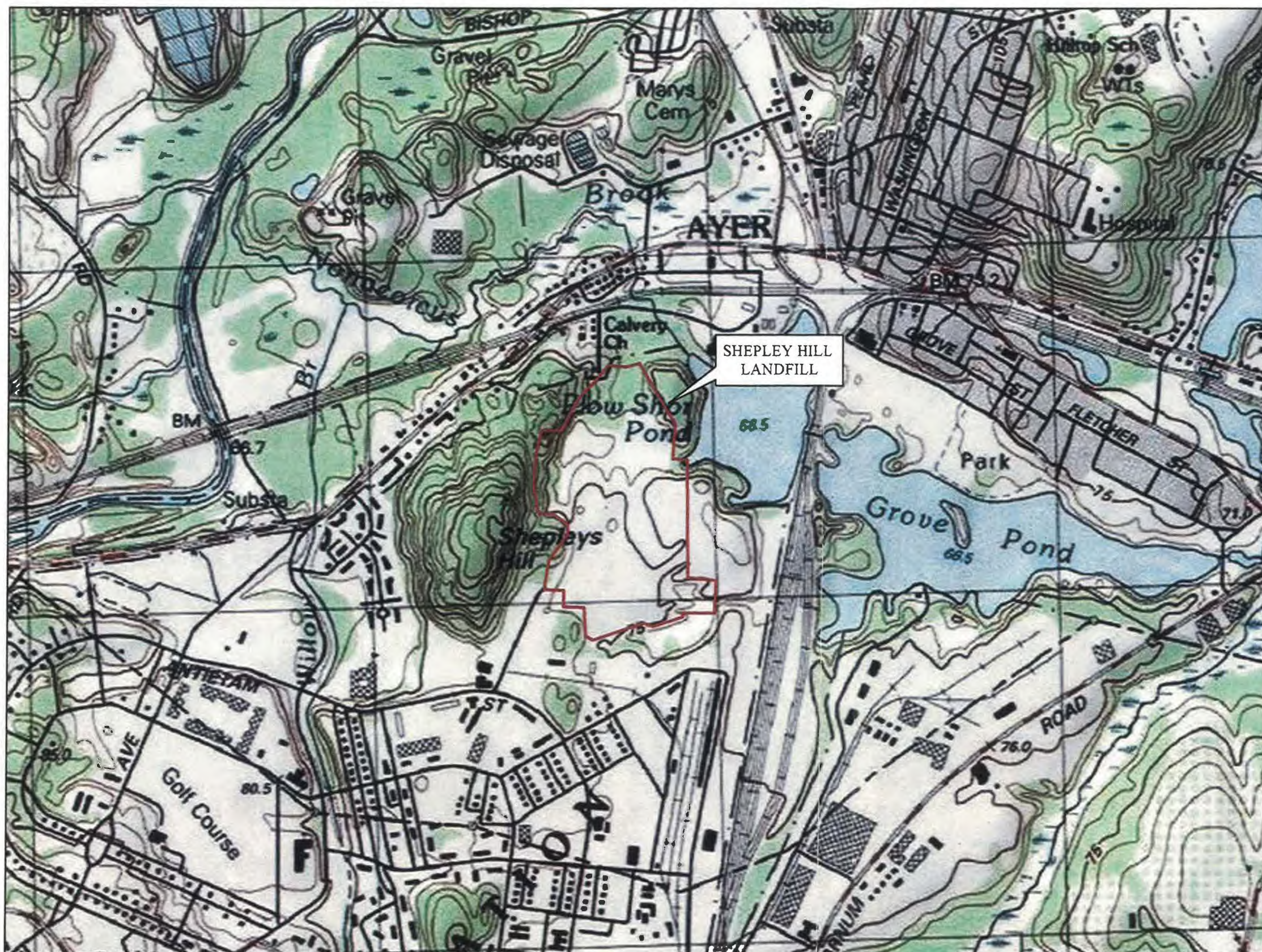
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## FIGURES



## FIGURES





## FIGURE 1 SITE LOCUS

FORT DEVENS  
AYER, MASSACHUSETTS



0 1,000  
Feet  
1 in = 1,000 ft



### Legend

APPROXIMATE SITE BOUNDARY

NOTES AND SOURCE INFORMATION:  
TOPO: 2009 NATIONAL GEOGRAPHIC SOCIETY, i-cubed  
IMAGERY: ESRI, i-cubed, USDA FSA, USGS, AEX,  
GEO EYE, GETMAPPING, AEROGRIID, IGP

DECEMBER 2010 ROV

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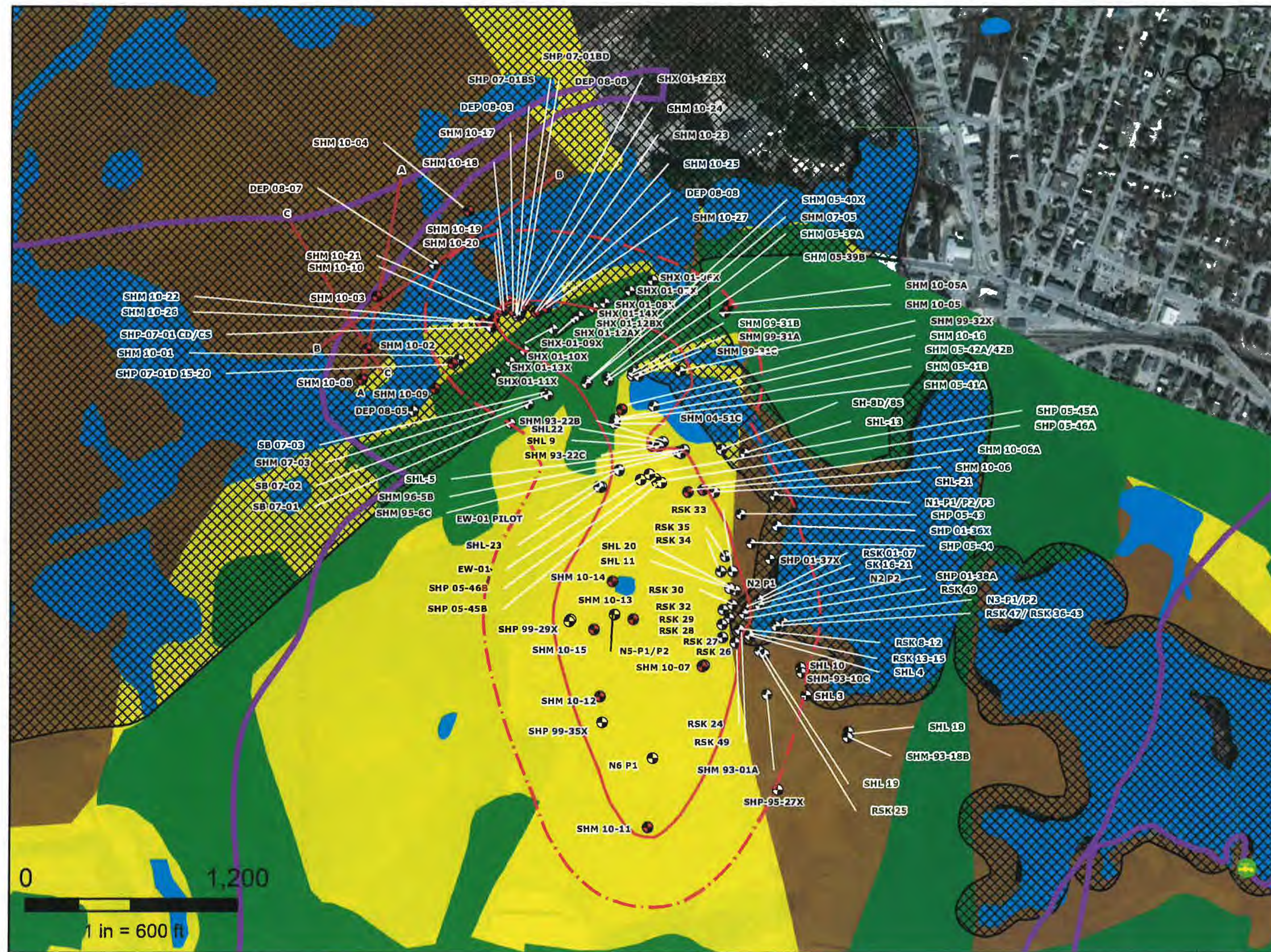
**LEGEND**

-  BORING/ WELL LOCATION
-  2010 WELL INSTALLATION
-  COMMUNITY GROUNDWATER SOURCE
-  TRANSECTS
-  IMPACTED AREA
-  400' FROM IMPACTED AREA
-  DEP APPROVED ZONE II
-  ACEC
-  WETLAND
-  NPDWSA
-  HIGH YIELD AQUIFER
-  MEDIUM YIELD AQUIFER

DECEMBER 2010 ROV; REVISED MAY 2011 ROV



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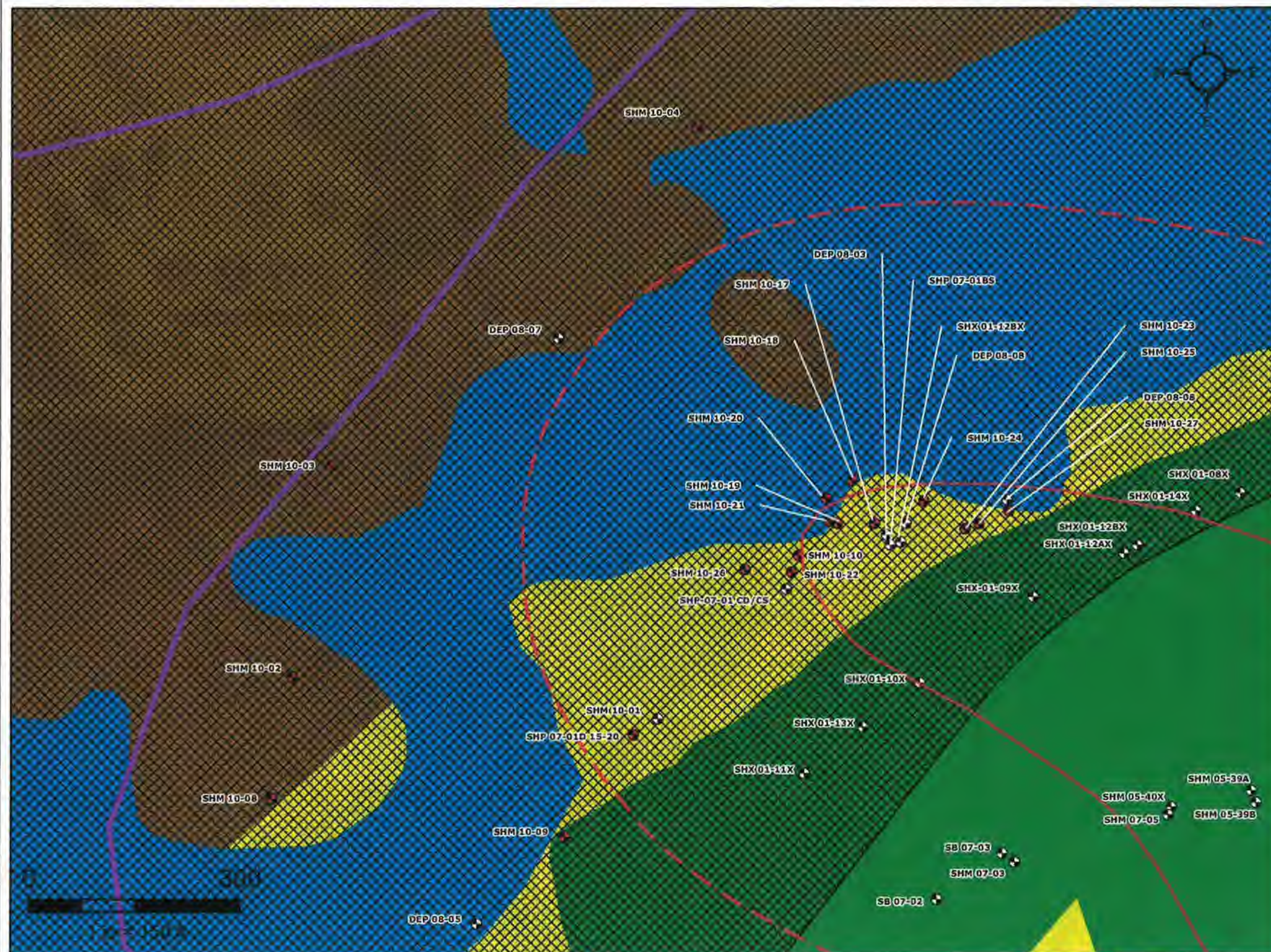
**FIGURE 5  
OVERALL SITE PLAN -  
NORTHWESTERN  
ENLARGEMENT  
FORT DEVENS  
AYER, MASSACHUSETTS**

**LEGEND**

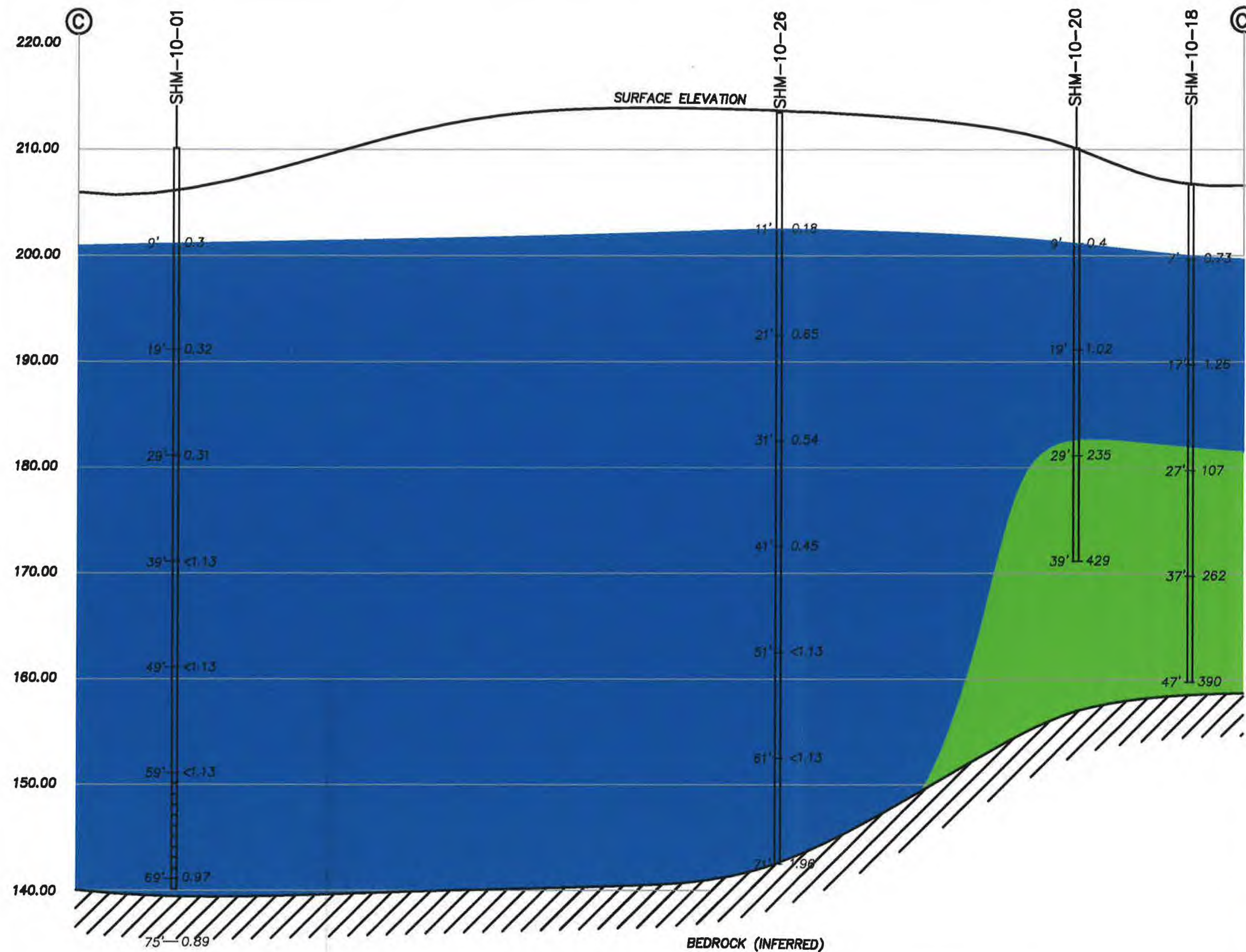
-  BORING/ WELL LOCATION
-  2010 WELL INSTALLATION
-  IMPACTED AREA
-  400' FROM IMPACTED AREA
-  DEP APPROVED ZONE II
-  ACEC
-  WETLAND
-  NPDWSA
-  HIGH YIELD AQUIFER
-  MEDIUM YIELD AQUIFER

**NOTES AND SOURCE INFORMATION:**  
 AERIAL IMAGERY: 2010 ESRI, I-cubed, USDA FSA,  
 USGS, AEX, GEOEYE, GETMAPPING, AEROGRIID,  
 IGP  
 WETLAND DATA: 2010 U.S. FISH AND WILDLIFE  
 SERVICE, DIVISION OF HABITAT AND  
 RESOURCE CONSERVATION  
 2010 AMEC EARTH AND ENVIRONMENTAL, PROPOSED  
 INVESTIGATIONS NEAR THE IMPACTED AREA. JDP  
 OFFICE OF GEOGRAPHIC INFORMATION (MASSGIS),  
 COMMONWEALTH OF MASSACHUSETTS EXECUTIVE  
 OFFICE OF ENVIRONMENTAL AFFAIRS  
 JUNE 2006 NON-POTENTIAL DRINKING WATER SOURCE  
 AREAS (NPDWSA)  
 JULY 2007 AQUIFERS  
 APRIL 2009 AREAS OF CRITICAL ENVIRONMENTAL  
 CONCERN (ACEC)  
 MARCH 2010 WELLHEAD PROTECTION AREAS  
 DECEMBER 2010 ROV; REVISED MAY 2011 ROV

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VERTICAL SCALE 1"=10'  
VERTICAL EXAGGERATION=5X

#### LEGEND

- DISSOLVED ARSENIC CONCENTRATION 0-100 ug/L  
BASED ON GROUNDWATER PROFILING
- DISSOLVED ARSENIC CONCENTRATION 100-500  
ug/L BASED ON GROUNDWATER PROFILING
- 47'-390 DEPTH - DISSOLVED ARSENIC  
CONCENTRATION ug/L
- POINTS TERMINATED AT REFUSAL  
CONDITIONS/POSSIBLE BEDROCK

**FIGURE 8**  
**GEOLOGICAL CROSS SECTION C-C'**  
**DISSOLVED ARSENIC CONCENTRATIONS**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

MAP PREPARED 12/1/10.  
REV. 5-4-11

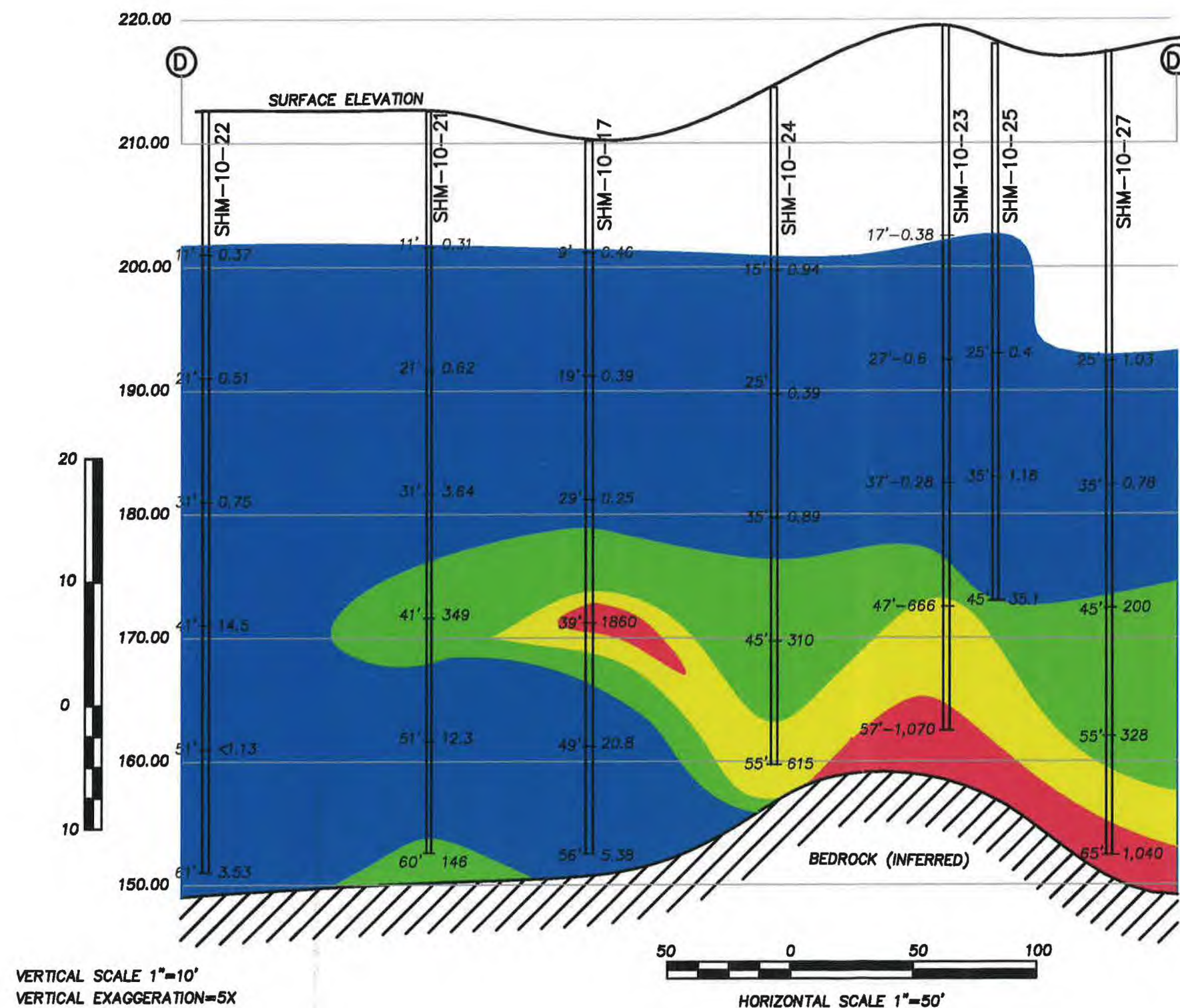
PLAN PREPARED BY:  
NRS



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**FIGURE 9**  
**GEOLOGICAL CROSS SECTION D-D'**  
**DISSOLVED ARSENIC CONCENTRATIONS**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

MAP PREPARED 12/1/10.  
REV. 5-2-11

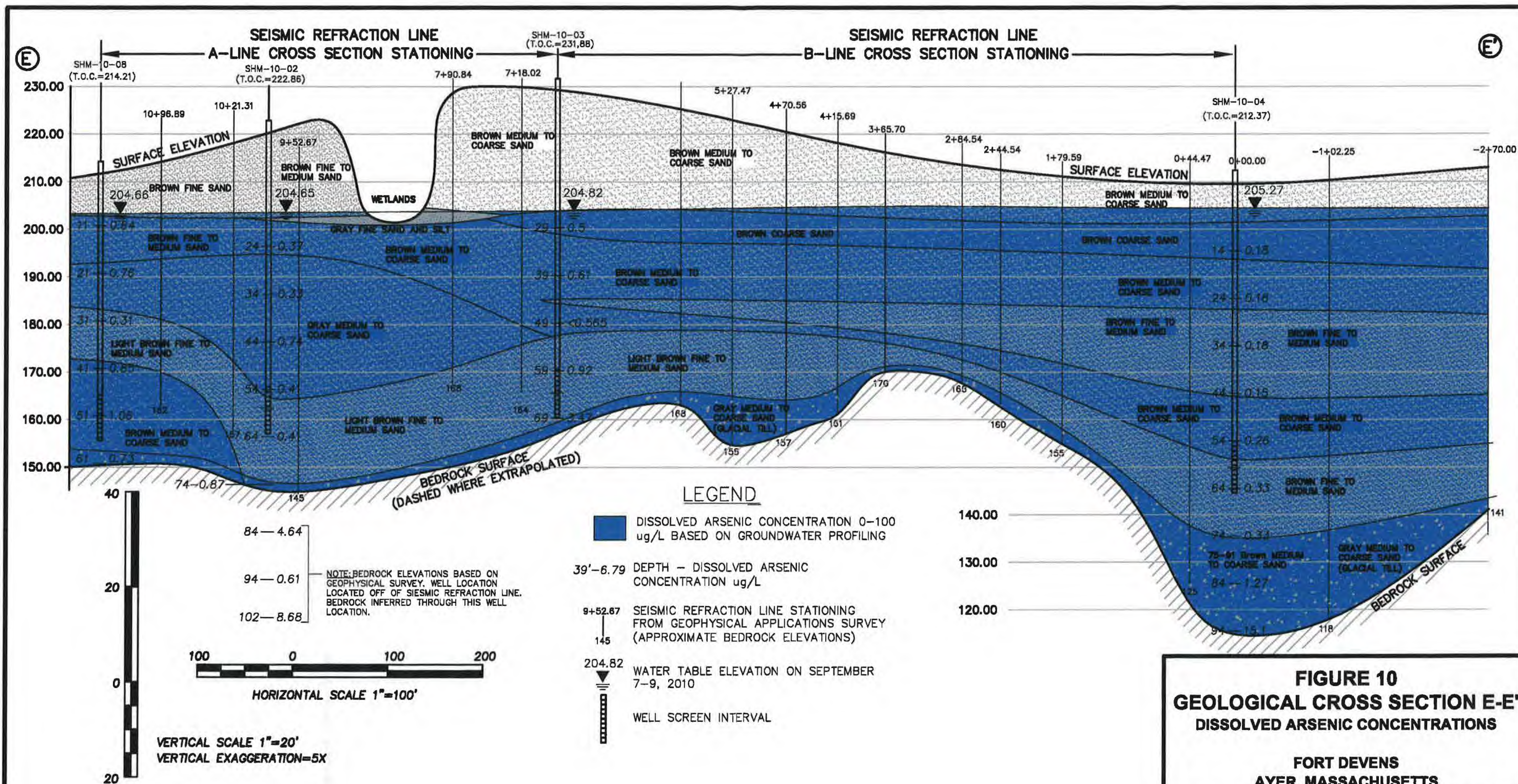
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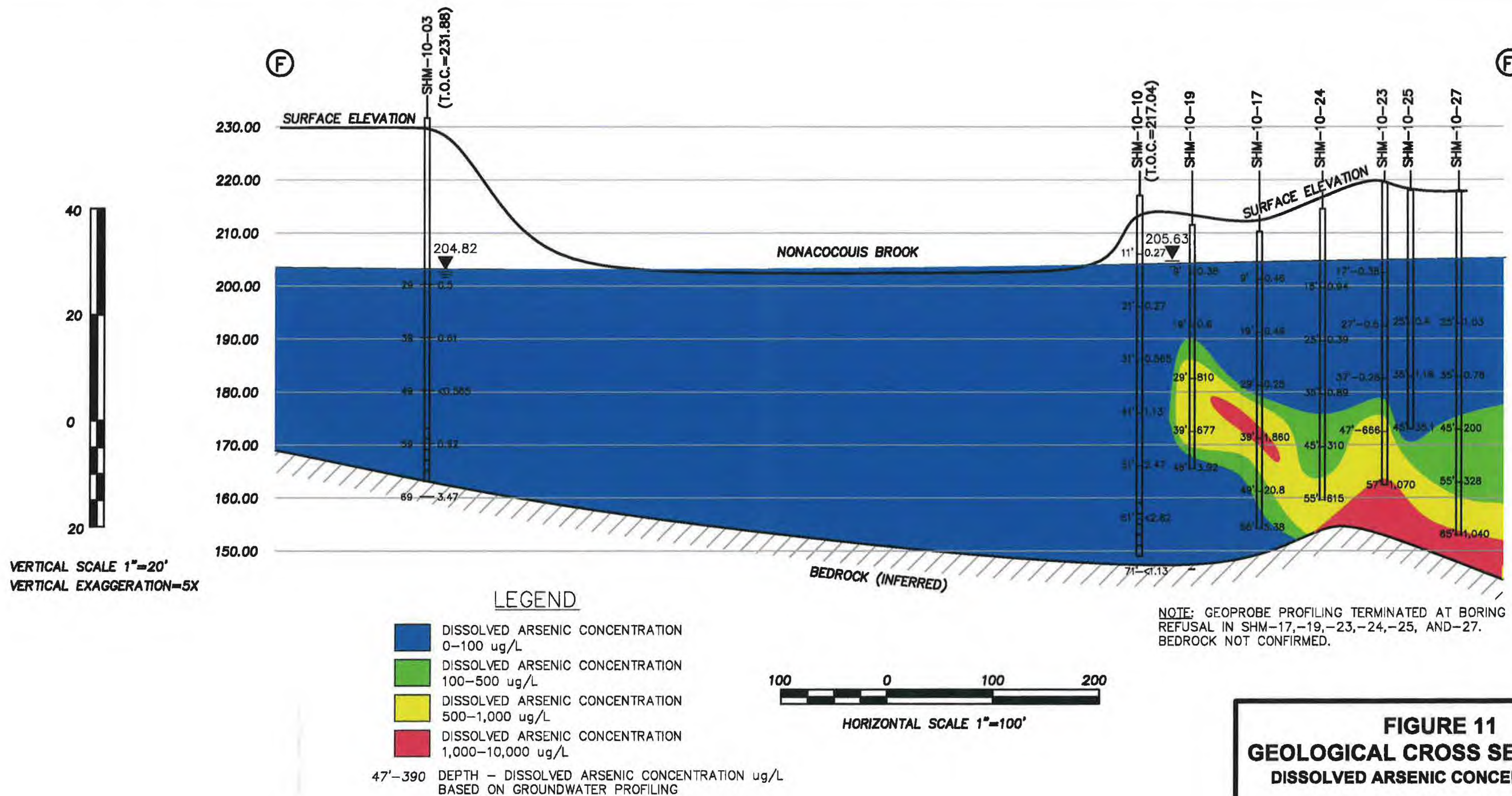
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**FIGURE 11**  
**GEOLOGICAL CROSS SECTION F-F'**  
**DISSOLVED ARSENIC CONCENTRATIONS**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

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 REV. 4/26/11.

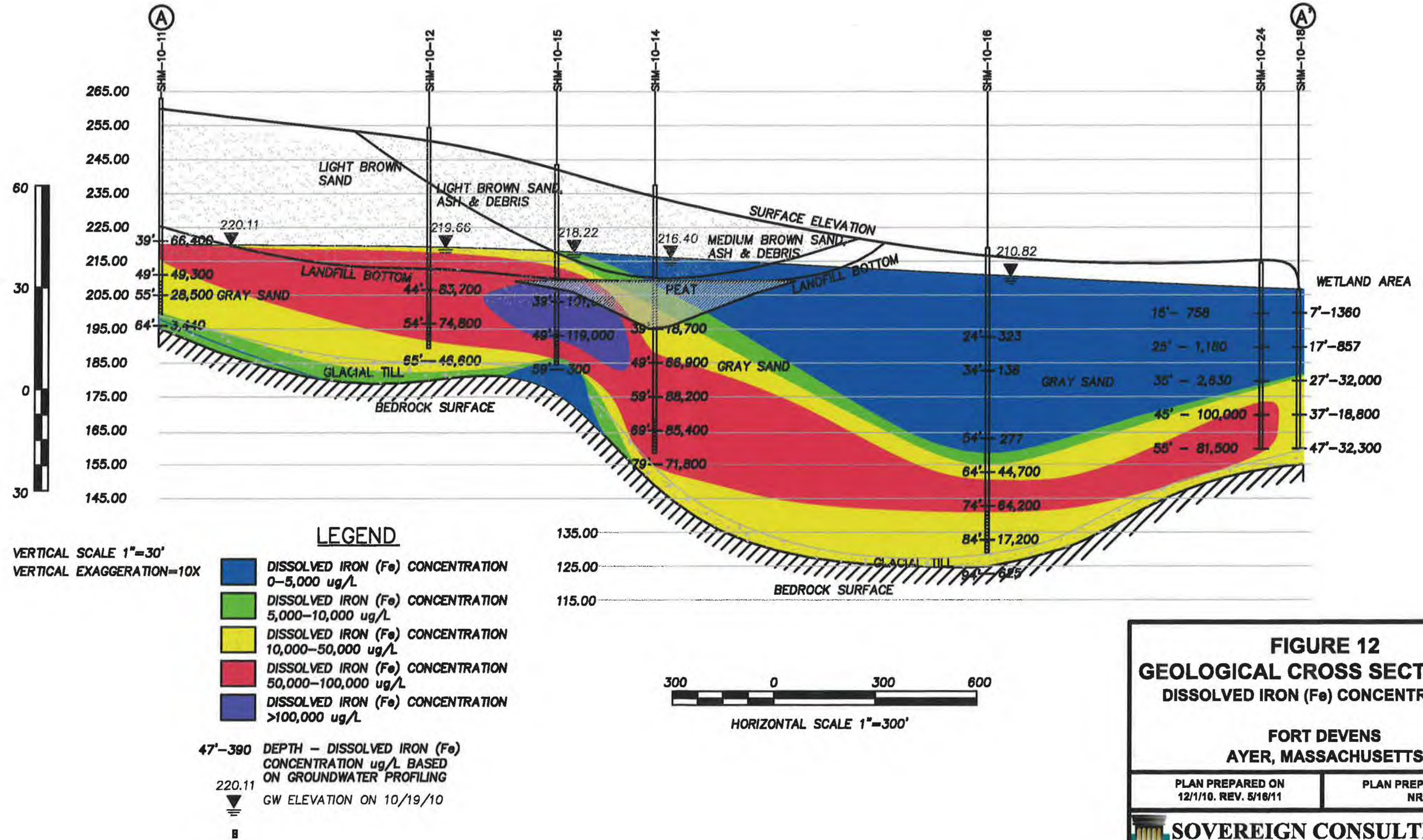
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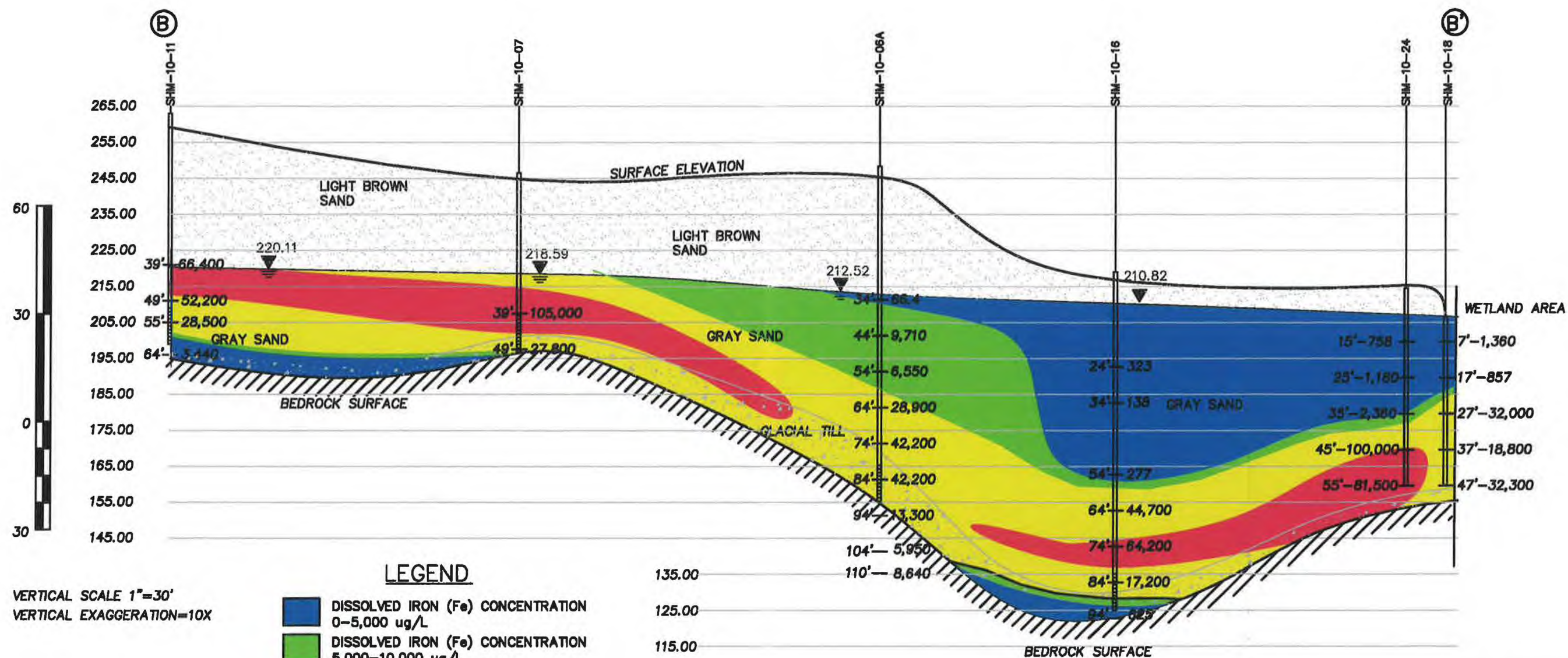
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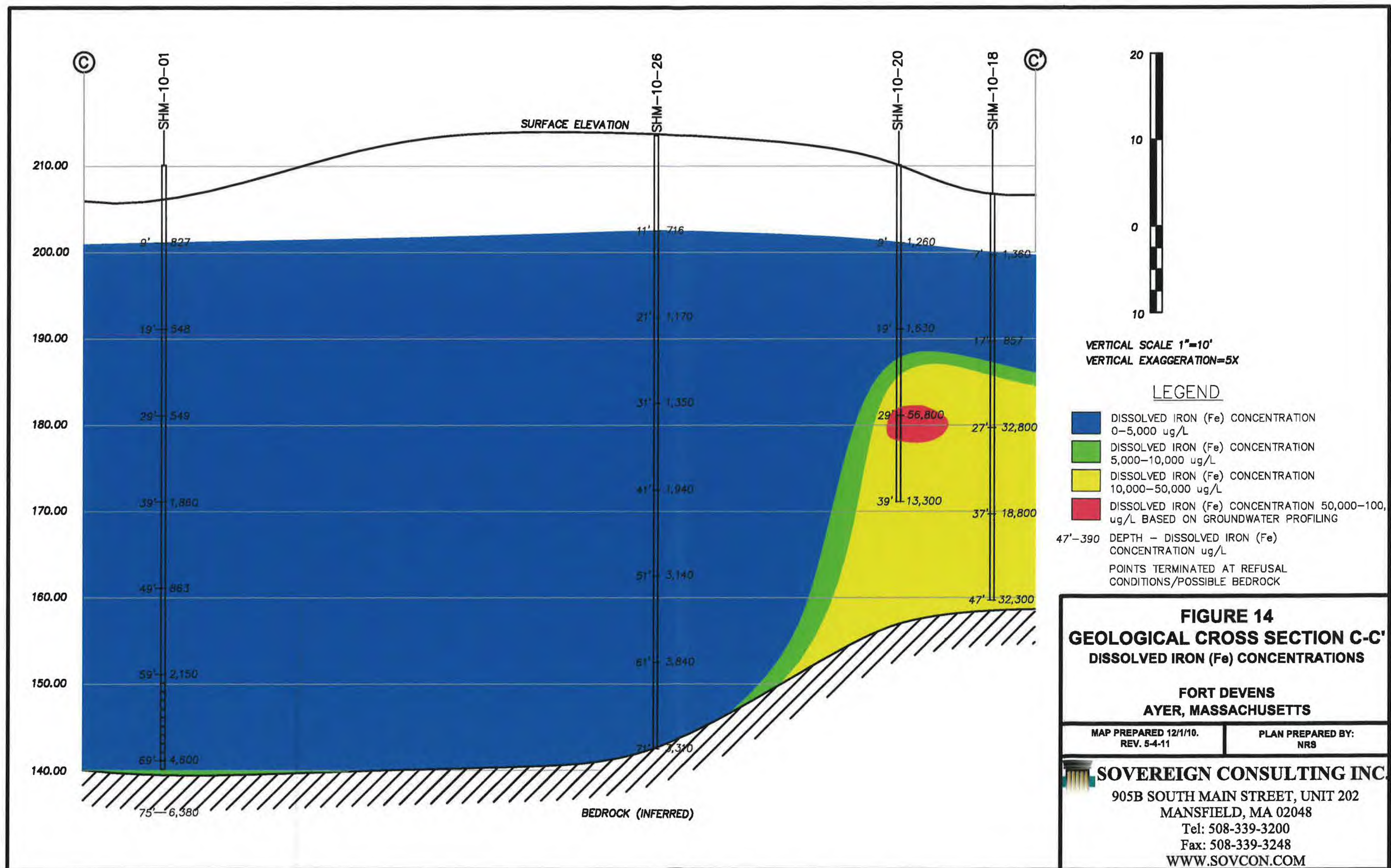




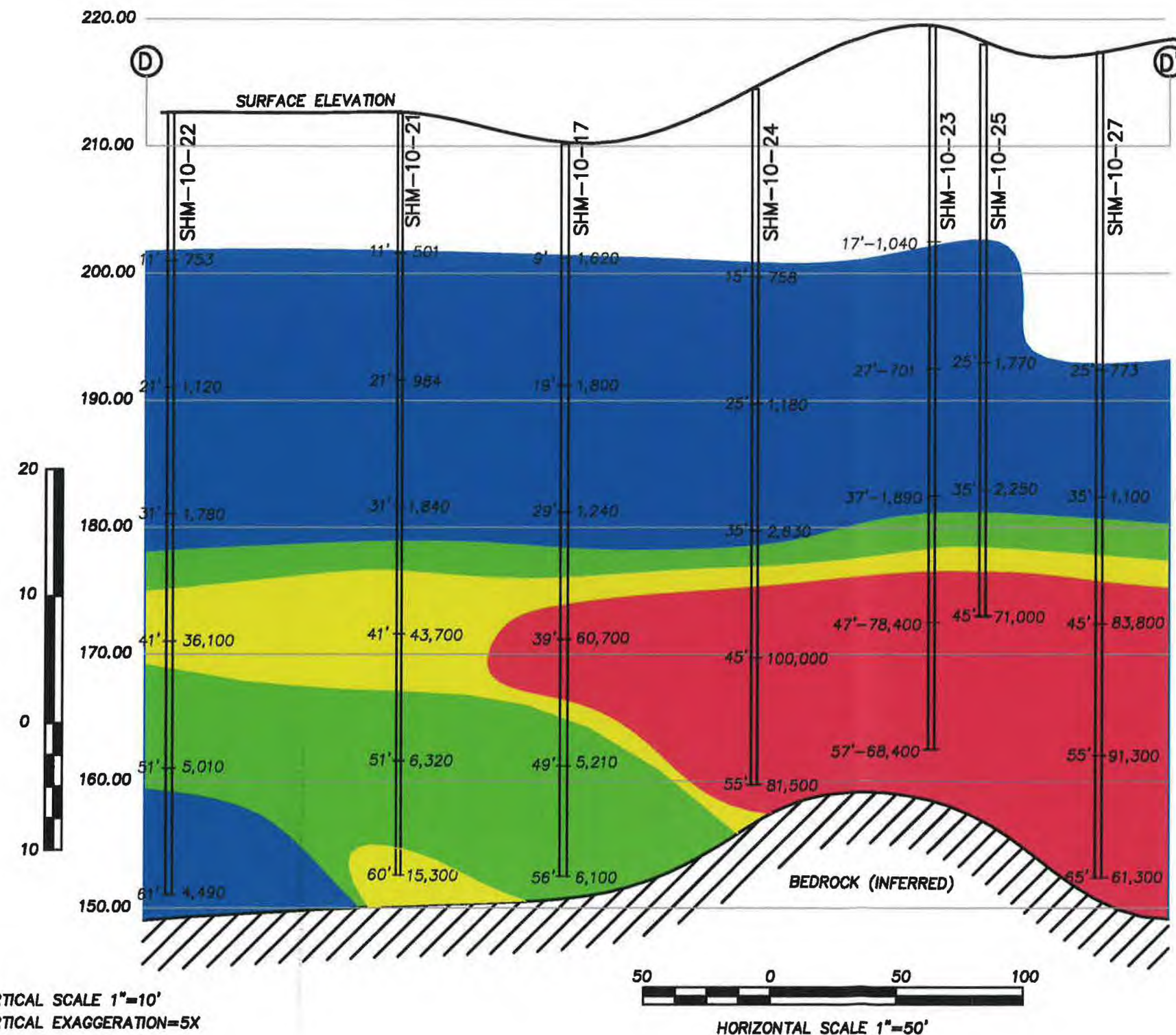












### LEGEND

- DISSOLVED IRON (Fe)  
CONCENTRATION 0-5,000 ug/L
- DISSOLVED IRON (Fe)  
CONCENTRATION 5,000-10,000 ug/L
- DISSOLVED IRON (Fe)  
CONCENTRATION 10,000-50,000 ug/L
- DISSOLVED IRON (Fe)  
CONCENTRATION 50,000-100,000 ug/L
- DISSOLVED IRON (Fe)  
CONCENTRATION >100,000 ug/L
- 47'-390 DEPTH - DISSOLVED IRON (Fe)  
CONCENTRATION ug/L BASED ON  
GROUNDWATER PROFILING  
POINTS TERMINATED AT REFUSAL  
CONDITIONS/POSSIBLE BEDROCK

**FIGURE 15**  
**GEOLOGICAL CROSS SECTION D-D'**  
**DISSOLVED IRON (Fe) CONCENTRATIONS**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

MAP PREPARED 12/1/10.  
REV. 5-3-11

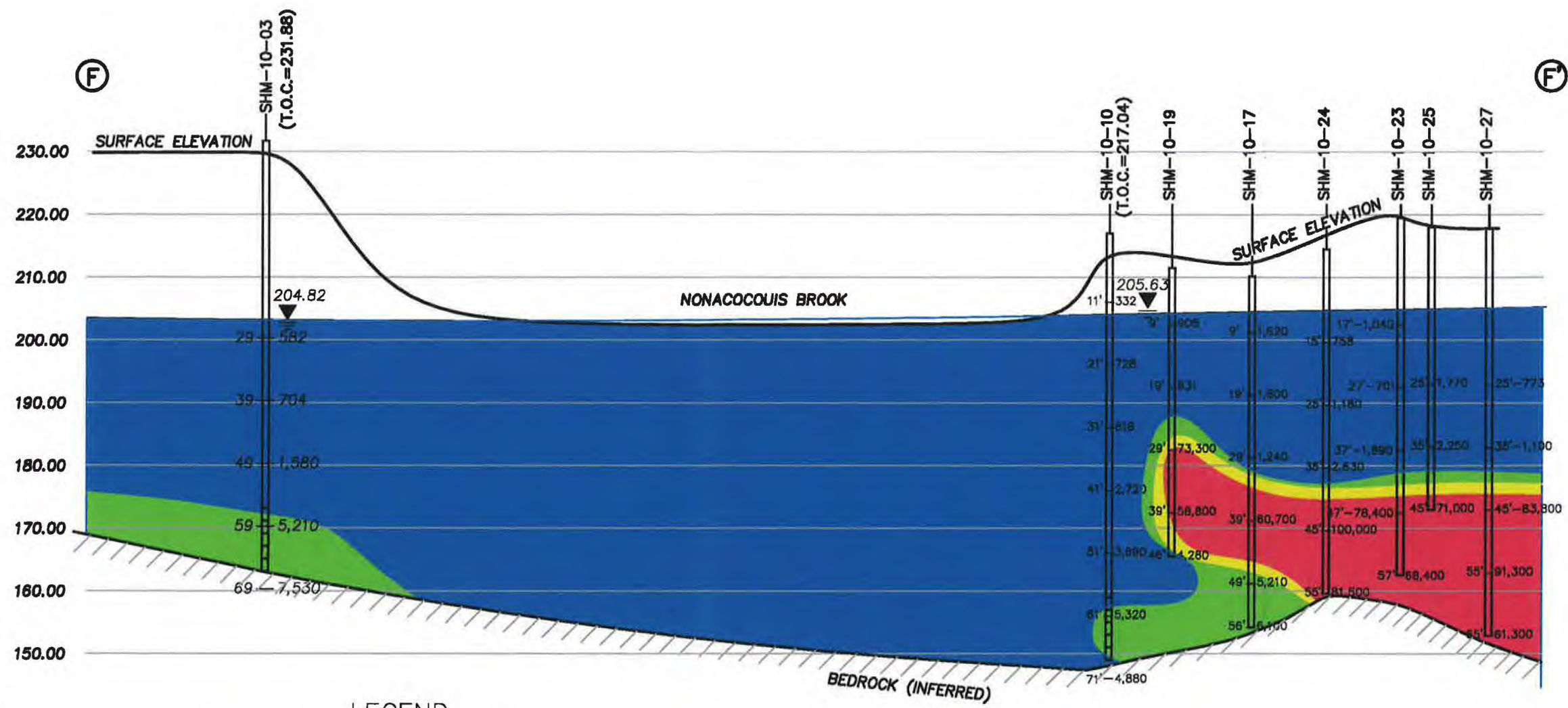
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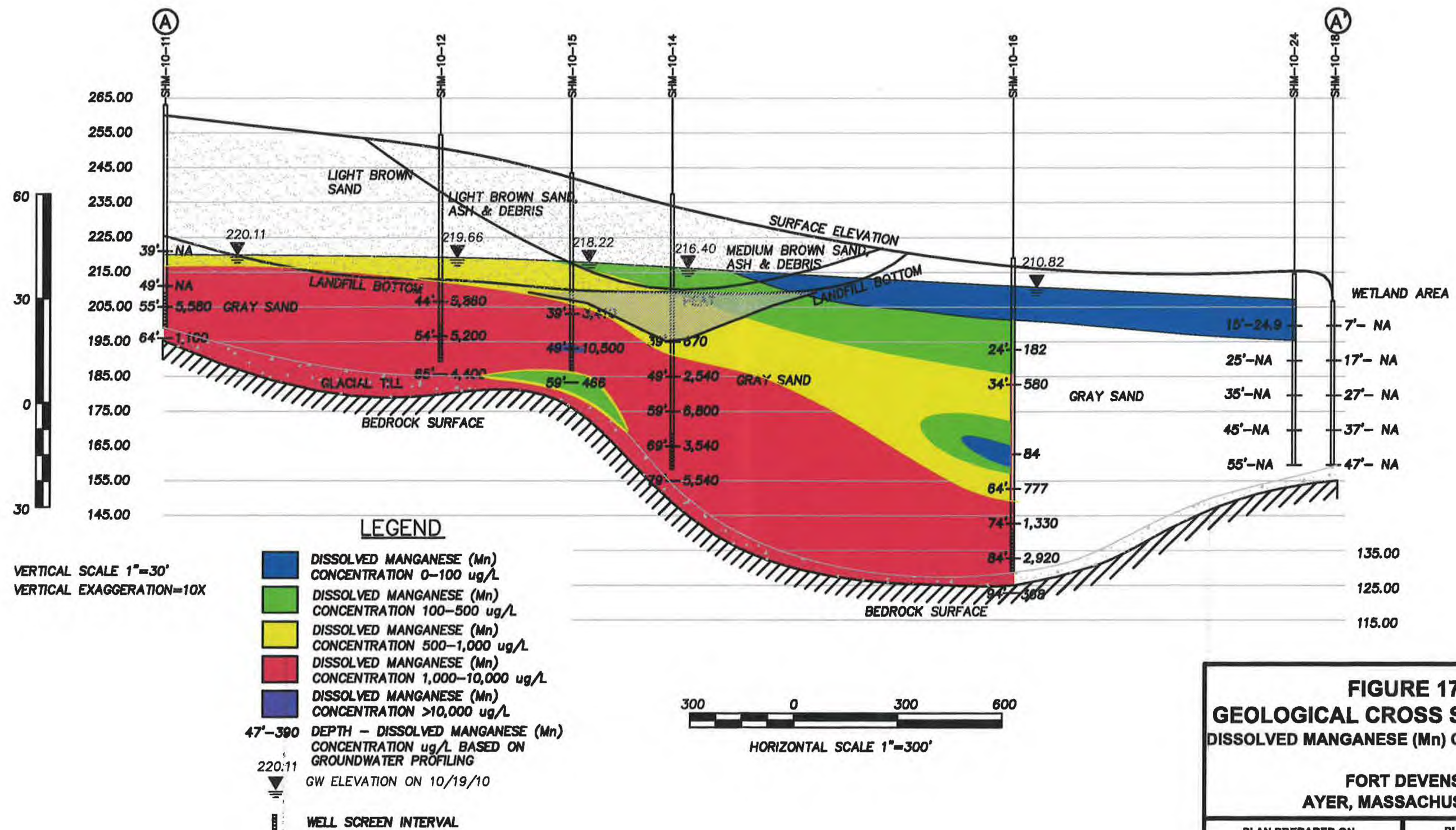
**FIGURE 16**  
**GEOLOGICAL CROSS SECTION F-F'**  
**DISSOLVED IRON (Fe) CONCENTRATIONS**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

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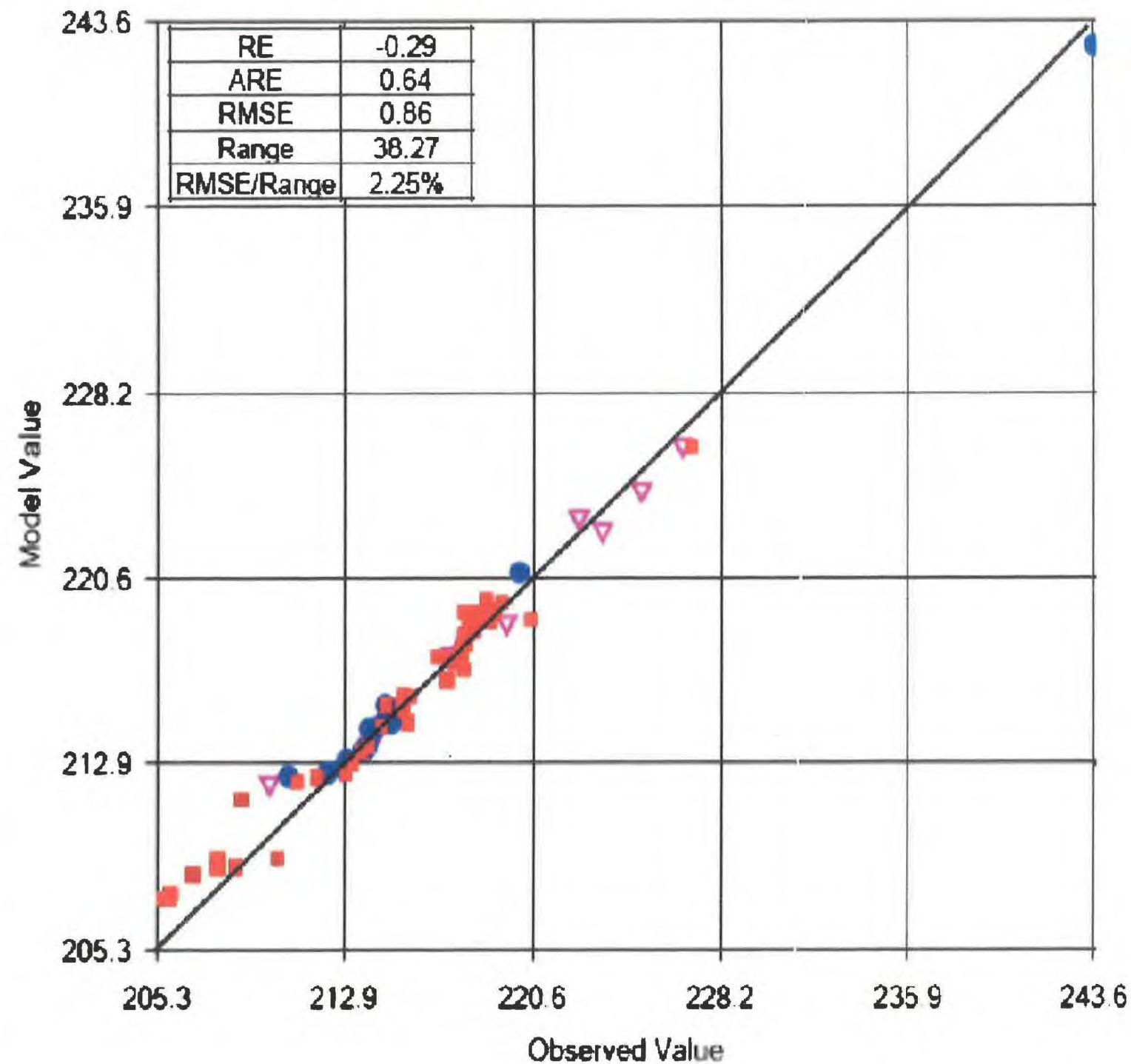
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Shepley's Hill Landfill  
Focused Feasibility Study  
Supplemental Hydrogeologic Assessment



- Model Layer 1
- Model Layer 2
- ▽ Model Layer 3

**FIGURE 31**  
**CORRELATION BETWEEN LONG TERM**  
**AVERAGE AND PREDICTED**  
**ELEVATIONS: SHL008**  
**FORT DEVENS**  
**AYER, MASSACHUSETTS**

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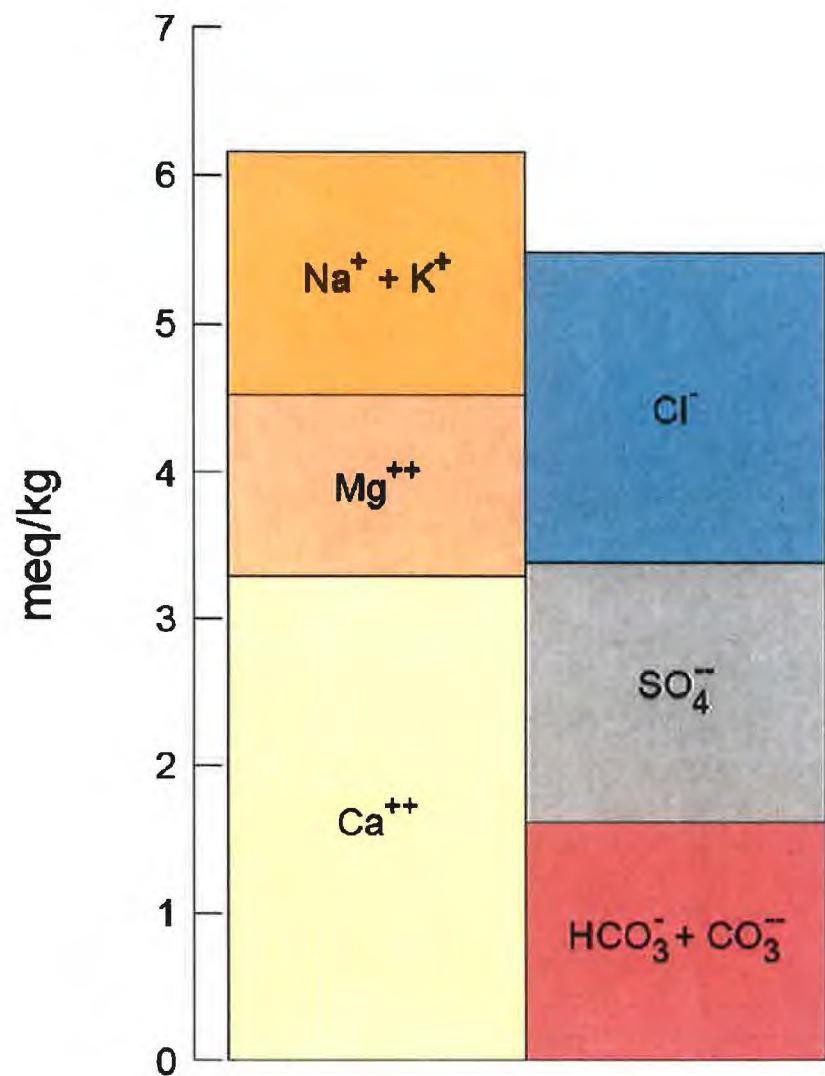




FIGURE  
33

**amec**





**FIGURE 34**  
**CATION-ANION BALANCE AND**  
**BICARBONATE IN SH-10-04**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

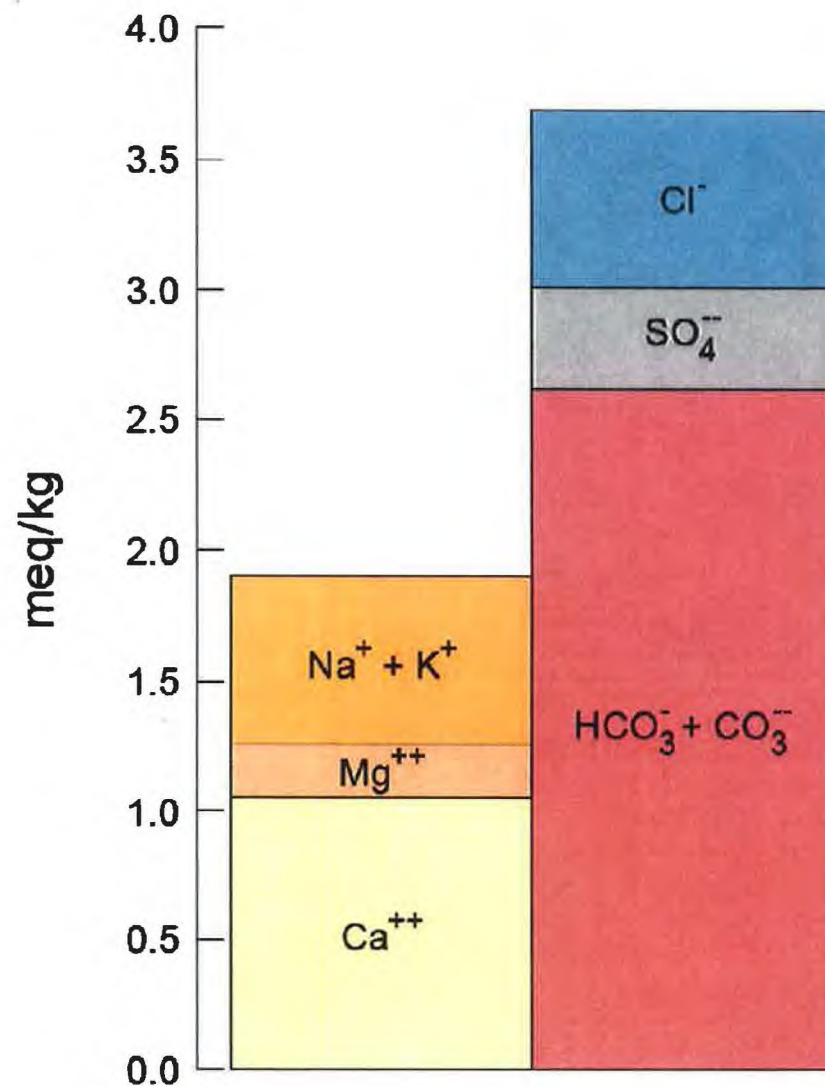
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**FIGURE 35**  
**CATION-ANION BALANCE AND**  
**BICARBONATE IN SH-10-11**

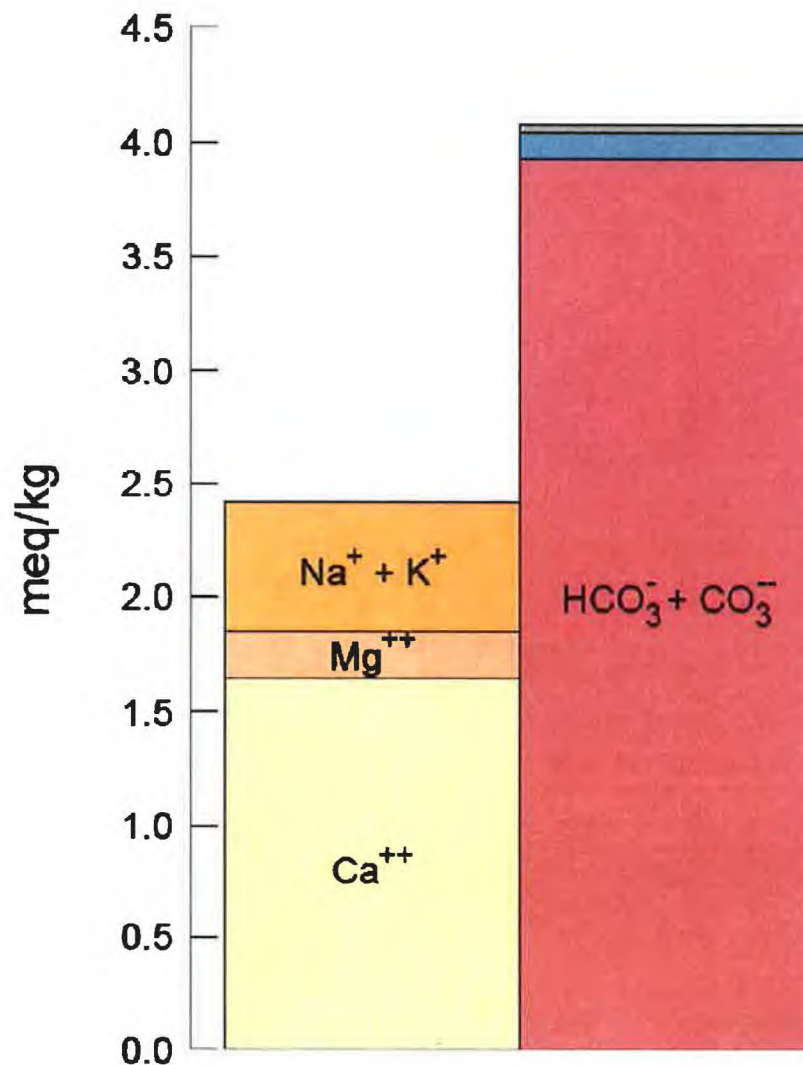
**FORT DEVENS**  
**AYER, MASSACHUSETTS**

PLAN PREPARED ON:  
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**FIGURE 36**  
**CATION-ANION BALANCE AND**  
**BICARBONATE IN SH-10-12**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

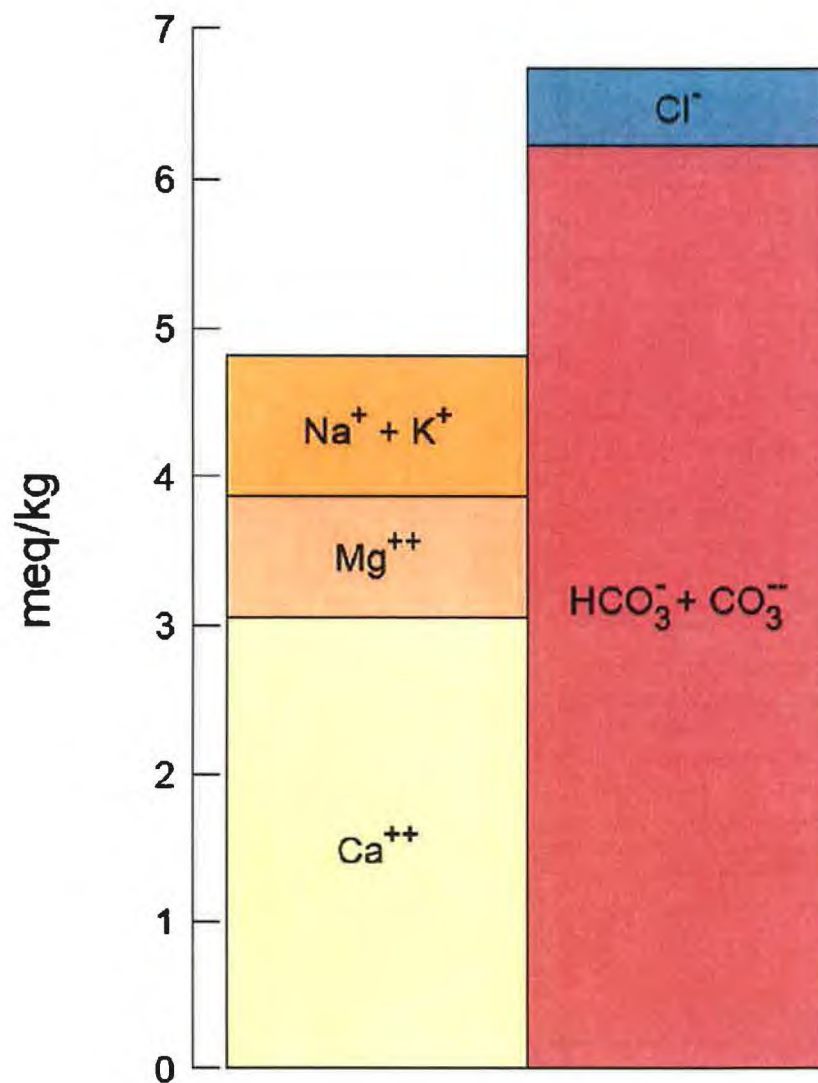
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**FIGURE 37**  
**CATION-ANION BALANCE AND**  
**BICARBONATE IN SH-10-13**

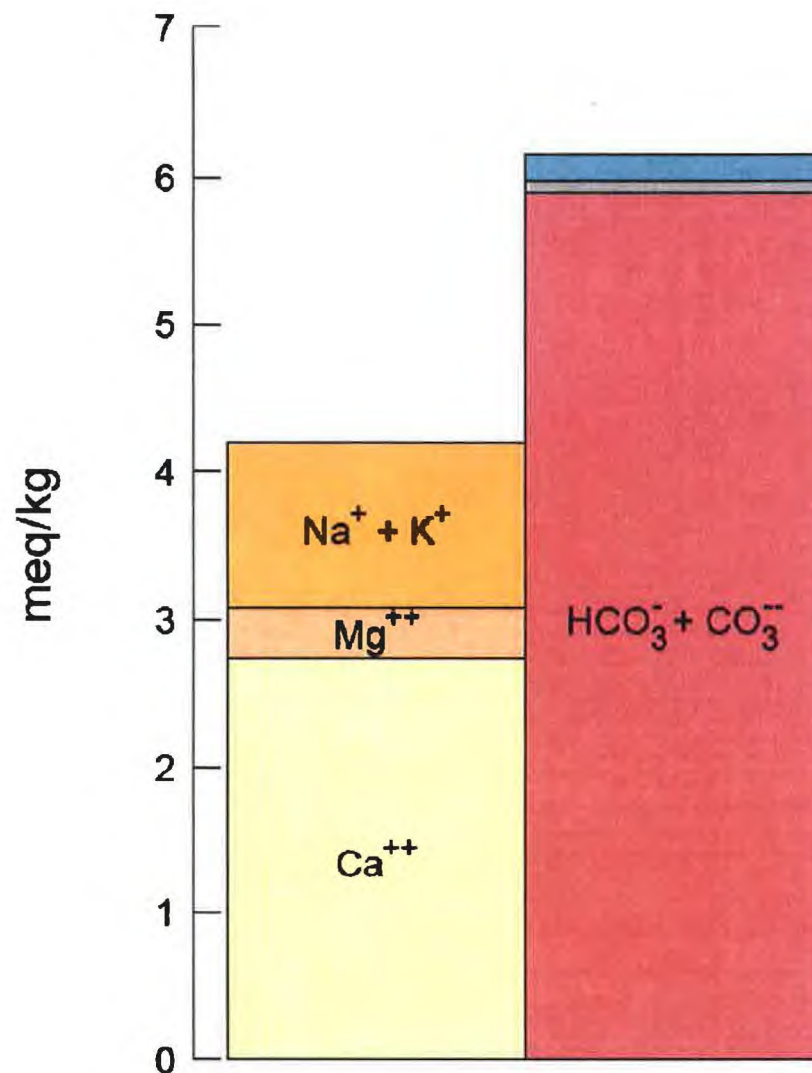
**FORT DEVENS**  
**AYER, MASSACHUSETTS**

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**FIGURE 38**  
**CATION-ANION BALANCE AND**  
**BICARBONATE IN SH-10-14**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

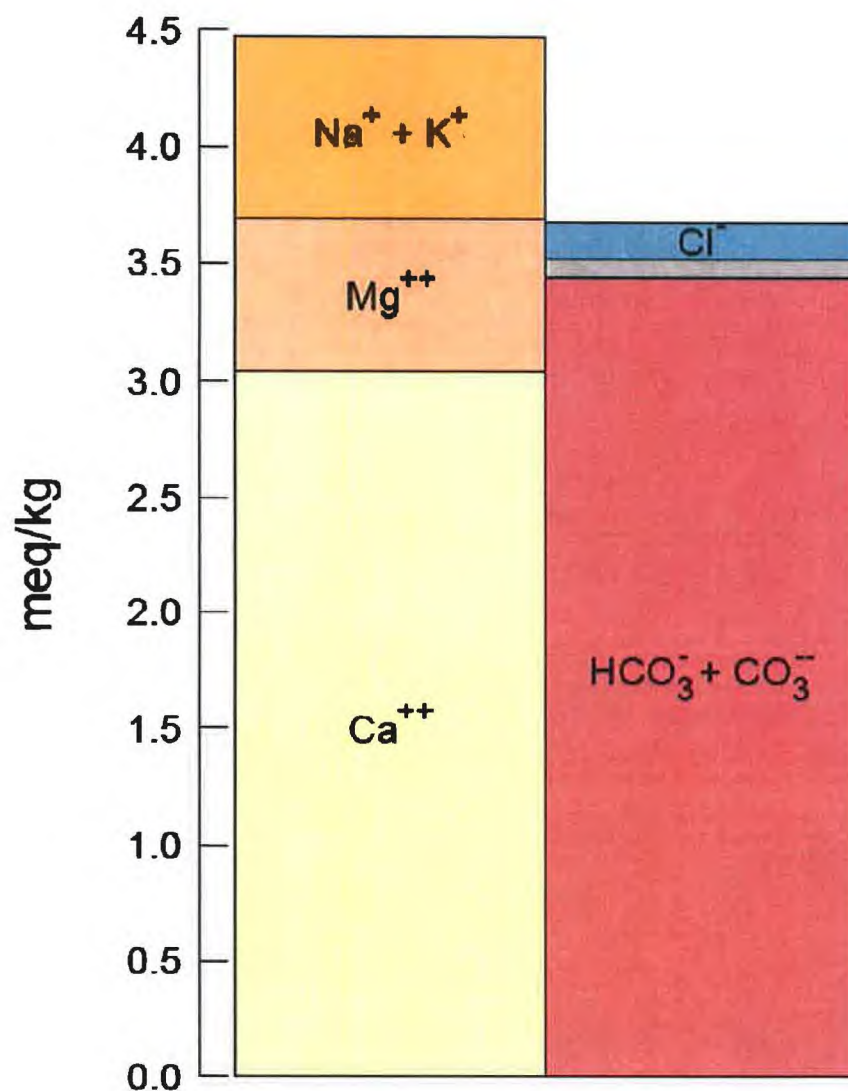
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**FIGURE 39**  
**CATION-ANION BALANCE AND**  
**BICARBONATE IN SH-10-15**

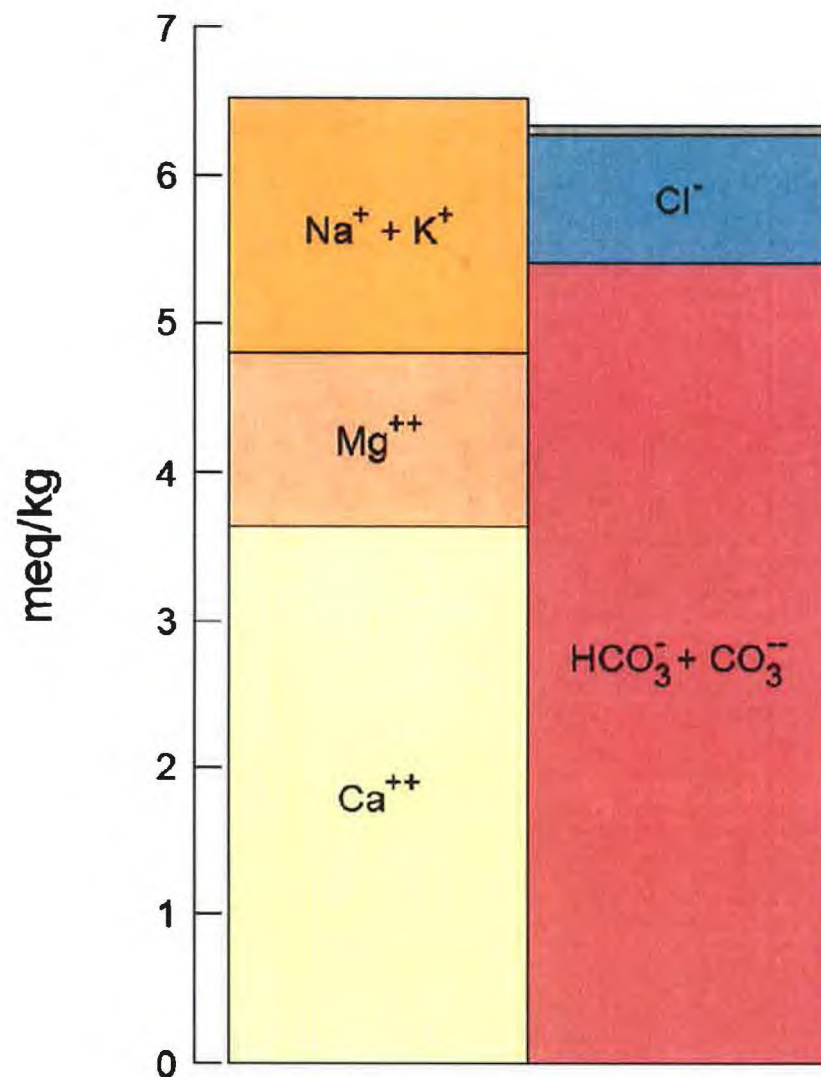
**FORT DEVENS**  
**AYER, MASSACHUSETTS**

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**FIGURE 40**  
**CATION-ANION BALANCE AND**  
**BICARBONATE IN SH-10-16**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

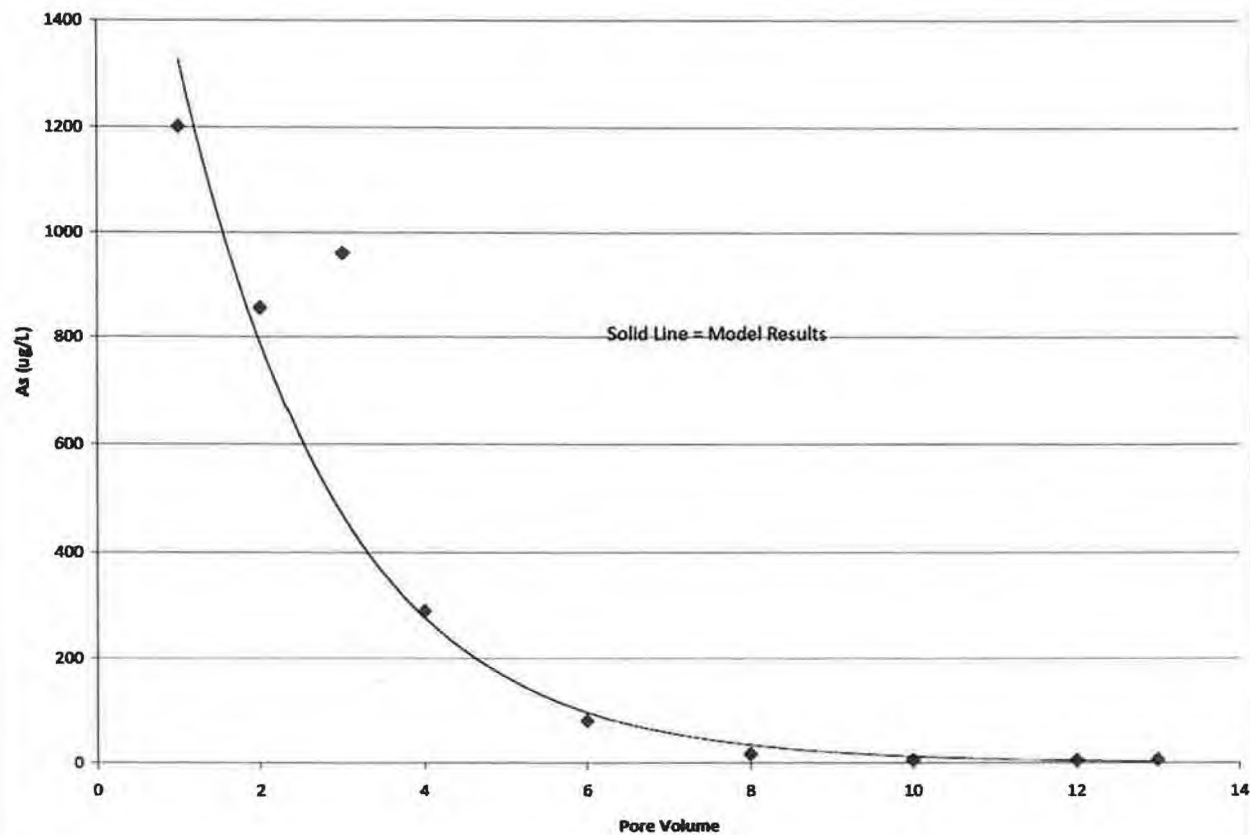
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**FIGURE 41**  
**ARSENIC IN COLUMN EFFLUENT**

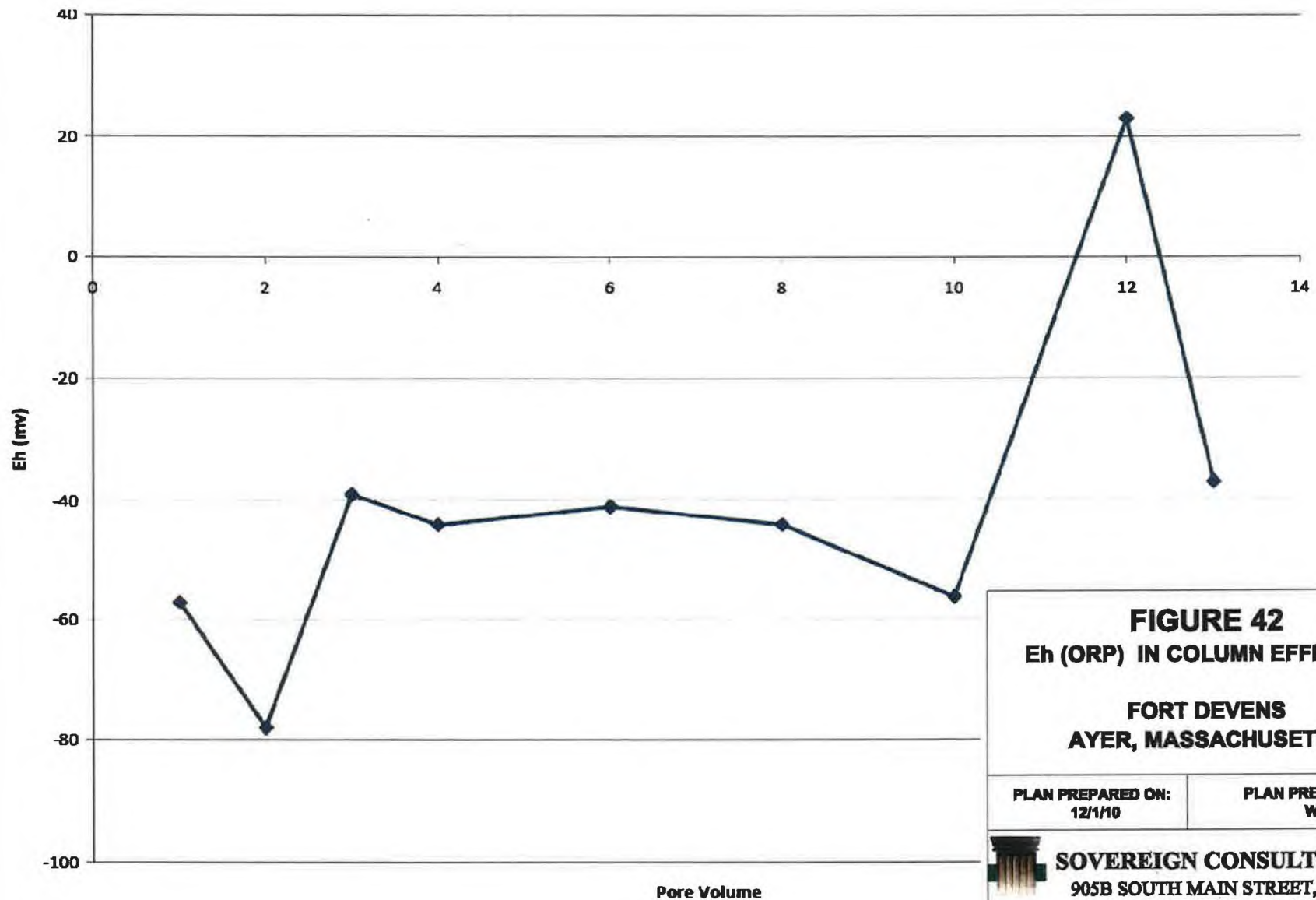
**FORT DEVENS**  
**AYER, MASSACHUSETTS**

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**FIGURE 42**  
**Eh (ORP) IN COLUMN EFFLUENT**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

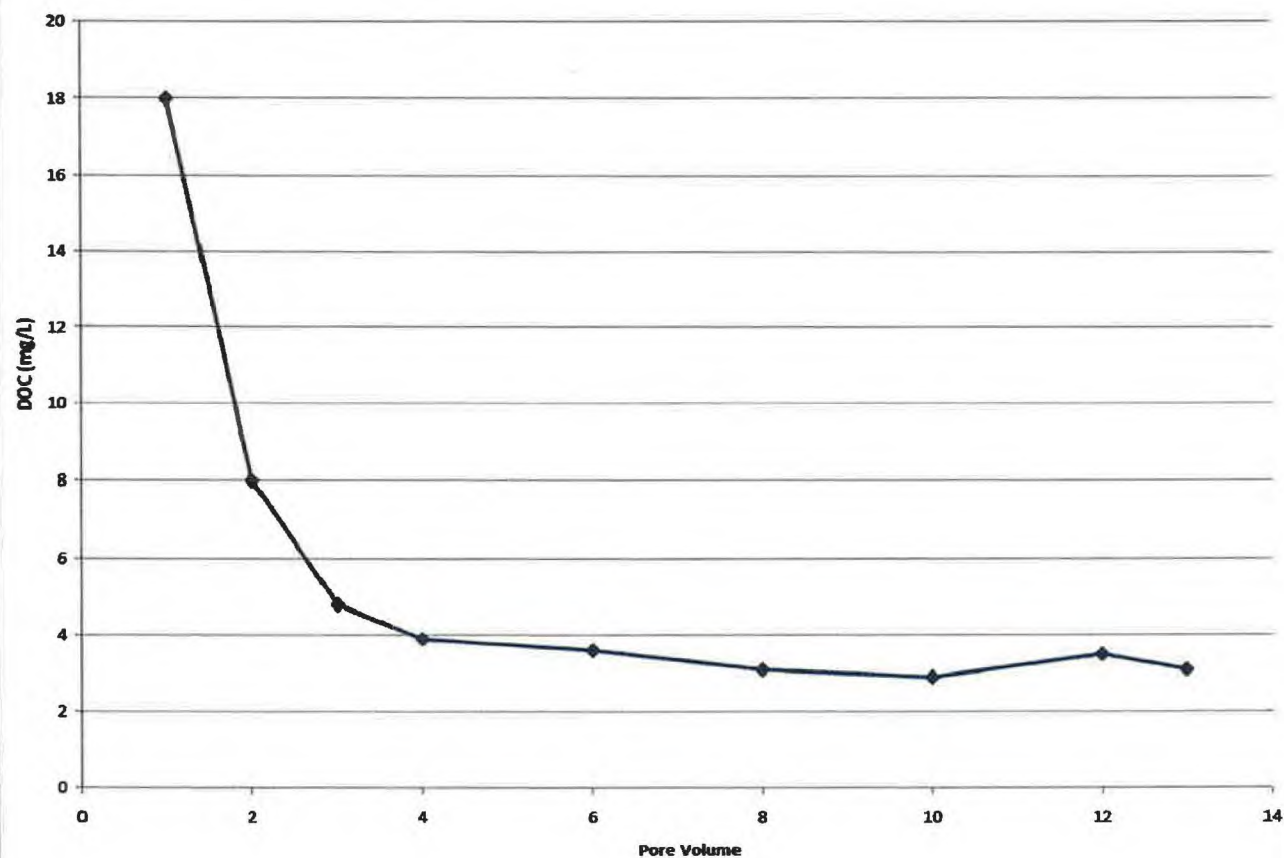
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**FIGURE 43**  
**DOC IN COLUMN EFFLUENT**

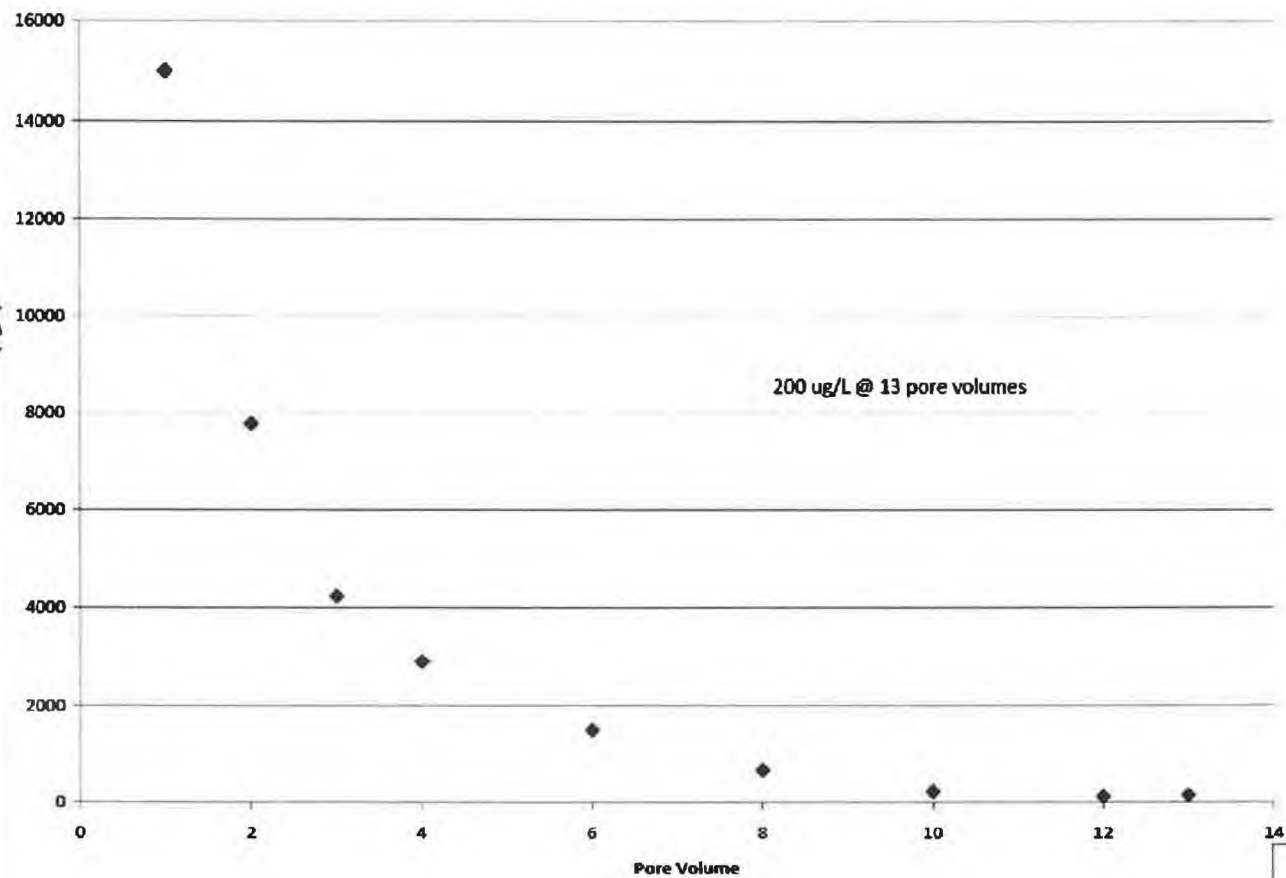
**FORT DEVENS**  
**AYER, MASSACHUSETTS**

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**FIGURE 44**  
**MODEL RESULTS FOR INITIAL**  
**CONCENTRATION OF**  
**15,000 ug/l ARSENIC**  
**FORT DEVENS**  
**AYER, MASSACHUSETTS**

PLAN PREPARED ON:  
12/1/10

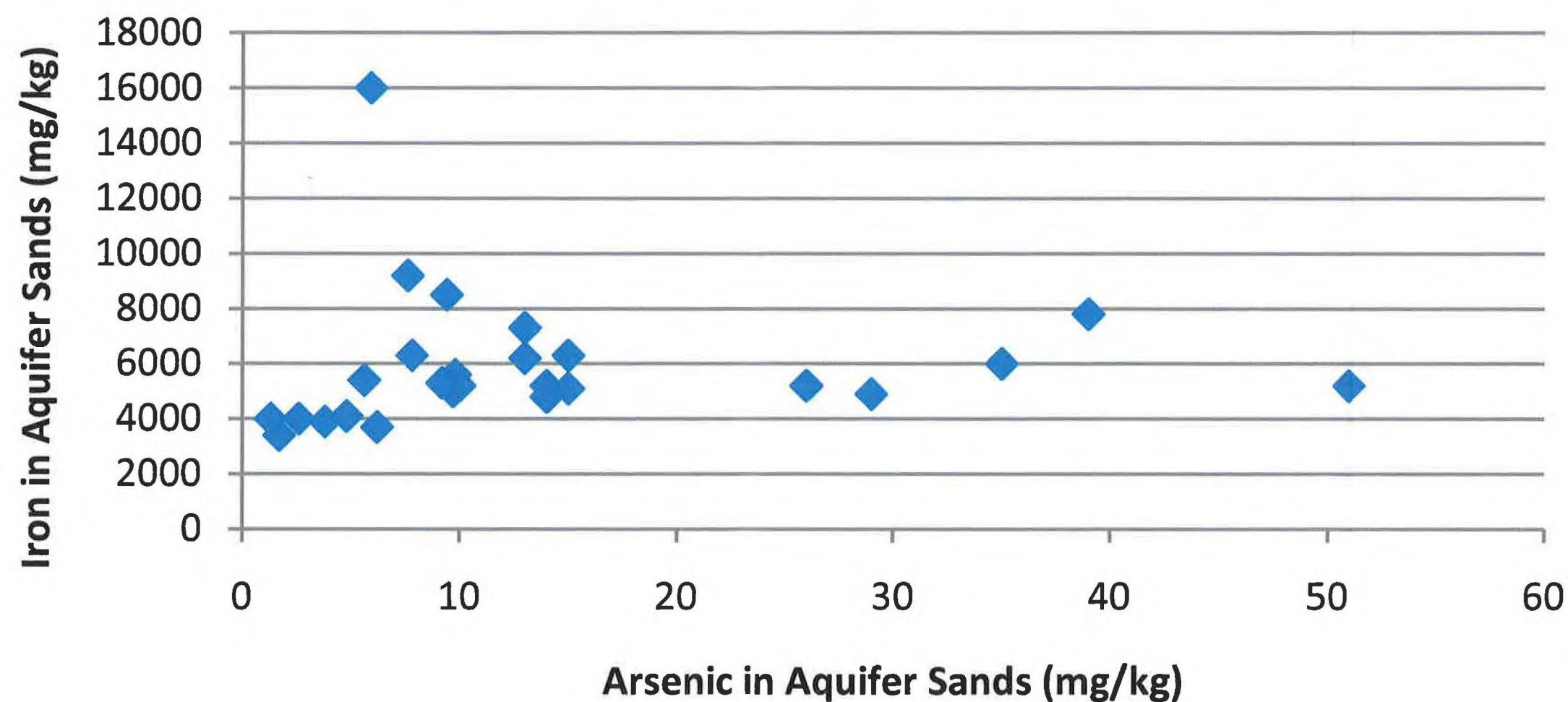
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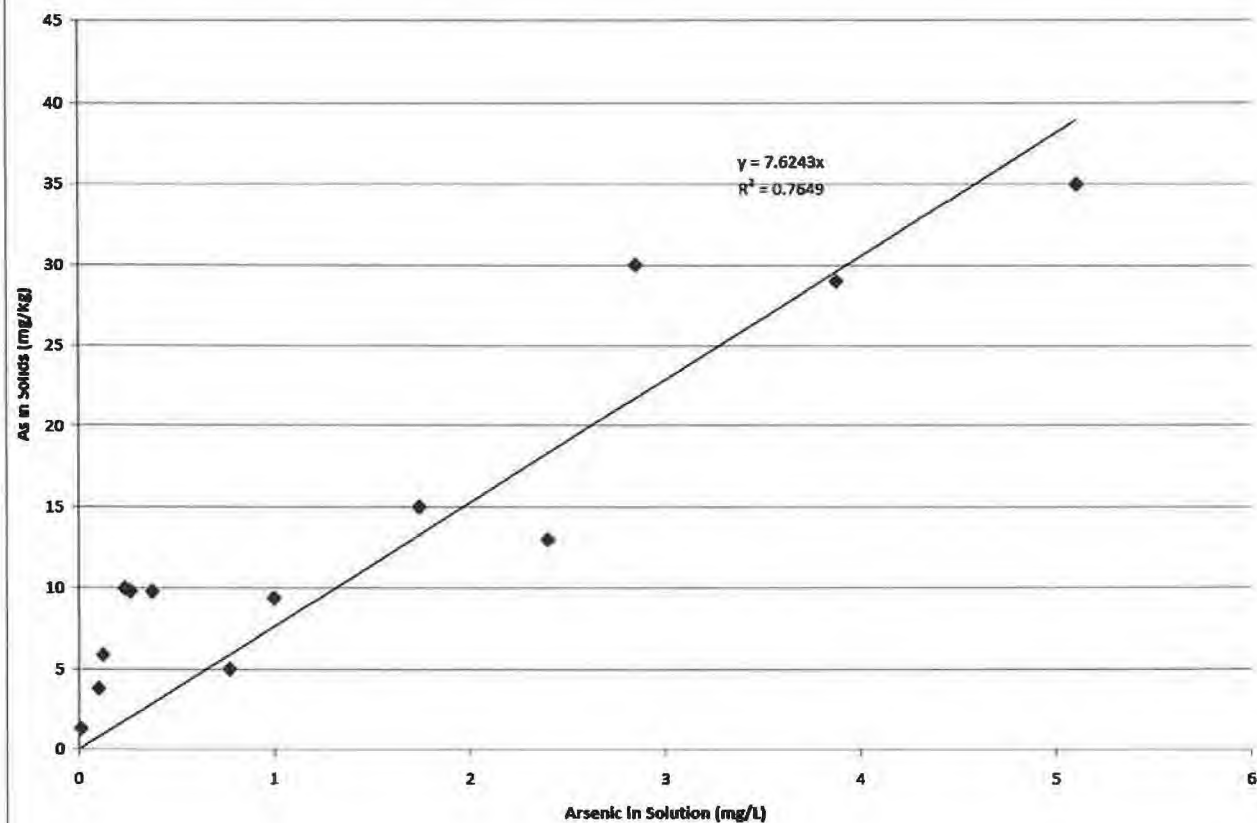


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**Figure 45. Arsenic vs. Iron in Aquifer Sands**





**FIGURE 46**  
**ARSENIC DISTRIBUTION IN SOLIDS**  
**VS SOLUTION (Kd=SLOPE OF LINE)**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

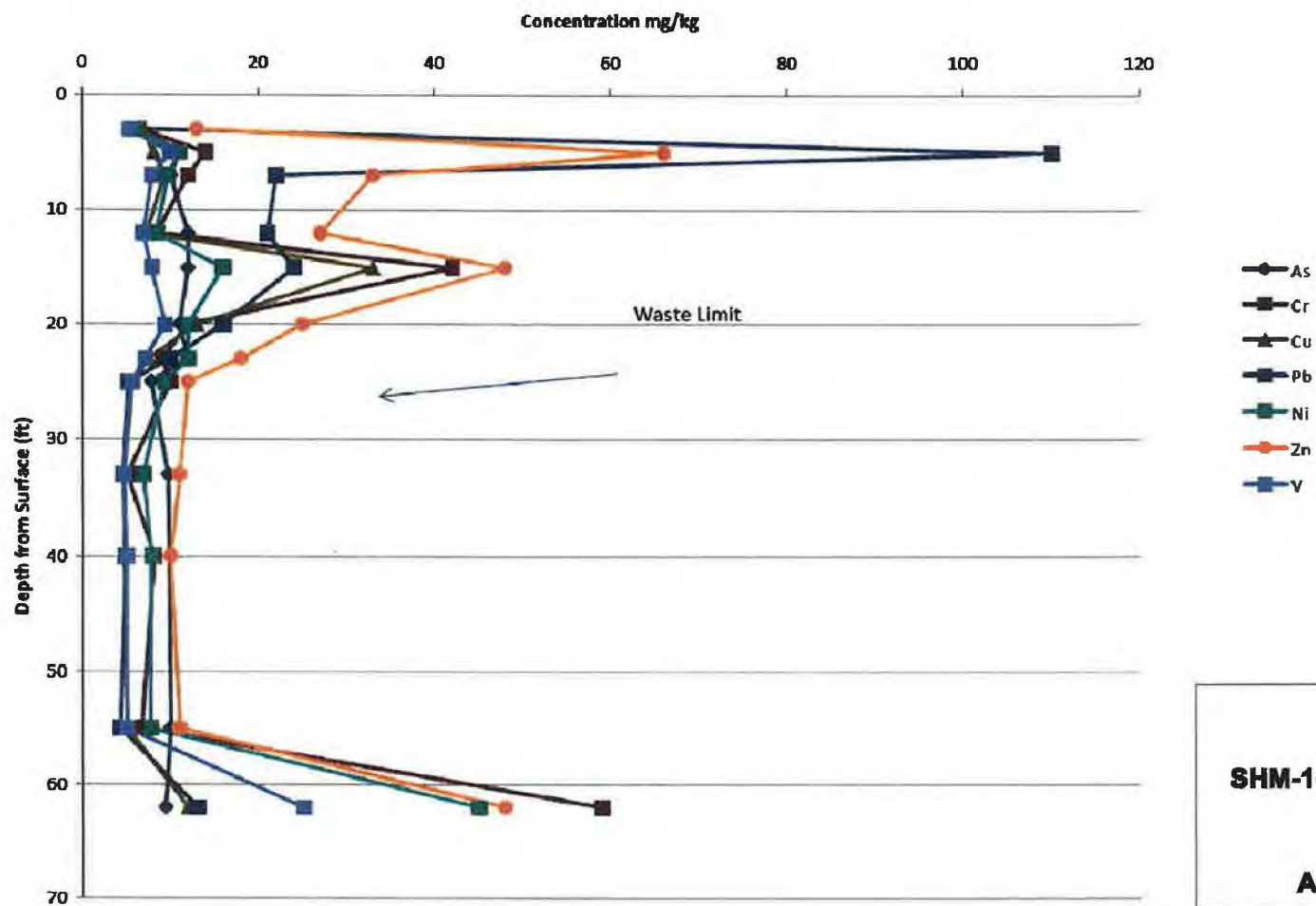
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**FIGURE 47**

**SHM-10-11 TRACE METAL PROFILE**

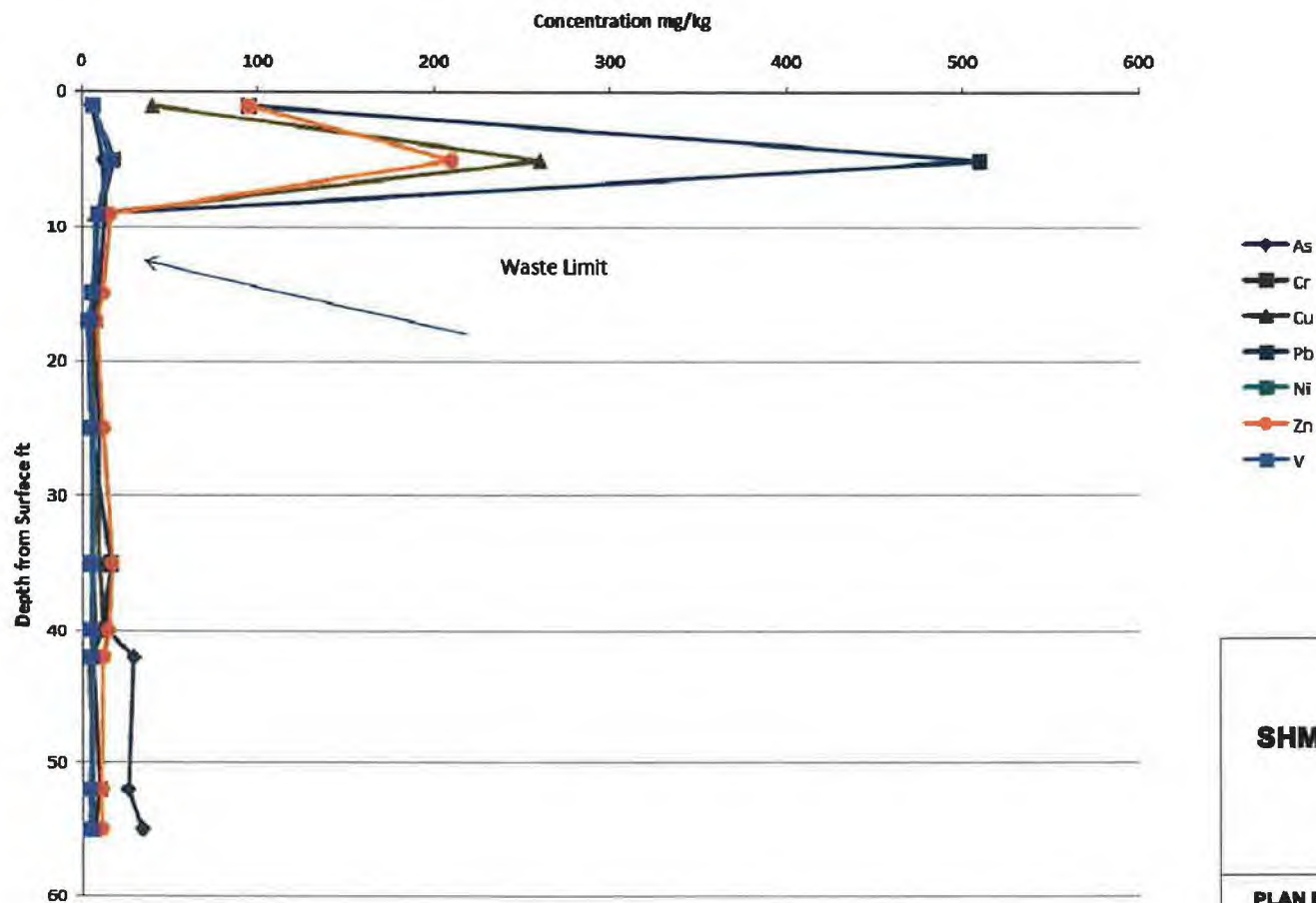
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**FIGURE 48**

**SHM-10-12 TRACE METAL PROFILE**

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AYER, MASSACHUSETTS**

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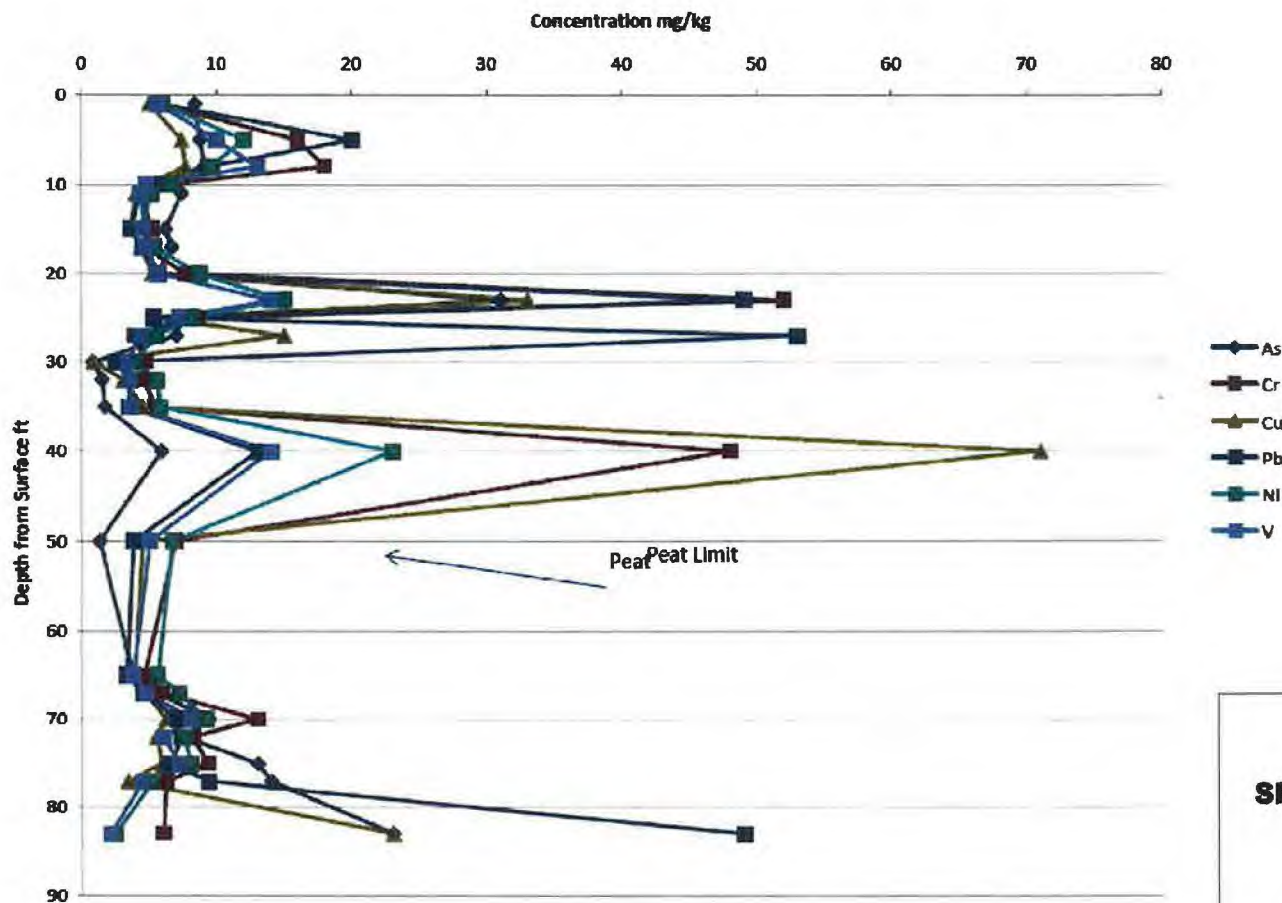
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**FIGURE 49**

**SHM-10-13 TRACE METAL PROFILE**

**FORT DEVENS  
AYER, MASSACHUSETTS**

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12/1/10

PLAN PREPARED BY:  
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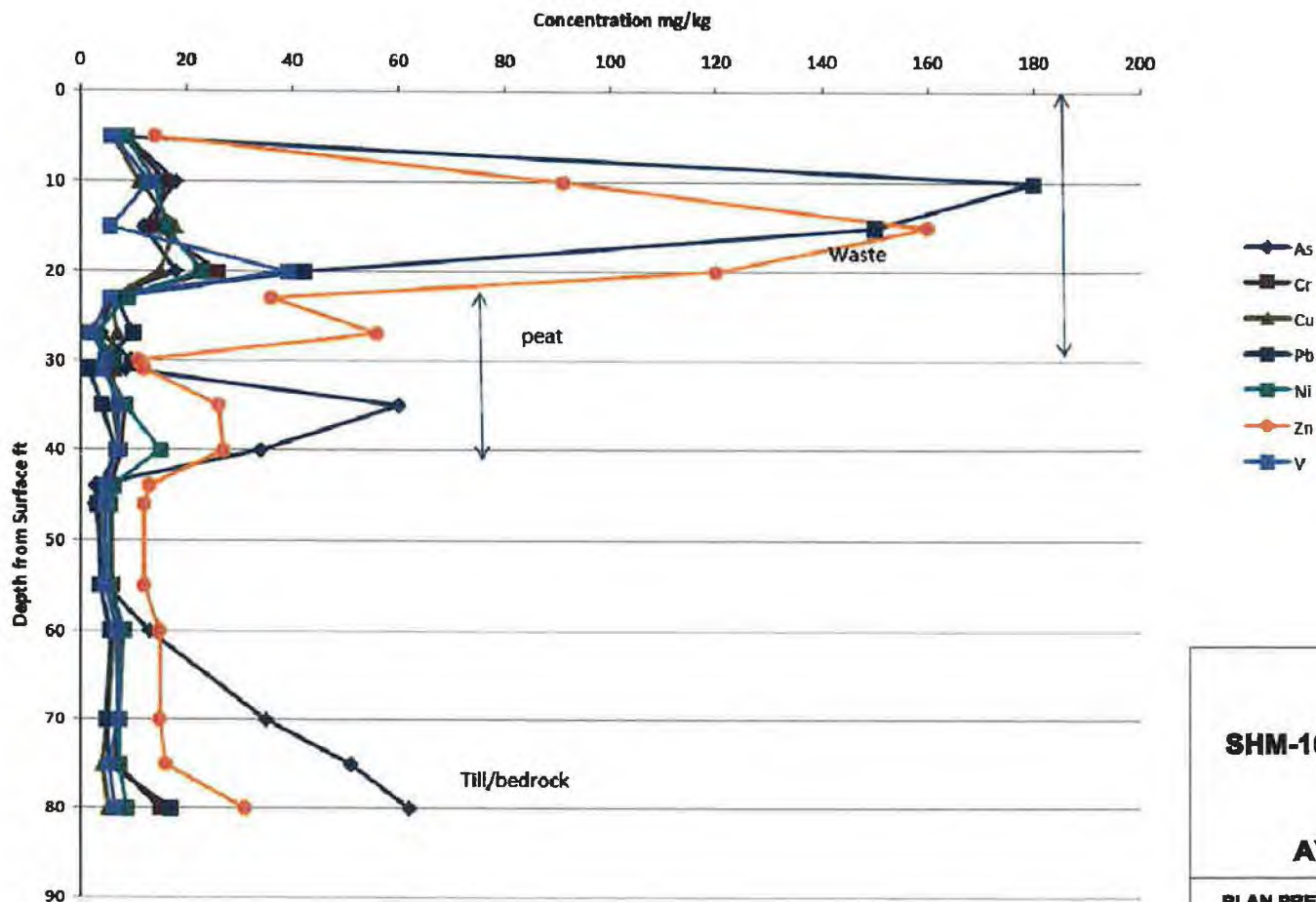
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**FIGURE 50**

**SHM-10-14 TRACE METAL PROFILE**

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AYER, MASSACHUSETTS**

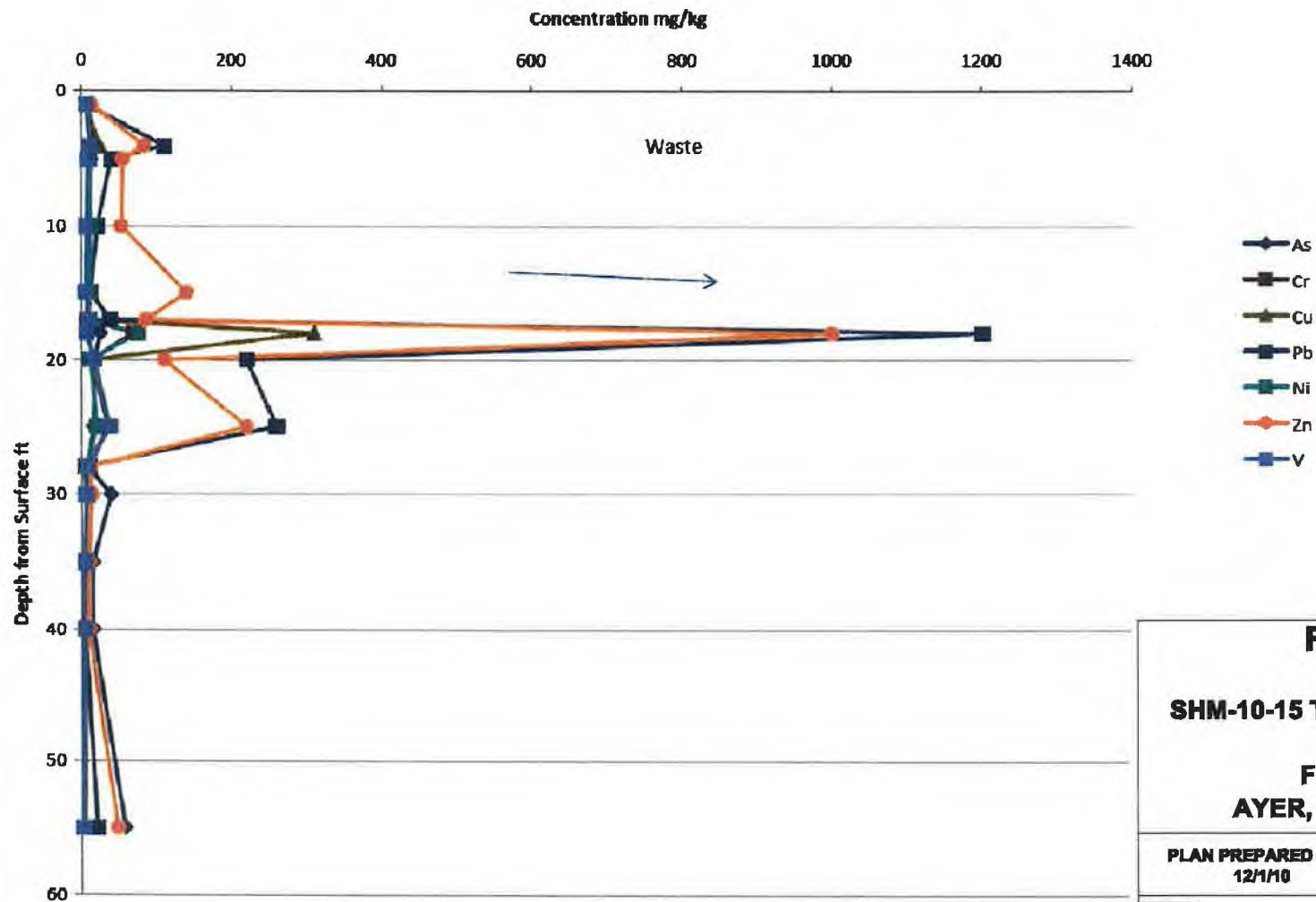
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**FIGURE 51**

**SHM-10-15 TRACE METAL PROFILE**

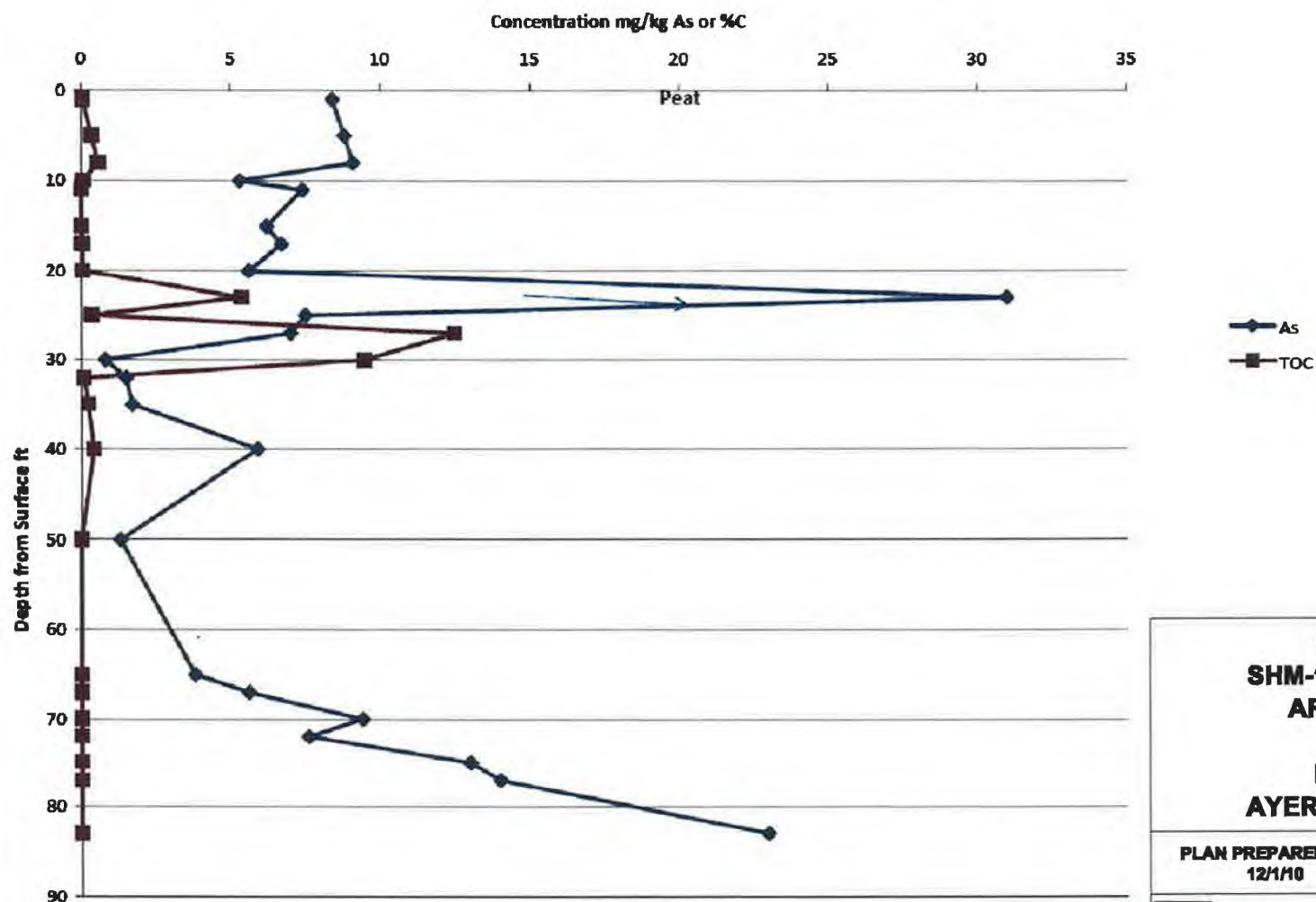
**FORT DEVENS  
AYER, MASSACHUSETTS**

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**FIGURE 52**  
**SHM-10-13 CARBON AND**  
**ARSENIC PROFILE**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

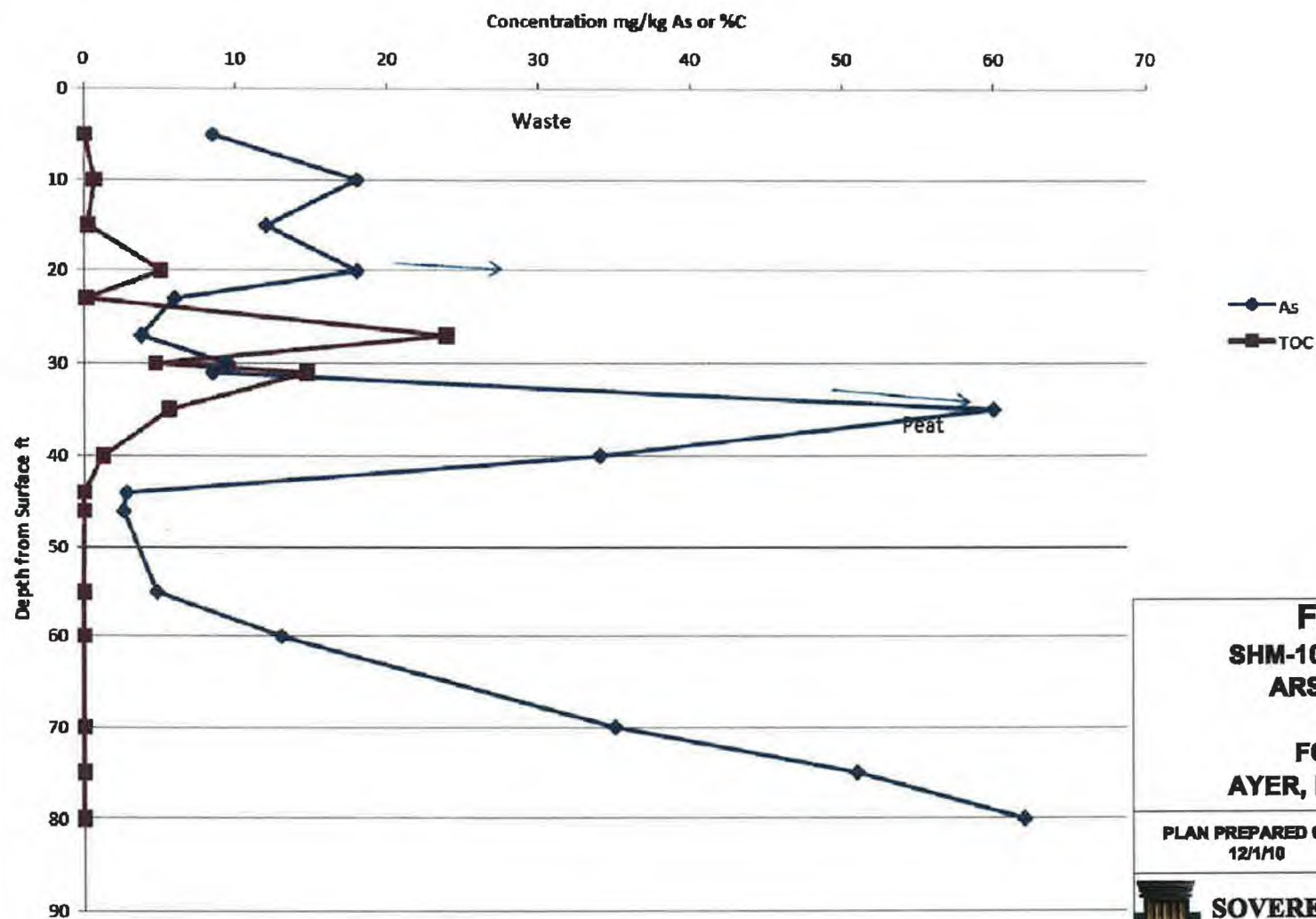
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**FIGURE 53**  
**SHM-10-14 CARBON AND**  
**ARSENIC PROFILE**

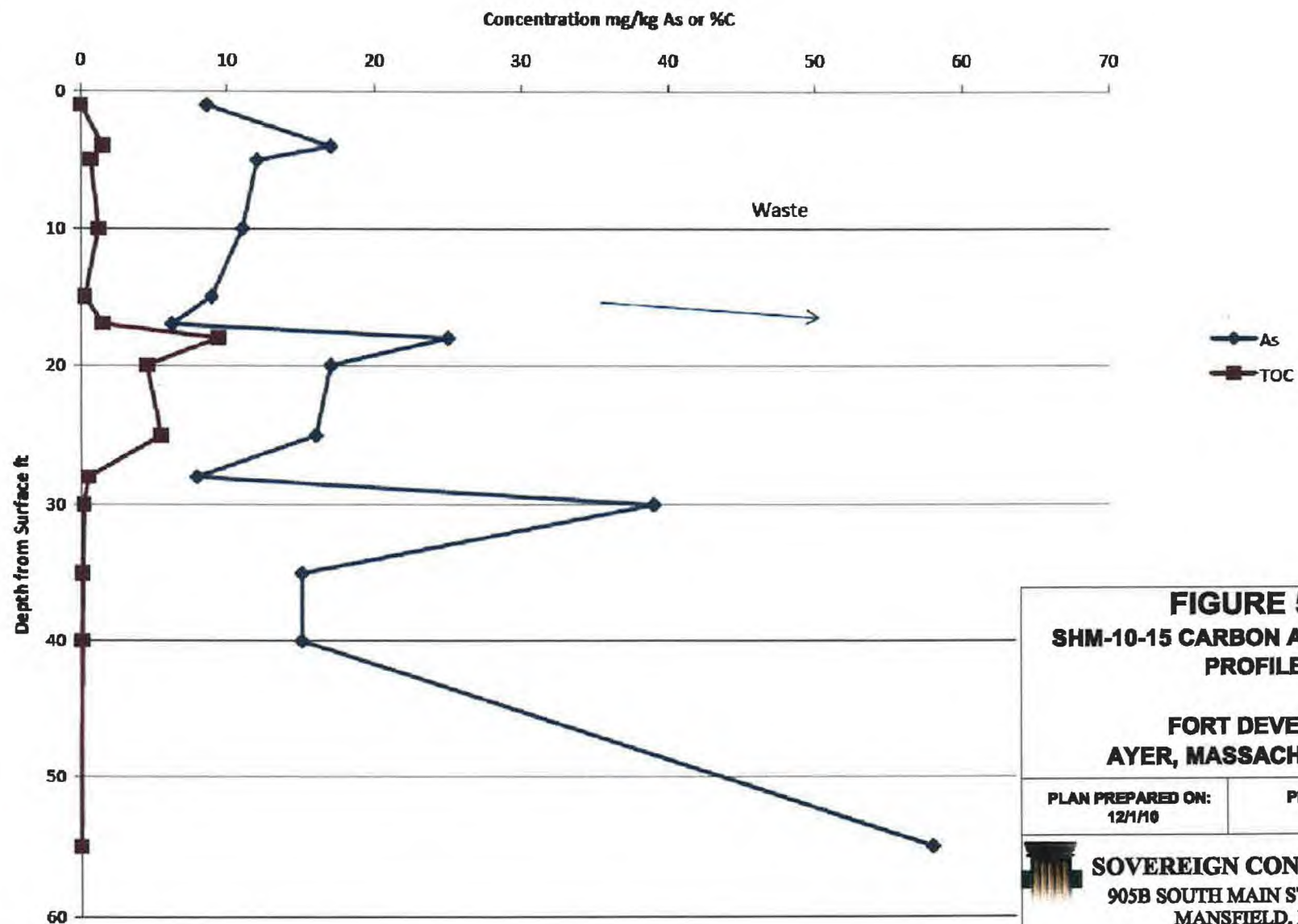
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**FIGURE 54**  
**SHM-10-15 CARBON AND ARSENIC**  
**PROFILE**

**FORT DEVENS**  
**AYER, MASSACHUSETTS**

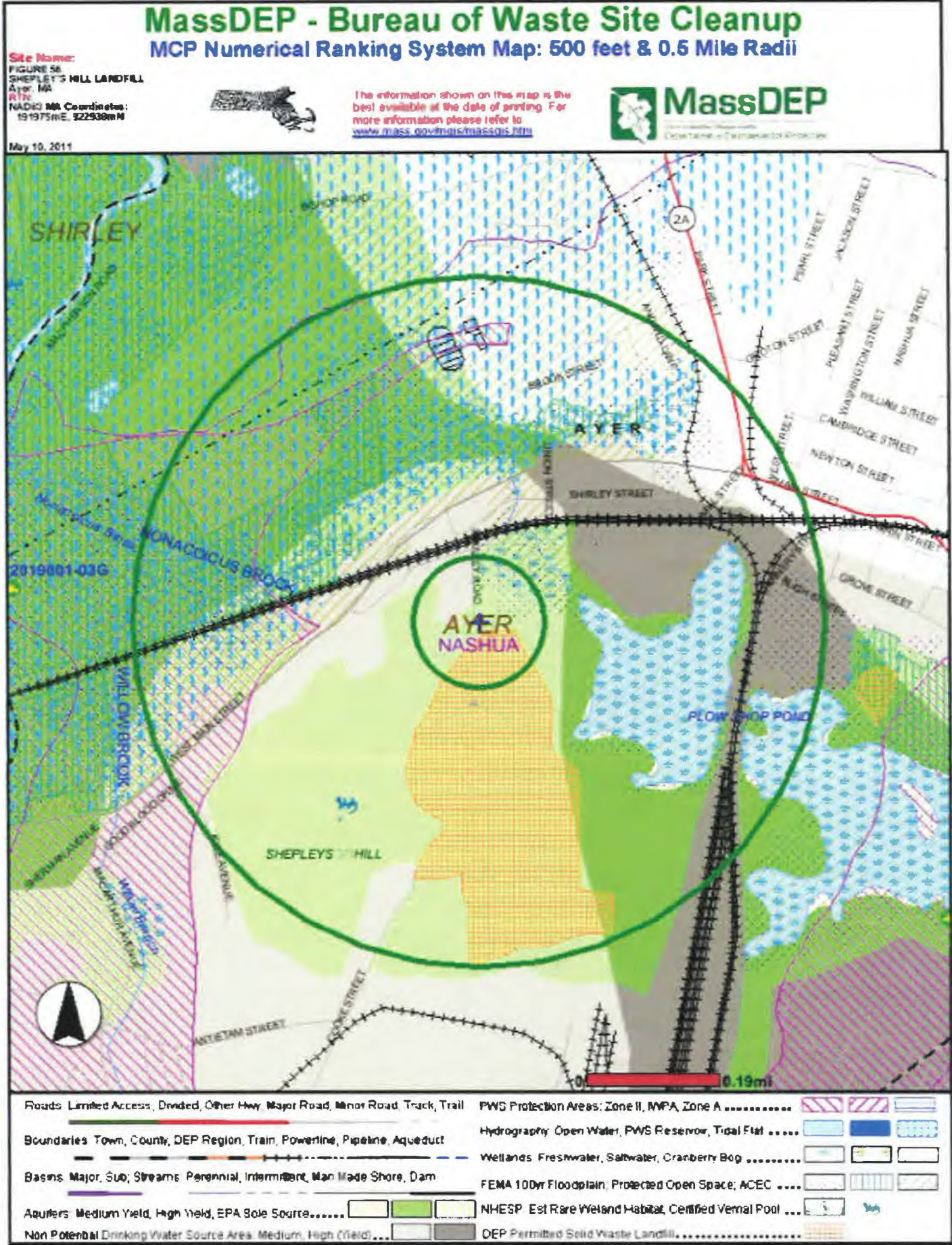
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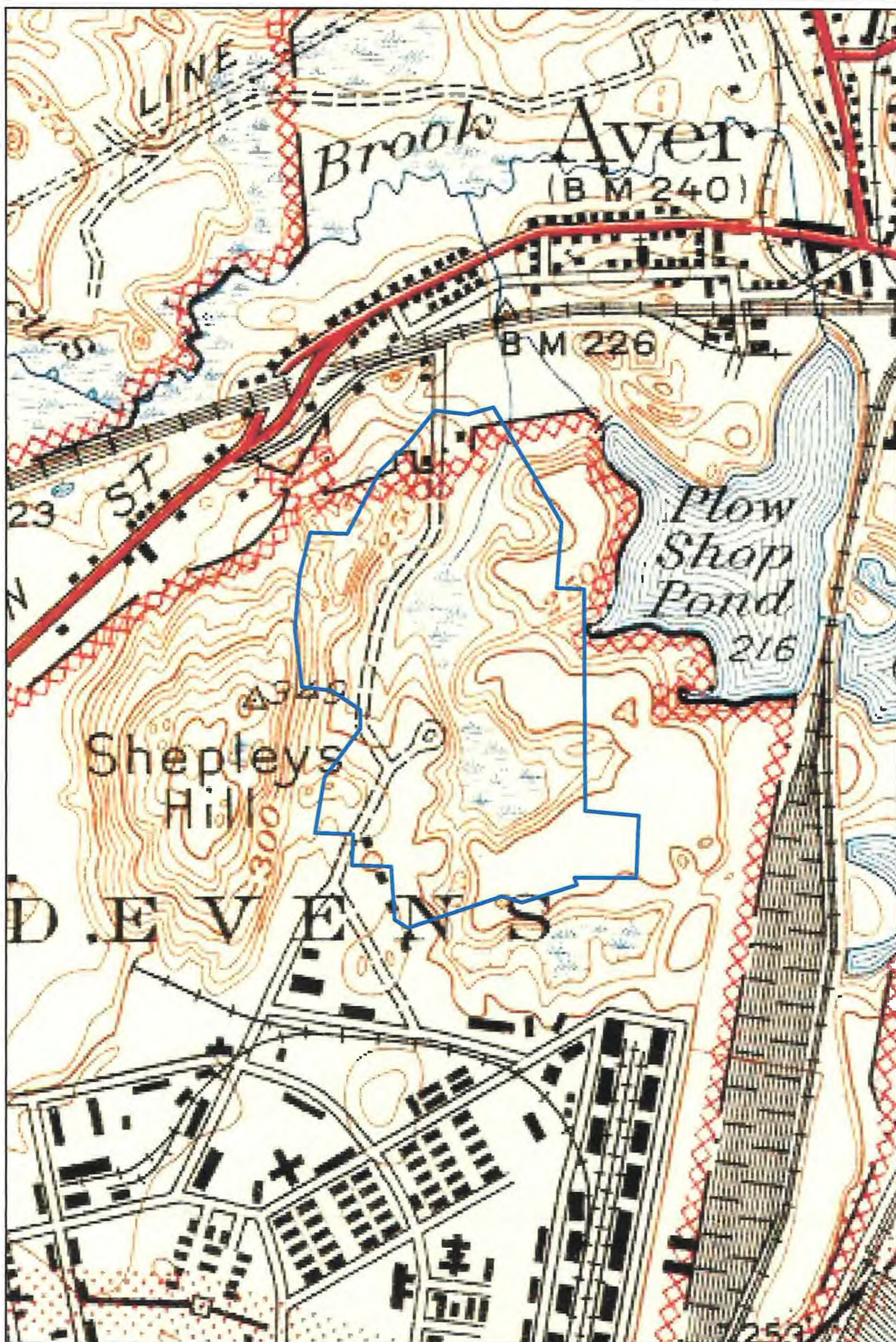
**FIGURE 56**  
**MASSACHUSETTS DEPARTMENT**  
**OF ENVIRONMENTAL PROTECTION**  
**PRIORITY RESOURCES (21E)**

FORT DEVENS  
 AYER, MASSACHUSETTS



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0 1,000  
Feet

APPROXIMATE SITE BOUNDARY

SOURCE INFORMATION:  
1944 AYER, MASSACHUSETTS QUADRANGLE, USGS 7.5 MINUTE SERIES.  
ACCESSED FROM UNIVERSITY OF NEW HAMPSHIRE DIAMOND  
LIBRARY IN MAY 2011 <<http://docs.unh.edu/nhkopos/Ayer7.5MA.htm>>

MAY 2011 ROV

# FIGURE 57 HISTORICAL TOPOGRAPHIC MAP



FORT DEVENS  
AYER, MASSACHUSETTS



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NOTES:  
CONTOUR INTERVAL EQUALS 10'  
DATUM IS MEAN SEA LEVEL  
TOPOGRAPHIC MAP SURVEYED IN 1923 AND 1935 AND  
REVISED IN 1944



**TABLE 1**  
**Technical Objective and Approach for Data Collection**  
**Shepley's Hill Landfill, Devens, Massachusetts**

Objective	Hypothesis	Data Gaps	Technical Approach
<b>From EPA Additional Work Letter</b>			
<b>North Plume Delineation &amp; Monitoring for Impacted Area</b> Delineate the north plume in all directions to depth in order to establish final delineated plume boundaries.  Install additional monitoring wells to be incorporated into the long-term monitoring program that will ensure that there are permanent monitoring locations for all significant areas of the plume (e.g., West Main Street) and to serve as sentry wells to ensure that the plume does not migrate further beyond the final delineated plume boundaries. Incorporate these wells into a revised long-term monitoring plan.	<p>The plume north of the capture zone has stable limits bounded by bedrock and advective flow of unimpacted or oxygenated groundwater (GW).</p> <p>The plume limits in the area of Mohimco Rd are near SHM-07-03 on the west and SHM-99-32X on the east; in the area of West Main St are west of DEP-08-03 and near DEP-08-08 on the east; and in the area of Nonacicus Brook are southwest of DEP-08-07 (See Figure 1).</p>	<p>GW chemistry data above, below, and lateral to the plume in the following general areas:</p> <ul style="list-style-type: none"> <li>• West Main St west of DEP-08-03</li> <li>• Nonacicus Brook north west of DEP-08-05 and southwest of DEP-08-07</li> <li>• North of the brook, NE of DEP-08-07</li> <li>• East of SHX-01-06X</li> </ul>	<p>Install borings extending to bedrock in each area and collect GW samples at 10-ft intervals for arsenic and field parameters. Complete permanent wells based on profile results and sample twice for metals. Map plume in 3D based on the results</p>
2a. North Plume Capture at Boundary Operate and/or modify the treatment system to contain the arsenic plume in the vicinity of the base boundary near the north end of the landfill and demonstrate that the arsenic plume is captured.	The latest revised GW model and other lines of evidence as presented in the 2008 Annual Report (ECC 2009) suggest that impacted GW at the toe of the landfill is fully contained, subject to some uncertainty on the eastern plume extent at the toe	GW chemistry data east of the toe of the landfill, in the area east of SHM-96-5B.	Install boring(s) extending to bedrock and collect GW samples at 10-ft intervals for metals and field parameters. Complete permanent well(s) based on profile results and sample twice for metals.
2b. North Plume Monitored Natural Attenuation (MNA) for the Impacted Area Once capture is demonstrated, establish that monitored natural attenuation will be effective at remediating the north plume (i.e., the Impacted Area) within a timeframe that is reasonable given the circumstances of the site	MNA in the Impacted Area will be effective based on immobilization of dissolved arsenic. Effectiveness depends on: (1) demonstration of a static or shrinking plume (see objective #1); (2) determining rates and mechanisms of attenuation; (3) determining stability of immobilized arsenic; and (4) establishing a monitoring plan and contingency plans (USEPA 2007). The time required for arsenic to be immobilized in the Impacted Area by MNA or by an aggressive remedy are both decades or longer.	Aquifer mineralogy and association of arsenic with the various solid phase components. Time to achieve MCLs due to flushing with unimpacted GW, both for MNA and aggressive (FFS Alternative 3B) scenarios.	Collect co-located soil and GW samples from the Impacted Area for chemical and microscopic-spectroscopic analysis of solids. Conduct flushing timeframe study similar to USGS Saco Landfill study; test cores of aquifer material from the Impacted Area and use reaction model to simulate immobilization.
3. Landfill Gas Impacts Complete an evaluation of landfill gas impacts in the area of the north plume (i.e., the Impacted Area) in accordance with the EPA Guidance for Evaluating Landfill Gas Emissions from Closed or Abandoned Facilities to ensure that methane emanating from the landfill will not cause unacceptable risks (i.e., explosive conditions) in nearby structures.	Results of monitoring perimeter soil gas probes at the north end of the landfill indicate that methane is not migrating offsite laterally through soil. Offsite structures in the Impacted Area north of the capture zone may have methane intrusion from groundwater if sufficient levels of methane volatilize from the top of the water table and migrate through the vadose zone.	None at this time.	Conduct vapor intrusion modeling based on conservative estimates of site conditions. Discuss results and need for site-specific measurements with BCT.
4. East Plume Delineation and Capture Eliminate the continuing discharge of high-arsenic groundwater to Plow Shop Pond sediments. It is expected that new groundwater monitoring wells, as recommended in EPA's October 2, 2008 letter and in Section 5.3 of ORD's Final Report, will be completed and data from these wells will be considered in this effort.	Discharge of shallow arsenic impacted groundwater from the eastern portion of the landfill to Red Cove may be controlled using GW injection, extraction, or in-situ treatment.	Arsenic GW concentrations and flow rates between SHL and Red Cove.	Update GW model based on pond flux measurements and use model for citing wells upgradient of Red Cove. Install borings extending to bedrock and collect GW samples at 10-ft intervals for metals and field parameters. Complete permanent well(s) based on profile results and sample twice for metals.
<b>From 9/30/09 Draft FFS:</b>			
5. Arsenic Source Strength Estimate the arsenic source strength and duration, including the quantity of arsenic that may be mobilized and the strength and duration of sources of reducing conditions.	Potential sources of arsenic in groundwater include bedrock, bedrock-derived soils, and landfill wastes, which are located above and below the water table. Arsenic is dissolved from the source materials by landfill-induced reducing conditions in groundwater. A portion of the landfill overlies a swamp where naturally-occurring reducing conditions may also have existed.	Aquifer mineralogy and association of arsenic with the various solid phase components. Time to deplete source materials due to mobilization.	Collect co-located solid and GW samples from source materials for chemical and microscopic-spectroscopic analysis of solids. Conduct flushing timeframe study; test cores of source material using reduced groundwater to simulate mobilization of metals.

Objective	Hypothesis	Data Gaps	Technical Approach
6. Air Sparging Feasibility: Evaluate implementability of a horizontal sparging well installation (FES Alternative 4) based on geologic conditions and arsenic distribution.	Air sparging may be feasible for immobilization of arsenic in groundwater flow from the landfill eastward into Red Cove.	Treatment system configuration and impacts of immobilized metals on local GW flow.	Develop a pilot test of air sparging between the landfill and Red Cove.
7. Floc Removal Feasibility: Evaluate implementability, conceptual design, and costs of floc removal in Red Cove (FES Alternative 2).	Arsenic-bearing floc accumulating in Red Cove sediments may be removed or sequestered to reduce risks to ecological receptors. The FES alternative incorporating this remedy assumes that the source of floc is continuing.	None at this time.	Evaluate floc removal remedies in the AOC 72 FSSR.
8. Landfill Consolidation Feasibility: Evaluate implementability of onsite waste management for landfill consolidation (FES Alternative 5) based on waste volumes and footprint.	Landfill wastes may be removed from below the water table and the landfill reconstructed and lined to eliminate leaching to groundwater. This FES alternative assumes that wastes would be relocated within the existing landfill footprint.	None at this time.	Map current waste extent based on photos, maps, and boring logs. Complete a conceptual design for the reconstructed landfill, including construction and waste management methods, sufficient for estimating costs to -30/+50% accuracy.
<b>From Modified Workplan (MNA/SS Evaluation)</b>			
<b>2.3 North Plume Monitored Natural Attenuation (MNA) for the Impacted Area.</b>  Once capture is demonstrated, establish that monitored natural attenuation will be effective at remediating the north plume (i.e., the Impacted Area) within a timeframe that is reasonable given the circumstances of the site.	MNA in the Impacted Area will be effective based on immobilization of dissolved arsenic. Effectiveness depends on: (1) demonstration of a static or shrinking plume (see objective #1); (2) determining rates and mechanisms of attenuation; (3) determining stability of immobilized arsenic; and (4) establishing a monitoring plan and contingency plans (USEPA 2007).	<p>The time to achieve MCLs or an achievable background level by aquifer flushing with upgradient groundwater, for both for MNA and more aggressive alternative scenarios (FES3B)</p> <p>The time required to deplete the landfill's ability to maintain reducing conditions resulting in trace element mobilization, and time required to meet background conditions or pre-landfill conditions</p>	<p>Based on data collected to date and Tier 1 through Tier 4 elements needed to assess important MNA components, additional site data is required for:</p> <ul style="list-style-type: none"> <li>• Plume Stability;</li> <li>• Plume Extent and Redox Front</li> <li>• Impact of Current Remediation;</li> <li>• Fate and Transport;</li> </ul> <p>To address these criterion the following is proposed:</p> <p><b>Task 2.3 Evaluation of MNA</b></p> <p><b>Task 2.3.1 Plume Stability</b> Additional data for plume stability will be collected under Task 2.3.2</p> <p><b>Task 2.3.2 Redox Boundary</b> Analyze existing data Advance DPT, well points in this area as deemed necessary to supplement existing delineation work being performed Identify changes in DO, Eh (or ORP)</p> <p>Identify changes in total and dissolved iron and total and dissolved arsenic, TSS and DOC</p> <p>Evaluate redox front between plume and Brook</p> <p><b>Task 2.3.3 Impact of Current Remediation</b> Additional data for effect of remediation collected under Task 1.4 and Task 1.2</p> <p><b>Task 2.3.4 Fate and Transport Data Analysis</b> Analyze data from the plume delineation work, the geophysical survey and the transect wells to determine redox boundary and arsenic geochemistry</p> <p>Determine arsenic fate in plume using transect well data and geochemical modeling</p>



Objective	Hypothesis	Data Gaps	Technical Approach
<p><b>2.3 North Plume Monitored Natural Attenuation (MNA) for the Impacted Area - Continued</b></p>			<p>Monitor for changes in redox, arsenic, iron, DOC, TSS and changes in water composition such as increase in sulfate or alkalinity.</p> <p>Conduct column studies for flushing time to background and determination of aquifer capacity for adsorbing arsenic.</p> <p>Conduct flushing timeframe study similar to USGS Saco Landfill study.</p> <p>Test cores of aquifer material from the Impacted Area and Use reaction model to simulate immobilization.</p> <p><b>Groundwater sampling</b> Collection of groundwater from monitoring wells planned for the transect study</p> <p><b>Task 2.3.5 Data Analysis</b> Analyze data, estimate arsenic uptake and based on results, redefine scope or sampling</p> <p>Conduct geochemical speciation calculations, modeling and statistical analysis</p>
<p><b>2.6 SourceStrength/Landfill Reducing Environment Evaluation</b></p> <p>Estimate the duration of the landfill's ability to maintain reducing /methanogenic conditions.</p>	<p>Arsenic, iron and other constituents are dissolved from the source materials by landfill-induced reducing conditions in groundwater. A portion of the landfill overlies a swamp where naturally-occurring reducing conditions may also have existed.</p> <p>While potential sources of arsenic in groundwater include bedrock, bedrock-derived soils, and possibly landfill wastes, the ultimate control is the ability of the landfill to maintain reducing conditions.</p> <p>Arsenic and other redox sensitive species will continue to mobilize as long as reducing conditions prevail. What time frame for achieving this is reasonable?</p>	<p>The time required to deplete the landfill's ability to maintain reducing conditions resulting in trace element mobilization, and time required to meet background conditions or pre-landfill conditions</p>	<p><b>Task 2.6 Examination of Source Strength</b> Determine impact of landfill as a carbon source</p> <p><b>Task 2.6.1 Vertical profiling of the landfill</b> Five (5) test locations in landfill to bedrock. Co-located depth sampling of water</p> <p><b>Waste and Aquifer Solids Sampling:</b> The focus of the sampling will be on profiling TOC, DOC, DIC in the landfill. As long as strongly reducing conditions exist, arsenic will continue to enter groundwater:</p> <p>Collection of discrete samples from the waste and aquifer Collection of sands overlying bedrock</p> <p>Collection of the upper 5 ft of bedrock and weathered bedrock</p> <p><b>Sample analysis</b> Water samples will be collected from the proposed borings. Testing will include typical field parameters (Eh, DO, Turbidity, Conductivity) Total and dissolved TAL metals, TOC, DOC, DIC, and TSS</p> <p>Waste samples and underlying sands and bedrock will be analyzed for Total metal(loid)s (TAL), TOC, X-ray Diffraction (XRD) for common mineralogy, Sequential Extraction, Thin-section/XRD/scanning electron microscopy for identification of arsenic and metal bearing phases.</p>

Objective	Hypothesis	Data Gaps	Technical Approach
2.6 SourceStrength/Landfill Reducing Environment Evaluation - Continued			<p><b>Task 2.6.2 Conduct Bench Testing</b> Test cores of source material and groundwater to simulate mobilization degradation of carbon and effect on trace elements, especially arsenic.</p> <p><b>Task 2.6.3 Data Analysis and Reporting</b> Estimation of time to depletion via carbon content (TOC, DOC, &amp; DIC)</p> <p>Vertical profiling of solids and water co-collected to determine relative sources of analytes to the plume</p> <p>Estimation of degradation rate and time to "completion"</p> <p><b>Speciation calculations and reactive transport modeling</b></p>



**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Arsenic			Calcium		Iron		Magnesium		Manganese	
					Total (ug/L)	Dissolved (ug/L)	Field Kit (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
GP-10-01	GP-10-01-009	5/27/2010	10:00	9	0.48 J	0.3 J	<5	NA	10,400	NA	827	NA	1,380	NA	21.6
	GP-10-01-019	5/27/2010	10:35	19	4.61	0.32 J	<5	NA	12,400	NA	548	NA	1,430	NA	49.7
	GDUP-052710	5/27/2010	10:35	19	NA	0.27 J	NA	NA	12,700	NA	525	NA	1,440	NA	45.5
	GP-10-01-029	5/27/2010	11:20	29	11.4	0.31 J	5	NA	10,600	NA	549	NA	1,170	NA	196
	GP-10-01-039	5/27/2010	11:45	39	9.39	< 1.13	5	NA	49,000	NA	1,860	NA	4,670	NA	14,000
	GP-10-01-049	5/27/2010	12:30	49	7.39	< 1.13	5	NA	15,300	NA	863	NA	1,480	NA	6,450
	GP-10-01-059	5/27/2010	13:11	59	18.9	< 1.13	5	NA	34,600	NA	2,150	NA	3,040	NA	12,100
	GP-10-01-069	5/27/2010	15:20	69	11.3	0.97 J	5	NA	39,900	NA	4,600	NA	4,300	NA	3,570
	GP-10-01-075	5/27/2010	16:30	75	2.35	0.89 J	5	NA	26,400	NA	6,380	NA	3,870	NA	3,310
GP-10-02	GP-10-02-024	6/7/2010	9:30	24	0.41 J	0.37 J	<5	NA	90,800	NA	1,130	NA	13,100	NA	560
	GP-10-02-034	6/7/2010	10:42	34	0.67	0.33 J	<5	NA	103,000	NA	1,560	NA	15,500	NA	1,440
	GDUP-060710	6/7/2010	10:42	34	NA	< 0.226	NA	NA	102,000	NA	1,520	NA	14,800	NA	1,380
	GP-10-02-044	6/7/2010	11:35	44	1.64	0.74 J	<5	NA	113,000	NA	2,140	NA	15,900	NA	2,060
	GP-10-02-054	6/7/2010	12:27	54	2.43	0.41 J	<5	NA	107,000	NA	2,150	NA	14,800	NA	2,200
	GP-10-02-064	6/7/2010	13:08	64	5.87	0.41 J	<5	NA	110,000	NA	3,500	NA	15,000	NA	1,990
	GP-10-02-074	6/7/2010	15:05	74	36.9	0.87 J	<5	NA	252,000	NA	4,010	NA	34,300	NA	2,910
	GP-10-02-084	6/7/2010	18:12	84	24.8	4.64	<5	NA	288,000	NA	19,600	NA	38,700	NA	2,680
GP-10-03	GP-10-03-029	6/10/2010	08:25	29	0.89	0.5	<5	NA	27400 J	NA	582	NA	3,580	NA	71
	GP-10-03-039	6/10/2010	9:20	39	6.79	0.61 J	<5	NA	76,800	NA	704	NA	9,840	NA	59.8
	GDUP-061010	6/10/2010	9:20	39	NA	< 0.452	NA	NA	83,800	NA	790	NA	10,900	NA	68.4
	GP-10-03-049	6/10/2010	10:00	49	14.6	< 0.565	<5	NA	110,000	NA	1,580	NA	12,900	NA	62.9
	GP-10-03-059	6/10/2010	10:40	59	42.1	0.92 J	<5	NA	103,000	NA	5,210	NA	11,400	NA	254
	GP-10-03-069	6/10/2010	11:20	69	8.74	3.17	5	NA	224,000	NA	7,530	NA	29,500	NA	1,735
	GDUP2-061010	6/10/2010	11:20	69	NA	3.85	NA	NA	252,000	NA	8,210	NA	32,700	NA	710
GP-10-04	GP-10-04-014	6/8/2010	12:40	14	2.26	0.18 J	<5	NA	2,200	NA	1170	NA	315	NA	210
	GP-10-04-024	6/8/2010	14:00	24	2.19	0.18 J	<5	NA	2,100	NA	256	NA	218	NA	58.1
	GDUP-060810	6/8/2010	14:00	24	NA	0.16 J	NA	NA	2,240	NA	199	NA	218	NA	63
	GP-10-04-034	6/8/2010	14:50	34	1.22	0.18 J	<5	NA	3,670	NA	438	NA	533	NA	84.4
	GP-10-04-044	6/8/2010	15:10	44	3.37	0.15 J	<5	NA	19,000	NA	629	NA	2,020	NA	86.6
	GP-10-04-054	6/8/2010	15:50	54	13.7	0.26 J	<5	NA	57,400	NA	3,040	NA	14,500	NA	811
	GP-10-04-064	6/8/2010	15:25	64	8.02	0.33 J	<5	NA	75,300	NA	1,200	NA	12,600	NA	510
	GP-10-04-074	6/8/2010	17:15	74	24.3	0.33 J	<5	NA	19,400	NA	3,000	NA	2,470	NA	433
GP-10-05	GP-10-04-084	6/8/2010	17:50	84	26.7	1.27	<5	NA	5,640	NA	896	NA	743	NA	91.4
	GP-10-04-094	6/8/2010	18:30	94	214	15.1	10-20	NA	154,000	NA	3,630	NA	20,300	NA	3,170
	GP-10-05-015	6/9/2010	9:50	15	2.08	0.31 J	<5	NA	7540 J	NA	262	NA	1,090	NA	483
	GP-10-05-025	6/9/2010	10:25	25	1.02 J	0.58 J	<5	NA	17,000	NA	1150	NA	2,590	NA	11,200
	GDUP-060910	6/9/2010	10:25	25	NA	< 0.565	NA	NA	16,800	NA	572	NA	2,600	NA	11,200
GP-10-05A	GP-10-05-035	6/9/2010	10:53	35	130	112	150	NA	12,400	NA	12,600	NA	2,260	NA	4,610
	GP-10-05-045	6/9/2010	11:24	45	86.4	84.7	80-100	NA	18,800	NA	11,200	NA	2,550	NA	2,320
	GP-10-05A-029	6/9/2010	13:20	29	0.93	0.62 J	<5	NA	8,140	NA	604	NA	878	NA	63.8
	GP-10-05A-039	6/9/2010	14:05	39	13	0.35 J	<5	NA	13,600	NA	2,310	NA	2,810	NA	221
	GDUP2-060910	6/9/2010	14:05	39	NA	0.33 J	NA	NA	13,900	NA	2,510	NA	2,850	NA	237
	GP-10-05A-049	6/9/2010	14:55	49	4.86	1.12	<5	NA	16,400	NA	3,360	NA	1,990	NA	203
	GP-10-05A-059	6/9/2010	15:57	59	3.48	0.39 J	<5	NA	17,700	NA	1,840	NA	2,050	NA	214
	GP-10-05A-069	6/9/2010	17:15	69	29.8	0.59	<5	NA	19,400	NA	797	NA	2,340	NA	466
	GP-10-05A-079	6/9/2010	18:45	79	65	2.18	<5	NA	16,500	NA	57.9	NA	1,940	NA	114
	GP-10-05A-089	6/9/2010	19:20	89	24.5	5.09	<5	NA	20,000	NA	467	NA	1,990	NA	70.3
	GP-10-05A-099	6/9/2010	19:40	99	364	4.16	<5	NA	65,800	NA	558	NA	5,740	NA	294
	GP-10-05A-109	6/9/2010	20:10	109	911	1.92	<5	NA	111,000	NA	3,730	NA	13,500	NA	1,320



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Boring Location	Sample ID	Date	Time (Military Format)	Depth	Arsenic			Calcium		Iron		Magnesium		Manganese	
					Total (ug/L)	Dissolved (ug/L)	Field Kit (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
GP-10-06	GP-10-06-024	5/24/2010	11:50	24	17.2	10	10	NA	3,100	NA	641	NA	274	NA	112
	GP-10-06-034	5/24/2010	12:40	34	120	121	150-200	NA	14,900	NA	14400 J	NA	1,480	NA	763
	GP-10-06-044	5/24/2010	13:35	44	155	129	100	NA	18,300	NA	34,400	NA	1,480	NA	982
	GP-10-06-054	5/26/2010	8:50	54	67.5	42.9	5	NA	80,700	NA	75,400	NA	10,800	NA	3,000
	GDUP-052610	5/26/2010	8:50	54	NA	49.1	NA	NA	87,800	NA	82,000	NA	11,400	NA	3,250
	GP-10-06-064	5/26/2010	9:45	64	683	750	150	NA	65,700	NA	122,000	NA	9,540	NA	2,840
	GP-10-06-074	5/26/2010	11:15	74	2,390	2070	>500	NA	53,400	NA	107,000	NA	10,100	NA	2,470
	GP-10-06-079	5/26/2010	12:00	79	2,660	2540	>500	NA	56,600	NA	72,200	NA	10,700	NA	3,490
GP-10-06A	GP-10-06A-034	5/24/2010	15:15	34	0.59	0.37 J	0	NA	2,830	NA	66.4	NA	398	NA	43.2
	GP-10-06A-044	5/24/2010	16:00	44	595	55.1	40	NA	9,030	NA	9,710	NA	737 J	NA	2,370
	GP-10-06A-054	5/24/2010	17:40	54	1090	18	10	NA	26,300	NA	6,550	NA	1,930	NA	6,920
	GP-10-06A-064	5/25/2010	9:50	64	170	36.7	20	NA	18,400	NA	28,900	NA	2,380	NA	2,780
	GDUP-052510	5/25/2010	9:50	64	NA	31.4	NA	NA	18,000	NA	28,900	NA	2,360	NA	2,830
	GP-10-06A-074	5/25/2010	11:10	74	134	58.6	30-40	NA	26,500	NA	42,200	NA	2,990	NA	2,460
	GP-10-06A-084	5/25/2010	13:00	84	186	106	60	NA	27,500	NA	42,200	NA	4,080	NA	3,050
	GP-10-06A-094	5/25/2010	14:40	94	382	< 1.13	5	NA	73,700	NA	13,300	NA	10,200	NA	17,900
	GP-10-06A-104	5/25/2010	16:30	104	405	< 1.13	0	NA	97,900	NA	5,950	NA	12,800	NA	6,530
	GP-10-06A-110	5/25/2010	17:35	110	333	1.17 J	20	NA	96,800	NA	8,640	NA	13,200	NA	6,670
GP-10-07	GP-10-07-039	5/19/2010	14:00	39	1,240	1350	>500	57,400	62,800	96,400	105,000	8,250	9,080	2,430	2,660
	GP-10-07-049	5/20/2010	13:45	49	283	58	5-10	135,000	65100 J	251000	27800 J	99900 J	11,000	9140 J	5330 J
	GDUP-052010	5/20/2010	13:45	49	304	58.2	5-10	129,000	64,600	276000	26,800	114000	10,900	9200	5,250
GP-10-08	GP-10-08-011	6/3/2010	12:10	11	2.08	0.64	<5	NA	24,600	NA	581	NA	3,440	NA	70.7
	GDUP-060310	6/3/2010	12:10	11	NA	0.67	NA	NA	23,500	NA	565	NA	3,310	NA	69.7
	GP-10-08-021	6/3/2010	13:20	21	3.19	0.76	<5	NA	44,200	NA	679	NA	6,040	NA	199
	GP-10-08-031	6/3/2010	14:30	31	3.6	0.31 J	<5	NA	109,000	NA	2,040	NA	13,200	NA	2,340
	GP-10-08-041	6/3/2010	15:00	41	3.77	0.85 J	<5	NA	131,000	NA	2,090	NA	15,000	NA	949
	GP-10-08-051	6/3/2010	17:20	51	19.8	1.06	<5	NA	172,000	NA	3,300	NA	23,000	NA	777
	GDUP-060310	6/3/2010	17:20	51	NA	0.92 J	NA	NA	172,000	NA	3,180	NA	23,300	NA	769
	GP-10-08-061	6/3/2010	18:05	61	2.07	0.73 J	<5	NA	142,000	NA	4,710	NA	18,500	NA	1,060
GP-10-09	GP-10-09-021	5/28/2010	9:15	21	0.45 J	0.27 J	<5	NA	4,780	NA	88.3	NA	400	NA	34.6
	GP-10-09-031	5/28/2010	10:00	31	183	0.15 J	<5	NA	10,100	NA	685	NA	895	NA	82.2
	GDUP-052810	5/28/2010	10:00	31	NA	0.17 J	NA	NA	10,700	NA	778	NA	944	NA	102
	GP-10-09-041	6/1/2010	11:30	41	12.6	0.25 J	<5	NA	17,700	NA	853	NA	1,860	NA	66
	GP-10-09-051	6/1/2010	13:00	51	13	0.27 J	<5	NA	23,500	NA	1,760	NA	2,390	NA	138
	GDUP-060110	6/1/2010	13:00	51	NA	0.23 J	NA	NA	22,300	NA	1,580	NA	2,280	NA	136
	GP-10-09-061	6/1/2010	14:20	61	6.8	0.940	<5	NA	43,800	NA	2,200	NA	5,370	NA	362
	GP-10-09-071	6/1/2010	16:45	71	23.3	0.680	<5	NA	47,200	NA	2,070	NA	5,680	NA	349
	GP-10-09-081	6/1/2010	17:50	81	15.5	0.850	<5	NA	44,000	NA	3,430	NA	5,300	NA	382
GP-10-10	GP-10-10-011	6/2/2010	14:45	11	0.34 J	0.27 J	<5	NA	8360 J	NA	332	NA	1,210	NA	34.5
	GP-10-10-021	6/2/2010	16:00	21	1.59	0.27 J	<5	NA	16,200	NA	728	NA	1,780	NA	56.5
	GDUP-060210	6/2/2010	16:00	21	NA	0.22 J	NA	NA	16,400	NA	732	NA	1,770	NA	58.2
	GP-10-10-031	6/2/2010	16:30	31	1.29 J	<0.565	<5	NA	19,300	NA	818	NA	2,260	NA	4,370
	GP-10-10-041	6/2/2010	17:15	41	1.86 J	1.13 J	<5	NA	33,600	NA	2,720	NA	4,950	NA	10,800
	GP-10-10-051	6/2/2010	18:00	51	4.4 J	2.47 J	<5	NA	72,900	NA	3,690	NA	10,800	NA	14,300
	GP-10-10-061	6/2/2010	19:00	61	11.1	< 2.82	<5	NA	113,000	NA	5,230	NA	14,600	NA	30,700
	GP-10-10-071	6/3/2010	10:00	71	13.7	< 1.13	<5	NA	105000 J	NA	4,880	NA	14,900	NA	15,500

Notes  
NA - Not Applicable  
ug/L is micrograms per liter  
mg/l - miligrams per liter  
J means estimated results  
B indicates that analyte was detected in the associated method blank



**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Potassium		Sodium		Turbidity NTU	DO mg/L	pH	Temp Celsius	Spec Cond uS/cm	ORP mV	Color
					Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)							
GP-10-01	GP-10-01-009	5/27/2010	10:00	9	NA	2,310	NA	35,500	10	5.34	6.35	10.08	365	107	Clear
	GP-10-01-019	5/27/2010	10:35	19	NA	2,740	NA	60,100	90	2.61	5.99	11.36	401	84.3	Clear
	GDUP-052710	5/27/2010	10:35	19	NA	2,770	NA	59,800							
	GP-10-01-029	5/27/2010	11:20	29	NA	2,730	NA	64,500	230	4.49	6.08	11.07	385	83.2	Cloudy
	GP-10-01-039	5/27/2010	11:45	39	NA	4,610	NA	53,800	80	0.37	6	11.81	671	62.7	Clear
	GP-10-01-049	5/27/2010	12:30	49	NA	2,420	NA	19,600	65	0.43	6.38	12.46	218	36.1	Clear
	GP-10-01-059	5/27/2010	13:11	59	NA	2,490	NA	11,200	170	0.23	6.25	11.68	307	15.5	Clear
	GP-10-01-069	5/27/2010	15:20	69	NA	3,240	NA	20,000	200	0.35	6.39	12.36	195	-40.6	Cloudy
	GP-10-01-075	5/27/2010	16:30	75	NA	3,750	NA	48,100	33	1.9	6.54	14.4	469	63.8	Clear
GP-10-02	GP-10-02-024	6/7/2010	9:50	24	NA	3,760	NA	45,400	2.8	0.41	6.29	11.08	776	24.3	Clear
	GP-10-02-034	6/7/2010	10:42	34	NA	4,320	NA	48,800	13.4	0.29	6.39	11.48	818	14.6	
	GDUP-060710	6/7/2010	10:42	34	NA	4,060	NA	46,300							
	GP-10-02-044	6/7/2010	11:35	44	NA	4,640	NA	58,700	41.1	0.28	6.46	11.27	777	11.3	
	GP-10-02-054	6/7/2010	12:27	54	NA	4,170	NA	52,900	85.7	0.29	6.5	12.09	757	2.6	
	GP-10-02-064	6/7/2010	13:08	64	NA	4,580	NA	83,500	454	0.71	6.55	12.01	965	-14.7	
	GP-10-02-074	6/7/2010	15:05	74	NA	7,680	NA	196,000	Max	0.32	6.41	12.07	2550	-5.5	
	GP-10-02-084	6/7/2010	18:12	84	NA	10,500	NA	236,000	Max	0.31	6.57	12.39	2863	-60.8	
	GP-10-02-094	6/8/2010	9:25	94	NA	8,450	NA	302,000	Max	1.15	570	12.54	2831	-97.9	
	GP-10-02-102	6/8/2010	10:10	102	NA	11,100	NA	155,000	Max	0.42	6.26	14.33	2345	-169.9	
GP-10-03	GP-10-03-029	6/10/2010	08:25	29	NA	2,900	NA	126,000	3.2	7.03	607	10.01	799	79.5	
	GP-10-03-039	6/10/2010	9:20	39	NA	4,660	NA	312,000	58	2.63	6.3	10.27	1916	29.8	
	GDUP-061010	6/10/2010	9:20	39	NA	5,010	NA	345,000							
	GP-10-03-049	6/10/2010	10:00	49	NA	6,040	NA	471,000	404	2	6.85	10.36	2563	14.5	
	GP-10-03-059	6/10/2010	10:40	59	NA	7,040	NA	598,000	Max	0.86	6.53	10.68	3212	-40.4	
	GP-10-03-069	6/10/2010	11:20	69	NA	9,330	NA	156,000	68.9	0.52	6.72	10.79	3470	5.8	
	GDUP2-061010	6/10/2010	11:20	69	NA	10,500	NA	502,000							
GP-10-04	GP-10-04-014	6/8/2010	12:40	14	NA	422	NA	3,460	18.7	8.32	6.17	13.34	26	50.1	
	GP-10-04-024	6/8/2010	14:00	24	NA	716	NA	3,080	4.65	6.22	6.07	12.88	34	73.1	
	GDUP-060810	6/8/2010	14:00	24	NA	619	NA	2,920							
	GP-10-04-034	6/8/2010	14:50	34	NA	859	NA	4,090	42.1	3.47	5.73	11.22	44	58.5	
	GP-10-04-044	6/8/2010	15:10	44	NA	1,280	NA	15,800	29.3	1.52	5.13	11.57	224	114.4	
	GP-10-04-054	6/8/2010	15:50	54	NA	3,360	NA	36,700	784	0.42	5.4	11.29	644	21.9	
	GP-10-04-064	6/8/2010	15:25	64	NA	3,020	NA	73,900	245	0.57	5.4	11.58	856	30.8	
	GP-10-04-074	6/8/2010	17:15	74	NA	3,260	NA	207,000	Max	0.38	6.28	11.17	935	-91.6	
	GP-10-04-084	6/8/2010	17:50	84	NA	2,000	NA	181,000	Max	0.32	6.01	11.53	79.8	-40.7	
	GP-10-04-094	6/8/2010	18:30	94	NA	12,300	NA	325,000	Max	0.29	6.33	12.05	244.5	-1,509	
GP-10-05	GP-10-05-015	6/9/2010	9:50	15	NA	1,280	NA	11,200	1.08	0.74	6.32	12.82	109	102.9	Clear
	GP-10-05-025	6/9/2010	10:25	25	NA	1,700	NA	23,800	3.54	1.77	5.85	12.55	242	73	Clear
	GDUP-060910	6/9/2010	10:25	25	NA	1,580	NA	23,900							
	GP-10-05-035	6/9/2010	10:53	35	NA	1,160	NA	19,100	17.8	1.45	6.21	13.25	214	-56	Clear
	GP-10-05-045	6/9/2010	11:24	45	NA	1,710	NA	28,700	36.9	2.24	6.17	2.76	255	-68	Clear
GP-10-05A	GP-10-05A-029	6/9/2010	13:20	29	NA	3,200	NA	272,000	1.52	992	6	16.24	1194	63.2	Clear
	GP-10-05A-039	6/9/2010	14:05	39	NA	1,420	NA	27,400	57.7	2.79	5.22	14.72	209	110	Clear
	GDUP2-060910	6/9/2010	14:05	39	NA	1,490	NA	30,400							
	GP-10-05A-049	6/9/2010	14:55	49	NA	1,500	NA	18,600	39	4.87	5.81	14.29	172	76	
	GP-10-05A-059	6/9/2010	15:57	59	NA	1,980	NA	24,200	32.9	1.73	6.18	13.89	208	39	Tan/Clear
	GP-10-05A-069	6/9/2010	17:15	69	NA	1,880	NA	22,200	Hand Pumped						
	GP-10-05A-079	6/9/2010	18:45	79	NA	1,550	NA	17,700	No Readings, Silted up and Clogged Screen						
	GP-10-05A-089	6/9/2010	19:20	89	NA	1,940	NA	17,800	No Readings, Silted up and Clogged Screen						
	GP-10-05A-099	6/9/2010	19:40	99	NA	4,190	NA	30,800	No Readings, Silted up and Clogged Screen						
	GP-10-05A-109	6/9/2010	20:10	109	NA	6,990	NA	104,000	No Readings, Silted up and Clogged Screen						

**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Potassium		Sodium		Turbidity NTU	DO mg/L	pH	Temp Celsius	Spec Cond uS/cm	ORP mV	Color
					Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)							
GP-10-06	GP-10-06-024	5/24/2010	11:50	24	NA	817	NA	639	50	0.19	5.57	9.16	26	127.5	Clear
	GP-10-06-034	5/24/2010	12:40	34	NA	2,700	NA	2,120	31	0.39	2.99	12.66	103	-12.3	Clear
	GP-10-06-044	5/24/2010	13:35	44	NA	3,440	NA	3,730	800	0.19	5.65	15.69	194	4.9	Cloudy
	GP-10-06-054	5/26/2010	8:50	54	NA	13,900	NA	35,400	Max	0.19	6.04	12.89	880	-119.6	Cloudy
	GDUP-052610	5/26/2010	8:50	54	NA	15,300	NA	38,000							
	GP-10-06-064	5/26/2010	9:45	64	NA	18,200	NA	30,800	Max	0.14	6	11.63	827	-120	Cloudy
	GP-10-06-074	5/26/2010	11:15	74	NA	10,700	NA	19,100	Max	0.14	4.08	14.16	725	-124	Cloudy
	GP-10-06-079	5/26/2010	12:00	79	NA	12,500	NA	24,700	Max	0.19	4.34	14.89	669	-109	Cloudy
GP-10-06A	GP-10-06A-034	5/24/2010	15:15	34	NA	526	NA	2,600	2.3	10.04	5.66	16.58	24	194.9	Clear
	GP-10-06A-044	5/24/2010	16:00	44	NA	2,560	NA	1,910	140	1.54	5.79	14.66	76	27	Cloudy
	GP-10-06A-054	5/24/2010	17:40	54	NA	2,320	NA	2,800	900	1.47	5.8	14.1	166	8.1	Cloudy
	GP-10-06A-064	5/25/2010	9:50	64	NA	5,090	NA	5,810	Max	0.1	6.55	15.54	67	-134	Cloudy
	GDUP-052510	5/25/2010	9:50	64	NA	5,280	NA	6,330							
	GP-10-06A-074	5/25/2010	11:10	74	NA	7,100	NA	12,200	Max	0.14	6.37	14.54	292	-115	Cloudy
	GP-10-06A-084	5/25/2010	13:00	84	NA	8,480	NA	14,600	Max	0.17	6.34	14.83	316	-115	Cloudy
	GP-10-06A-094	5/25/2010	14:40	94	NA	10,700	NA	39,700	Max	0.21	5.81	16.77	508	-119	Cloudy
GP-10-07	GP-10-07-039	5/19/2010	14:00	39	13,700	14,500	24,800	26,300							
	GP-10-07-049	5/20/2010	13:45	49	70800	23400 J	30200	27,800							
	GDUP-052010	5/20/2010	13:45	49	75200	23,300	28700	27,500							
GP-10-08	GP-10-08-011	6/3/2010	12:10	11	NA	1,560	NA	12,000							
	GDUP-060310	6/3/2010	12:10	11	NA	1,490	NA	11,700	12.7	6.97	6.78	11.73	189	20.1	Clear
	GP-10-08-021	6/3/2010	13:20	21	NA	2,220	NA	20,400	17.5	4.68	6.5	10.46	337	31.4	Clear
	GP-10-08-031	6/3/2010	14:30	31	NA	3,240	NA	38,500	44.4	0.51	6.43	13.57	660	-3.9	Tan / clear
	GP-10-08-041	6/3/2010	15:00	41	NA	3,550	NA	39,200	64.9	0.26	6.44	12.02	764	-8.6	Clear
	GP-10-08-051	6/3/2010	17:20	51	NA	5,200	NA	48,900	321	0.24	6.56	11.6	9.64	-42	Tan / Clear
	GDUP2-060310	6/3/2010	17:20	51	NA	5,190	NA	48,000							
	GP-10-08-061	6/3/2010	18:05	61	NA	4,390	NA	40,800	37.4	0.9	6.54	15	244	-4.3	Clear
GP-10-09	GP-10-09-021	5/28/2010	9:15	21	NA	1,030	NA	4,760	1.13	10.34	6.82	11.93	62	97.1	Clear
	GP-10-09-031	5/28/2010	10:00	31	NA	2,220	NA	33,600	596	6.35	6.11	12.82	223	71.6	Cloudy
	GDUP-052810	5/28/2010	10:00	31	NA	2,350	NA	33,200							
	GP-10-09-041	6/1/2010	11:30	41	NA	3,220	NA	134000 J	178	4.97	6.05	13.05	706	50.4	Cloudy
	GP-10-09-051	6/1/2010	13:00	51	NA	2,690	NA	134,000	333	2.15	6.24	12.56	714	161	Cloudy
	GDUP-060110	6/1/2010	13:00	51	NA	2,500	NA	132,000							
	GP-10-09-061	6/1/2010	14:20	61	NA	3,300	NA	30,500	87.1	1.04	6.62	13.19	401	-56.2	Clear
	GP-10-09-071	6/1/2010	16:45	71	NA	3,470	NA	45,300	82.2	1.19	6.66	12.92	486	-58.6	Cloudy
GP-10-10	GP-10-09-081	6/1/2010	17:50	81	NA	3,300	NA	36,500	93.2	1.18	6.66	13.3	428	-57.3	Clear
	GP-10-10-011	6/2/2010	14:45	11	NA	2,690	NA	12,500	2.5	10.93	6.73	10.89	130	56.2	Clear
	GP-10-10-021	6/2/2010	16:00	21	NA	2,490	NA	54,300	11.8	7.45	6.17	11.49	375	53.9	Clear
	GDUP-060210	6/2/2010	16:00	21	NA	2,560	NA	54,200							
	GP-10-10-031	6/2/2010	16:30	31	NA	5,480	NA	88,800	10.34	0.56	6.1	12.46	561	43.5	Clear
	GP-10-10-041	6/2/2010	17:15	41	NA	8,250	NA	43,300	26.3	0.29	6.19	13.26	509	-2.8	Clear
	GP-10-10-051	6/2/2010	18:00	51	NA	5,650	NA	32,400	26	0.26	6.32	12.59	594	-35.3	Clear
	GP-10-10-061	6/2/2010	19:00	61	NA	4,170	NA	39,600	90.6	0.32	6.34	12.02	87.6	-44.3	Clear
	GP-10-10-071	6/3/2010	10:00	71	NA	5,190	NA	44,500	121	0.36	6.41	12.72	737	-85	Tan

Notes NA - Not Applicable  
 ug/L is micrograms per liter  
 mg/l - milligrams per liter  
 J means estimated results  
 B indicates that analyte was detected in the associated method blank

DO - Dissolved Oxygen  
 ORP - Oxygen Reduction Potential



**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Alkalinity mg CaCO3/L	Ammonia mg/l	Nitrite mg/l	COD mg/l	Chloride mg/l	Nitrate mg/l	Sulfate mg/l	Notes
GP-10-01	GP-10-01-009	5/27/2010	10:00	9	23	0.214	< 0.002	< 7	42	3.6	18	
	GP-10-01-019	5/27/2010	10:35	19	30	0.0565 J	< 0.002	< 7	92	4.1	16	
	GDUP-052710	5/27/2010	10:35	19	31	0.241	< 0.002	< 7	90	3.7	16	
	GP-10-01-029	5/27/2010	11:20	29	31	0.0691 J	< 0.002	< 7	82	2.3	26	
	GP-10-01-039	5/27/2010	11:45	39	38	1.1	0.01 J	9.2 J	170	3.9	22	
	GP-10-01-049	5/27/2010	12:30	49	60	0.744	< 0.002	< 7	24	0.4	7.9	
	GP-10-01-059	5/27/2010	13:11	59	94	0.307	< 0.002	16 J	34	0.23	7.7	
	GP-10-01-069	5/27/2010	15:20	69	120	0.212	< 0.002	7	34	0.49	10	
	GP-10-01-075	5/27/2010	16:30	75	62	0.514	0.01 J	< 7	92	2.4	16	
GP-10-02	GP-10-02-024	6/7/2010	9:50	24	200	0.089	< 0.002	18 J	140	< 0.01	23	
	GP-10-02-034	6/7/2010	10:42	34	190	0.109	< 0.002	16 J	150	< 0.01	28	
	GDUP-060710	6/7/2010	10:42	34	190	0.092	< 0.002	27	150	< 0.01	29	
	GP-10-02-044	6/7/2010	11:35	44	200	0.293	< 0.002	13 J	130	< 0.01	18	
	GP-10-02-054	6/7/2010	12:27	54	230	0.268	< 0.002	16 J	110	< 0.01	16	
	GP-10-02-064	6/7/2010	13:08	64	270	0.196	< 0.002	20	160	< 0.01	23	
	GP-10-02-074	6/7/2010	15:05	74	140	0.178	< 0.002	29	780	0.026 J	31	
	GP-10-02-084	6/7/2010	18:12	84	170	0.08	< 0.002	31	880	< 0.01	32	
	GP-10-02-094	6/8/2010	9:25	94	150	0.081	< 0.002	38	840	< 0.01	34	
	GP-10-02-102	6/8/2010	10:10	102	210	0.077	< 0.002	40	640	< 0.01	30	
GP-10-03	GP-10-03-029	6/10/2010	08:25	29	46	0.0326 J	< 0.002	< 7	210	1.4	48	
	GP-10-03-039	6/10/2010	9:20	39	65	0.046 J	< 0.002	27	600	4.4	31	
	GDUP-061010	6/10/2010	9:20	39	65	< 0.025	< 0.002	22	620	4.3	33	
	GP-10-03-049	6/10/2010	10:00	49	53	0.0287 J	< 0.002	38	870	0.58	49	
	GP-10-03-059	6/10/2010	10:40	59	110	0.0264 J	< 0.002	47	1100	0.63	35	
	GP-10-03-069	6/10/2010	11:20	69	100	0.031 J	< 0.002	13	1200	0.02 J	38	
	GDUP2-061010	6/10/2010	11:20	69	100	< 0.025	< 0.002	47	1200	0.024 J	38	
GP-10-04	GP-10-04-014	6/8/2010	12:40	14	12	0.0296 J	< 0.002	< 7	5.7	0.028 J	0.74 J	
	GP-10-04-024	6/8/2010	14:00	24	11	0.0433 J	< 0.002	9 J	2	0.03 J	0.67 J	
	GDUP-060810	6/8/2010	14:00	24	11	0.0242 J	< 0.002	< 7	2.2	0.049 J	< 0.12	
	GP-10-04-034	6/8/2010	14:50	34	17	0.0205 J	< 0.002	< 7	2.1	0.1	< 0.12	
	GP-10-04-044	6/8/2010	15:10	44	22	0.024 J	< 0.002	< 7	23	3.6	< 0.12	
	GP-10-04-054	6/8/2010	15:50	54	100	2.67	0.01 J	11 J	67	5.8	87	
	GP-10-04-064	6/8/2010	15:25	64	120	0.103	0.01 J	20	120	3.8	97	
	GP-10-04-074	6/8/2010	17:15	74	100	0.0522 J	< 0.002	31	210	0.48	32	
	GP-10-04-084	6/8/2010	17:50	84	120	0.0319 J	< 0.002	16 J	150	0.12	34	
	GP-10-04-094	6/8/2010	18:30	94	140	0.0543 J	< 0.002	38	820	< 0.01	30	
GP-10-05	GP-10-05-015	6/9/2010	9:50	15	18	0.0356 J	< 0.002	25	19	0.64	9.9	
	GP-10-05-025	6/9/2010	10:25	25	55	0.152	< 0.002	29	48	0.012 J	6.3 B	
	GDUP-060910	6/9/2010	10:25	25	56	0.114	< 0.002	20	47	< 0.01	4.3 B	
	GP-10-05-035	6/9/2010	10:53	35	61	0.145	< 0.002	20	39	< 0.01	3.7 B	
	GP-10-05-045	6/9/2010	11:24	45	56	0.185	< 0.002	31	45	< 0.01	1.8 B	
GP-10-05A	GP-10-05A-029	6/9/2010	13:20	29	51	0.0425 J	< 0.002	56	380	1.9	16	
	GP-10-05A-039	6/9/2010	14:05	39	30	0.0324 J	< 0.002	16 J	34	2.1	25	
	GDUP2-060910	6/9/2010	14:05	39	32	0.0388 J	< 0.002	11 J	35	2.4	26	
	GP-10-05A-049	6/9/2010	14:55	49	44	0.0387 J	< 0.002	18 J	20	1.7	13	
	GP-10-05A-059	6/9/2010	15:57	59	44	0.092	< 0.002	< 7	43	0.72	13	
	GP-10-05A-069	6/9/2010	17:15	69	49	0.0442 J	< 0.002	< 7	30	1.2	14	
	GP-10-05A-079	6/9/2010	18:45	79	54	0.042 J	< 0.002	< 7	22	1	10	
	GP-10-05A-089	6/9/2010	19:20	89	55	0.0325 J	< 0.002	11 J	21	1	8.9	
	GP-10-05A-099	6/9/2010	19:40	99	170	0.082	< 0.002	< 7	56	0.26	24	
	GP-10-05A-109	6/9/2010	20:10	109	270	0.154	< 0.002	11 J	140	1	30	

TABLE 2  
Groundwater Profile Results  
Shepley's Hill Landfill, Devens, MA

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Alkalinity mg CaCO3/L	Ammonia mg/l	Nitrite mg/l	COD mg/l	Chloride mg/l	Nitrate mg/l	Sulfate mg/l	Notes
GP-10-06	GP-10-06-024	5/24/2010	11:50	24	12	0.0547 J	< 0.02	< 7	0.43 J	0.009 J	1.3	0.45u Filter
	GP-10-06-034	5/24/2010	12:40	34	59	2.28	< 0.02	< 7	1	0.37	3	
	GP-10-06-044	5/24/2010	13:35	44	80	1.21	0.025 J	< 7	0.95	0.12	17	may be closer to 150, 1100
	GP-10-06-054	5/26/2010	8:50	54	380	12.1	< 0.002	27	34	0.23	3.3	
	GDUP-052610	5/26/2010	8:50	54	380	12.2	< 0.002	18 J	30	0.36	2.4	
	GP-10-06-064	5/26/2010	9:45	64	330	9.04	< 0.002	32	20	0.3	0.85 J	
	GP-10-06-074	5/26/2010	11:15	74	290	2.8	< 0.002	170	14	0.024 J	1.2	Turned brown by time of test
	GP-10-06-079	5/26/2010	12:00	79	270	2.96	< 0.002	9.2 J	16	0.22	4.4	
GP-10-06A	GP-10-06A-034	5/24/2010	15:15	34	9	0.0232 J	< 0.02	< 7	1.4	0.023 J	5.6	
	GP-10-06A-044	5/24/2010	16:00	44	35	0.123	< 0.02	< 7	0.91	0.03 J	9.2	
	GP-10-06A-054	5/24/2010	17:40	54	81	1.05	< 0.02	< 7	1.5	0.05 J	16	
	GP-10-06A-064	5/25/2010	9:50	64	84	2.08	< 0.02	< 7	4.4	0.06	4.8	
	GDUP-052510	5/25/2010	9:50	64	84	2.22	< 0.02	< 7	4.8	0.08	5.6	
	GP-10-06A-074	5/25/2010	11:10	74	140	3.89	0.02 J	14 J	6.3	0.13	2.4	
	GP-10-06A-084	5/25/2010	13:00	84	140	4.92	< 0.02	11 J	5.4	0.12	3.3	
	GP-10-06A-094	5/25/2010	14:40	94	290	2.23	0.018 J	18 J	26	0.29	4.2	
	GP-10-06A-104	5/25/2010	16:30	104	360	0.947	< 0.002	18 J	28	0.32	3.6	
	GP-10-06A-110	5/25/2010	17:35	110	350	0.43	< 0.002	23	28	0.37	3.9	
GP-10-07	GP-10-07-039	5/19/2010	14:00	39	310	7.49	0.022 J	25	46	< 0.01	0.4 J	
	GP-10-07-049	5/20/2010	13:45	49	240	2.68	< 0.02	16 J	49	0.012 J	1.6	
	GDUP-052010	5/20/2010	13:45	49	250	2.68	0.022 J	16 J	49	0.011 J	1.6	
GP-10-08	GP-10-08-011	6/3/2010	12:10	11	67	0.02 J	< 0.002	< 7	21	0.01 J	8.1	
	GDUP-060310	6/3/2010	12:10	11	66	< 0.017	< 0.002	< 7	22	0.01 J	8.5	
	GP-10-08-021	6/3/2010	13:20	21	120	0.017	< 0.002	< 7	42	0.08	12	
	GP-10-08-031	6/3/2010	14:30	31	290	0.0719 J	< 0.002	< 7	71	< 0.01	14	
	GP-10-08-041	6/3/2010	15:00	41	320	0.0467 J	< 0.002	9 J	90	< 0.01	16	
	GP-10-08-051	6/3/2010	17:20	51	530	0.0358 J	< 0.002	13 J	67	< 0.01	10	
	GDUP2-060310	6/3/2010	17:20	51	530	0.017 J	< 0.002	< 7	66	< 0.01	10	
	GP-10-08-061	6/3/2010	18:05	61	410	0.0201 J	< 0.002	9 J	72	< 0.01	13	
GP-10-09	GP-10-09-021	5/28/2010	9:15	21	12	0.0491 J	< 0.002	< 7	2	0.78	8.6	
	GP-10-09-031	5/28/2010	10:00	31	18	0.0384 J	< 0.002	< 7	48	2.8	13	
	GDUP-052810	5/28/2010	10:00	31	18	0.017 J	< 0.002	9 J	45	2.9	13	
	GP-10-09-041	6/1/2010	11:30	41	32	0.0225 J	< 0.002	< 7	220	1.7	13	
	GP-10-09-051	6/1/2010	13:00	51	52	0.0364 J	< 0.002	9 J	200	2.3	16	
	GDUP-060110	6/1/2010	13:00	51	52	0.0166 J	< 0.002	< 7	200	2.2	16	
	GP-10-09-061	6/1/2010	14:20	61	120	0.0208 J	< 0.002	< 7	48	0.6	15	
	GP-10-09-071	6/1/2010	16:45	71	120	0.0326 J	< 0.002	< 7	85	0.67	14	
	GP-10-09-081	6/1/2010	17:50	81	110	0.0168 J	< 0.002	< 7	68	0.74	15	
GP-10-10	GP-10-10-011	6/2/2010	14:45	11	22	< 0.017	< 0.002	< 7	17	1.1	7.4	
	GP-10-10-021	6/2/2010	16:00	21	38	0.0274 J	< 0.002	< 7	82	2.2	12	
	GDUP-060210	6/2/2010	16:00	21	38	0.0224 J	< 0.002	11 J	83	2.4	11	
	GP-10-10-031	6/2/2010	16:30	31	80	2.21	< 0.002	< 7	120	0.26	16	
	GP-10-10-041	6/2/2010	17:15	41	130	5.01	< 0.002	9 J	76	0.028 J	6 B	
	GP-10-10-051	6/2/2010	18:00	51	300	0.54	< 0.002	18 J	25	0.047 J	0.98 JB	
	GP-10-10-061	6/2/2010	19:00	61	350	0.276	< 0.002	38	82	0.11	2.1 B	
	GP-10-10-071	6/3/2010	10:00	71	330	0.512	< 0.002	22	91	0.2	2.1 B	

Notes

NA - Not Applicable

ug/L is micrograms per liter

mg/l - milligrams per liter

J means estimated results

B indicates that analyte was detected in the associated method blank

COD - Chemical Oxygen Demand



**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Aluminum		Antimony		Arsenic			Barium		Beryllium		Cadmium		Calcium	
					Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Field Kit (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
GP-10-11	GP-10-11-039	8/3/2010	14:10	39	443	NA	NA	NA	263	264	80	NA	NA	NA	NA	NA	NA	19000	NA
	GP-10-11-049	8/3/2010	15:15	49	44400	NA	NA	NA	688	375	70	NA	NA	NA	NA	NA	NA	26500	NA
	DUP3-080310	8/3/2010	15:15	49	35200	NA	NA	NA	641	396	NA	NA	NA	NA	NA	NA	NA	26100	NA
	GP-10-11-059	8/3/2010	19:00	55	49400	< 7.64	NA	1.17 J	760	236	150	NA	27.3	NA	< 0.236	NA	< 0.236	61600	44000
	GP-10-11-064	8/4/2010	11:30	64	56600	44.1 J	NA	1.19	230	19.8	< 5	NA	26.5	NA	< 0.059	NA	< 0.059	285000	44400 J
GP-10-12	GP-10-12-044	8/5/2010	13:05	44	20200	< 19.1	NA	< 1.2	4320	3880	> 500	NA	36.1	NA	< 0.059	NA	< 0.590	33600	24500
	GP-10-12-054	8/5/2010	15:00	54	NA	19.1	NA	< 1.2	NA	2850	> 500	NA	29.9	NA	< 0.590	NA	< 0.590	NA	39500
	GP-10-12-065	8/9/2010	8:20	65	NA	14.1 J	NA	2.39	NA	38.9	30	NA	37.6	NA	< 0.236	NA	< 0.236	NA	55700
GP-10-13	GP-10-13-039	8/9/2010	14:45	39	32900	17	NA	0.22 J	176	124	30	NA	123	NA	< 0.059	NA	< 0.059	97100	81100
	GP-10-13-049	8/9/2010	17:00	49	NA	12.5 J	NA	0.81 J	NA	12.2	< 5	NA	98.6	NA	< 0.295	NA	< 0.295	NA	103000
	GP-10-13-059	8/10/2010	9:05	59	16000	8.44 J	NA	0.19 J	120	102	100	NA	244	NA	< 0.059	NA	< 0.059	80700	84000
	GP-10-13-069	8/10/2010	11:15	69	NA	< 19.1	NA	< 1.2	NA	1060	> 500	NA	68.3	NA	< 0.59	NA	< 0.59	NA	56700
	GP-10-13-079	8/10/2010	13:10	79	NA	5.88 J	NA	0.16 J	NA	123	20	NA	12.9	NA	< 0.059	NA	< 0.059	NA	32300
GP-10-14	GP-10-14-039	8/16/2010	09:50	39	1980	4.84 J	NA	0.14 JB	39.1	14.4	5	NA	49.8	NA	< 0.059	NA	< 0.059	63300	62700
	GP-10-14-049	8/16/2010	11:20	49	2400	35.8 J	NA	0.8 JB	774	772	250	NA	88	NA	< 0.236	NA	< 0.236	49100	50600
	DUP-081610	8/16/2010	11:20	49	6020	36.7 J	NA	< 0.48	792	762	NA	NA	85.4	NA	< 0.236	NA	< 0.236	49600	48500
	GP-10-14-059	8/16/2010	13:00	59	NA	< 19.1	NA	1.21 JB	NA	2400	> 500	NA	15.6	NA	< 0.59	NA	< 0.59	NA	52900
	GP-10-14-069	8/16/2010	14:35	69	NA	< 19.1	NA	< 1.20	5260	5110	> 500	NA	19.6	NA	< 0.590	NA	< 0.590	38500	36200
	GP-10-14-079	8/17/2010	07:45	79	8270	< 19.1	1.73 J	< 1.20	17300	15100	> 500	58.4	22.6	< 0.590	< 0.590	< 0.590	< 0.590	29900	30500
GP-10-15	GP-10-15-039	8/11/2010	9:30	39	NA	18.5 J	NA	< 0.480	NA	1740	> 500	NA	124	NA	< 0.236	NA	< 0.236	NA	45600
	GP-10-15-049	8/11/2010	11:25	49	2080	< 19.1	NA	< 1.20	17200	16600	70	NA	17.3	NA	< 0.590	NA	< 0.590	47700	49400
	GP-10-15-059	8/11/2010	14:45	59	NA	3.15	NA	0.19 J	NA	278	< 5	NA	7.5	NA	< 0.059	NA	< 0.059	NA	32100
GP-10-16	GP-10-16-024	8/17/2010	16:15	24	41800	7.68 JB	2.92	0.26 J	170	4.81	5	249	5.73	2.53	< 0.059	0.67 J	< 0.059	30600	14500
	DUP-081710	8/17/2010	16:15	24	44600	11.8 JB	2.88	0.2 J	164	3.87		255	5.99	2.55	< 0.059	0.66 J	< 0.059	30600	15900
	GP-10-16-034	8/18/2010	07:55	34	79600	42.3	3.2 J	0.51	333 J	1.97	5	558	8.23	6.35	< 0.059	1.36 J	< 0.059	57800	15000
	GP-10-16-054	8/18/2010	11:20	54	4030	16.9	2.82	0.8	19.9	1.89	< 5	25.9	8.15	0.34 J	< 0.059	0.19 J	< 0.059	35200	34700
	DUP-081810	8/18/2010	11:20	54	5710	18.9	3.6	0.64	26	2.05	NA	32.5	8.34	0.45 J	< 0.059	0.23 J	< 0.059	33600	35000
	GP-10-16-064	8/18/2010	13:40	64	NA	4.17 J	NA	0.28 J	NA	445	100	NA	39.2	NA	< 0.059	NA	< 0.059	NA	31300
	GP-10-16-074	8/19/2010	07:45	74	3540	7.02 J	1	0.42 J	248 J	216 J	100	59	36.3	0.17 J	< 0.059	< 0.059	< 0.059	52200	50900
	GP-10-16-084	8/19/2010	09:40	84	906	< 7.64	1.39 J	< 0.48	256	248	100	64.3	56.6	< 0.236	< 0.236	< 0.236	< 0.236	125000	122000
	DUP-081910	8/19/2010	09:40	84	1460	14.1 J	0.81 J	< 0.48	260	249	NA	67.4	59.4	< 0.236	< 0.236	< 0.236	< 0.236	128000	121000
	GP-10-16-094	8/19/2010	12:35	94	2880	5.34 J	1.01	0.23 J	19.3	3.44	< 5	35.8	10.1	0.3 J	< 0.059	0.07 J	< 0.059	39200	34700
GP-10-17	GP-10-17-009	8/2/2010	11:40	9	NA	NA	NA	NA	0.58	0.46 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-019	8/2/2010	12:20	19	NA	NA	NA	NA	0.78	0.39 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	DUP-080210	8/2/2010	12:20	19	NA	NA	NA	NA	0.66	0.49 J	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-029	8/2/2010	16:00	29	NA	NA	NA	NA	0.78	0.25 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-039	8/2/2010	16:45	39	NA	NA	NA	NA	1950	1860	500	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-049	8/2/2010	17:30	49	NA	NA	NA	NA	17.7	20.8	5	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-18	GP-10-18-007	8/2/2010	18:34	7	NA	NA	NA	NA	0.93	0.73	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-017	8/3/2010	8:25	17	NA	NA	NA	NA	1.87 J	1.26 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-027	8/3/2010	9:00	27	NA	NA	NA	NA	117	107	80	NA	NA	NA	NA	NA	NA	NA	NA
	DUP-080310	8/3/2010	9:00	27	NA	NA	NA	NA	118	107		NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-037	8/3/2010	11:00	37	NA	NA	NA	NA	274	262	60	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-047	8/3/2010	12:10	47	NA	NA	NA	NA	373	390	80	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-19	GP-10-19-009	8/3/2010	14:35	9	NA	NA	NA	NA	0.57	0.38 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	DUP2-080310	8/3/2010	14:35	9	NA	NA	NA	NA	0.53	0.35 J	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-019	8/3/2010	15:15	19	NA	NA	NA	NA	3.07	0.6	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-029	8/3/2010	16:05	29	NA	NA	NA	NA	886	810	100	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-039	8/3/2010	17:00	39	NA	NA	NA	NA	690	677	100	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-046	8/3/2010	18:15	46	NA	NA	NA	NA	23.3	3.92	5	NA	NA	NA	NA	NA	NA	NA	NA



TABLE 2  
Groundwater Profile Results  
Shepley's Hill Landfill, Devens, MA

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Aluminum		Antimony		Arsenic			Barium		Beryllium		Cadmium		Calcium	
					Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Field Kit (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
GP-10-20	GP-10-20-009	8/4/2010	9:30	9	NA	NA	NA	NA	1.6	0.4 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-20-019	8/4/2010	10:10	19	488	5.49 J	NA	NA	2.94	1.02	< 5	NA	NA	NA	NA	NA	NA	13100	12100
	DUP-080410	8/4/2010	10:10	19	573	5.81 J	NA	0.21 J	3.11	0.066	NA	NA	32.1	NA	< 0.500	NA	0.08 J	12500	12500
	GP-10-20-029	8/4/2010	11:00	29	NA	NA	NA	NA	220	235	40	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-20-039	8/4/2010	13:00	39	NA	NA	NA	NA	446	429	50	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-21	GP-10-21-011	8/4/2010	15:05	11	NA	NA	NA	NA	3.98	0.31 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-021	8/4/2010	15:45	21	446	6.21 J	NA	NA	1.71	0.62 J	< 5	NA	NA	NA	NA	NA	NA	22100	21600 J
	DUP2-080410	8/4/2010	15:45	21	344	8.05 J	NA	NA	1.48	0.63 J	NA	NA	NA	NA	NA	NA	NA	21600	22900
	GP-10-21-031	8/4/2010	16:30	31	NA	NA	NA	NA	5.05	3.64	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-041	8/4/2010	17:00	41	NA	NA	NA	NA	322	349	60	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-051	8/4/2010	18:05	51	NA	NA	NA	NA	18.7	12.3	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-060	8/4/2010	19:00	60	NA	NA	NA	NA	145	146	40	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-22	GP-10-22-011	8/10/2010	14:40	11	NA	NA	NA	NA	0.51	0.37 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-021	8/10/2010	15:00	21	NA	NA	NA	NA	1.71	0.51	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-031	8/10/2010	15:50	31	NA	NA	NA	NA	2.65	0.75 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-041	8/10/2010	16:30	41	NA	NA	NA	NA	15.8	14.5	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-051	8/10/2010	17:30	51	NA	NA	NA	NA	5.02	< 1.13	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-061	8/10/2010	18:30	61	NA	NA	NA	NA	6.56	3.53	< 5	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-23	GP-10-23-017	8/5/2010	11:00	17	59.8	6.6 J	NA	NA	0.52	0.38 J	< 5	NA	NA	NA	NA	NA	NA	9860	9680
	DUP-080510	8/5/2010	11:00	17	49.2	5.6 J	NA	0.15 J	1.45	1.4	NA	NA	13.5	NA	< 0.059	NA	< 0.059	10500	10300
	GP-10-23-027	8/5/2010	11:45	27	735	5.22 J	NA	NA	2.86	0.6 J	< 5	NA	NA	NA	NA	NA	NA	16200	16300
	GP-10-23-037	8/5/2010	12:25	37	NA	NA	NA	NA	5.38	0.28 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-23-047	8/5/2010	14:20	47	NA	NA	NA	NA	610	666	500	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-23-057	8/5/2010	16:05	57	2900	< 9.56	NA	NA	1060	1070	500	NA	NA	NA	NA	NA	NA	83200	85000
	DUP2-080510	8/5/2010	16:05	57	4180	< 9.56	NA	< 0.600	1160	1100	NA	NA	43.8	NA	< 0.295	NA	< 0.295	90800	86500
GP-10-24	GP-10-24-015	8/9/2010	15:44	15	138	8.52 J	NA	NA	2.06	0.94 J	< 5	NA	NA	NA	NA	NA	NA	18200	17500
	DUP-080910	8/9/2010	15:44	15	112	8.15 J	NA	< 0.240	1.52	0.8 J	NA	NA	43.4	NA	< 0.118	NA	< 0.118	18400	18600
	GP-10-24-025	8/9/2010	16:30	25	NA	NA	NA	NA	1.61	0.39 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-24-035	8/9/2010	17:05	35	NA	NA	NA	NA	5.03	0.89 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-24-045	8/9/2010	17:45	45	NA	NA	NA	NA	303	310	125	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-24-055	8/9/2010	18:30	55	NA	NA	NA	NA	629	615	250	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-25	GP-10-25-025	8/10/2010	10:00	25	NA	NA	NA	NA	44	0.4 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-25-035	8/10/2010	10:45	35	4660	18.7 J	NA	NA	10.9	0.58 J	< 5	NA	NA	NA	NA	NA	NA	20100	18600
	DUP-081010	8/10/2010	10:45	35	4580	6.72 J	NA	< 0.24	10.9	1.18	NA	NA	38.8	NA	< 0.118	NA	< 0.118	19500	19400
	GP-10-25-045	8/10/2010	11:50	45	2060	11.3 J	NA	NA	37.3	35.1	5	NA	NA	NA	NA	NA	NA	42800	43600
	DUP2-081010	8/10/2010	11:50	45	2300	9.92 J	NA	< 0.48	38	34.9	NA	NA	51.9	NA	< 0.236	NA	< 0.236	41800	42800
GP-10-26	GP-10-26-011	8/11/2010	9:20	11	94	12.4	NA	NA	0.6	0.18 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-021	8/11/2010	10:20	21	777	12.2	NA	NA	2.07	0.39 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	DUP-081110	8/11/2010	10:20	21	584	9.64 J	NA	< 0.120	1.72	0.65	NA	NA	15.3	NA	< 0.059	NA	< 0.059	16100	15700
	GP-10-26-031	8/11/2010	10:35	31	NA	NA	NA	NA	2.86	0.54	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-041	8/11/2010	11:05	41	NA	NA	NA	NA	4	0.45 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-051	8/11/2010	12:15	51	NA	NA	NA	NA	4.86 J	< 1.13	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-061	8/11/2010	13:40	61	NA	NA	NA	NA	6.48	< 1.13	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-071	8/11/2010	14:10	71	NA	NA	NA	NA	3.58 J	1.96 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-27	GP-10-27-025	8/11/2010	16:05	25	891	16.2	NA	NA	2.77	1.03	< 5	NA	NA	NA	NA	NA	NA	5570	5210
	DUP2-081110	8/11/2010	16:05	25	789	17.1	NA	< 0.120	1.11	0.38 J	NA	NA	14.8	NA	< 0.059	NA	< 0.059	5550	5380
	GP-10-27-035	8/11/2010	17:00	35	NA	NA	NA	NA	24.7	0.78 J	< 5	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-27-045	8/11/2010	17:25	45	NA	NA	NA	NA	199	200	70	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-27-055	8/11/2010	17:50	55	NA	NA	NA	NA	288	328	70	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-27-065	8/11/2010	18:45	65	NA	NA	NA	NA	1100	1040	> 500	NA	NA	NA	NA	NA	NA	NA	NA

Notes

NA - Not Applicable  
ug/L is micrograms per liter

mg/L - milligrams per liter  
J means estimated results

B indicates that analyte was detected in the associated method blank



**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Chromium		Cobalt		Copper		Iron		Lead		Magnesium		Manganese		Mercury	
					Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
GP-10-11	GP-10-11-039	8/3/2010	14:10	39	2.32	NA	NA	NA	NA	NA	67200	66400	0.74 J	NA	2610	NA	2120	NA	NA	NA
	GP-10-11-049	8/3/2010	15:15	49	271	NA	NA	NA	NA	NA	164000	49300	68.3	NA	13200	NA	5240	NA	NA	NA
	DUP3-080310	8/3/2010	15:15	49	254	NA	NA	NA	NA	NA	149000	52200	58	NA	9680	NA	5260	NA	NA	NA
	GP-10-11-059	8/3/2010	19:00	55	264	< 0.744	NA	19.5	NA	0.72 J	148000	28500	76.6	< 0.200	15600	3930	7700	5580	NA	0.09013 J
	GP-10-11-064	8/4/2010	11:30	64	744	0.6	NA	3.39	NA	0.49 J	180000	3440	65.2	0.18 J	30600 J	7570 J	7160	1100 J	NA	0.03814 J
GP-10-12	GP-10-12-044	8/5/2010	13:05	44	66.9	< 1.86	NA	10.9	NA	< 1.18	122000	83700	496	< 0.500	5900	2080	7180	5860	NA	0.02717 J
	GP-10-12-054	8/5/2010	15:00	54	NA	< 1.86	NA	4.18 J	NA	< 1.18	NA	74800	NA	< 0.500	NA	7500	NA	5200	NA	0.03853 J
	GP-10-12-065	8/9/2010	8:20	65	NA	< 0.744	NA	1.7 J	NA	0.66 J	NA	16600	NA	0.23 J	NA	5730	NA	4400	NA	0.1247 J
GP-10-13	GP-10-13-039	8/9/2010	14:45	39	136	2.22	NA	1.49	NA	0.32 J	148000	99500	38.9	0.05 J	17600	7600	1950	1380	NA	0.1389 J
	GP-10-13-049	8/9/2010	17:00	49	NA	2.66	NA	6.98	NA	2.62	NA	7840	NA	0.54 J	NA	19200	NA	6700	NA	< 0.012
	GP-10-13-059	8/10/2010	9:05	59	48.4	1.55	NA	0.79	NA	0.38 J	87100	74500	17	< 0.05	16400	14100	682	592	NA	< 0.012
	GP-10-13-069	8/10/2010	11:15	69	NA	< 1.86	NA	10.5	NA	< 1.18	NA	79800	NA	< 0.5	NA	7960	NA	3630	NA	< 0.012
	GP-10-13-079	8/10/2010	13:10	79	NA	0.26 J	NA	1.43	NA	0.98	NA	5580	NA	0.12 J	NA	3850	NA	218	NA	< 0.012
GP-10-14	GP-10-14-039	8/16/2010	09:50	39	15.2	0.61	NA	0.31 J	NA	0.27 J	22800	18700	4.17	< 0.050	7610	7010	783	670 J	NA	0.01239 J
	GP-10-14-049	8/16/2010	11:20	49	7.8	< 0.744	NA	1.51 J	NA	< 0.472	66000	66900	3.61	< 0.200	4370	3880	2420	2540	NA	< 0.0120
	DUP-081610	8/16/2010	11:20	49	14.2	< 0.744	NA	1.4 J	NA	< 0.472	69800	64200	9.02	< 0.200	5130	3750	2510	2440	NA	< 0.0120
	GP-10-14-059	8/16/2010	13:00	59	NA	< 1.86	NA	13	NA	< 1.18	NA	88200	NA	< 0.500	NA	4730	NA	6800	NA	< 0.012
	GP-10-14-069	8/16/2010	14:35	69	22.1	< 1.86	NA	21.5	NA	< 1.18	95400	85400	5.56	< 0.500	4250	3020	3700	3540	NA	< 0.0120
	GP-10-14-079	8/17/2010	07:45	79	20.9	< 1.86	14.2	8.83	24	< 1.18	80300	71800	10.3	0.59 J	5100	3390	5850	5540	< 0.0120	0.05669 J
GP-10-15	GP-10-15-039	8/11/2010	9:30	39	NA	1.52 J	NA	8.62	NA	< 0.472	NA	101000	NA	< 0.200	NA	4500	NA	3410	NA	0.04278 J
	GP-10-15-049	8/11/2010	11:25	49	5.05 J	< 1.85	NA	41.2	NA	< 1.18	126000	119000	2.98 J	< 0.500	7360	6920	10500	10500	NA	0.03205 J
	GP-10-15-059	8/11/2010	11:15	59	NA	0.51	NA	0.64	NA	2.22	NA	300	NA	0.050	NA	3950	NA	466	NA	0.01120
GP-10-16	GP-10-16-024	8/17/2010	16:15	24	106	0.22 J	71	3.85	83.8	0.25 J	56700	323	40.7	< 0.050	10700	1170	2500	182	0.04641 J	0.1034 J
	DUP-081710	8/17/2010	16:15	24	113	0.38 J	73.2	4.22	87.2	0.37 J	59500	349	41.2	< 0.050	117000	1290	2650	197	0.06234 J	0.1319 J
	GP-10-16-034	8/18/2010	07:55	34	284	0.22 J	122	3.2	272	0.33 J	145000	138	245	0.06 J	24700 J	2030	5080	580	0.2714 J	< 0.0120
	GP-10-16-054	8/18/2010	11:20	54	25	0.43 J	3.84	0.74	23.6	1.45	8900	277	22	0.07 J	4860	3500	180	84	< 0.0120	< 0.0120
	DUP-081810	8/18/2010	11:20	54	30	0.38 J	4.57	0.75	27.4	1.21	11400	300	25.6	0.08 J	5310	3610	200	86	0.03683 J	< 0.0120
	GP-10-16-064	8/18/2010	13:40	64	NA	0.36 J	NA	26	NA	0.47 J	NA	44700	NA	0.13 J	NA	6080	NA	777	NA	< 0.0120
	GP-10-16-074	8/19/2010	07:45	74	44.2	0.75	6.41	4.66	14.3	0.86	75900	64200	4.79	0.07 J	12800	11800	1420 J	1330 J	< 0.012	< 0.012
	GP-10-16-084	8/19/2010	09:40	84	10.5	< 0.744	7.11	5.45	9.33	0.61 J	20600	17200	1.73 J	< 0.2	18900	18200	3120	2920	< 0.012	< 0.012
	DUP-081910	8/19/2010	09:40	84	12.7	< 0.744	7.3	5.56	9.19	1.04 J	21500	17400	2.23	0.2 J	19700	18300	3130	2990	< 0.012	< 0.012
	GP-10-16-094	8/19/2010	12:35	94	48.8	< 0.186	5.08	1.54	192	4.32	17500	625	8.58	0.1 J	5320	4100	620	368	< 0.012	< 0.012
GP-10-17	GP-10-17-009	8/2/2010	11:40	9	NA	NA	NA	NA	NA	NA	1800 J	1620	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-019	8/2/2010	12:20	19	NA	NA	NA	NA	NA	NA	1870	1800	NA	NA	NA	NA	NA	NA	NA	NA
	DUP-080210	8/2/2010	12:20	19	NA	NA	NA	NA	NA	NA	1840	1870	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-029	8/2/2010	16:00	29	NA	NA	NA	NA	NA	NA	1810	1240	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-039	8/2/2010	16:45	39	NA	NA	NA	NA	NA	NA	65200	60700	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-049	8/2/2010	17:30	49	NA	NA	NA	NA	NA	NA	10100	5210	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-056	8/2/2010	17:45	56	NA	NA	NA	NA	NA	NA	30600	6100	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-18	GP-10-18-007	8/2/2010	18:34	7	NA	NA	NA	NA	NA	NA	1390	1360	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-017	8/3/2010	8:25	17	NA	NA	NA	NA	NA	NA	1190	857	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-027	8/3/2010	9:00	27	NA	NA	NA	NA	NA	NA	35400	32000	NA	NA	NA	NA	NA	NA	NA	NA
	DUP-080310	8/3/2010	9:00	27	NA	NA	NA	NA	NA	NA	34600	32800	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-037	8/3/2010	11:00	37	NA	NA	NA	NA	NA	NA	21300	18800	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-047	8/3/2010	12:10	47	NA	NA	NA	NA	NA	NA	35200	32300	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-19	GP-10-19-009	8/3/2010	14:35	9	NA	NA	NA	NA	NA	NA	1040	908	NA	NA	NA	NA	NA	NA	NA	NA
	DUP2-080310	8/3/2010	14:35	9	NA	NA	NA	NA	NA	NA	1030	982	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-019	8/3/2010	15:15	19	NA	NA	NA	NA	NA	NA	3680	831	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-029	8/3/2010	16:05	29	NA	NA	NA	NA	NA	NA	89800	73300	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-039	8/3/2010	17:00	39	NA	NA	NA	NA	NA	NA	65600	58800	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-046	8/3/2010	18:15	46	NA	NA	NA	NA	NA	NA	14400	4280	NA	NA	NA	NA	NA	NA	NA	NA

**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Chromium		Cobalt		Copper		Iron		Lead		Magnesium		Manganese		Mercury	
					Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
GP-10-20	GP-10-20-009	8/4/2010	9:30	9	NA	NA	NA	NA	NA	NA	2000	1260	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-20-019	8/4/2010	10:10	19	3.25	0.51	NA	NA	NA	NA	2910	1500	0.79 J	0.06 J	1840	1570	989	920	NA	NA
	DUP-080410	8/4/2010	10:10	19	3.31	0.43 J	NA	2.09	NA	J	2630	1630	0.99 J	< 0.050	1750	1620	949	933	NA	< 0.0120
	GP-10-20-029	8/4/2010	11:00	29	NA	NA	NA	NA	NA	NA	53000	56800	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-20-039	8/4/2010	13:00	39	NA	NA	NA	NA	NA	NA	16800	13300	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-21	GP-10-21-011	8/4/2010	15:05	11	NA	NA	NA	NA	NA	NA	2550	501	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-021	8/4/2010	15:45	21	3.23	0.43 J	NA	NA	NA	NA	1730	984	0.53 J	< 0.010	2760	2580	1050	1020 J	NA	NA
	DUP2-080410	8/4/2010	15:45	21	2.76	0.52 J	NA	NA	NA	NA	1550	1030	0.9 J	< 0.100	2690	2780	1020	1080	NA	NA
	GP-10-21-031	8/4/2010	16:30	31	NA	NA	NA	NA	NA	NA	3100	1840	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-041	8/4/2010	17:00	41	NA	NA	NA	NA	NA	NA	42500	43700	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-051	8/4/2010	18:05	51	NA	NA	NA	NA	NA	NA	11900	6320	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-060	8/4/2010	19:00	60	NA	NA	NA	NA	NA	NA	21200	15300	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-22	GP-10-22-011	8/10/2010	14:40	11	NA	NA	NA	NA	NA	NA	844	753	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-021	8/10/2010	15:00	21	NA	NA	NA	NA	NA	NA	2310	1120	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-031	8/10/2010	15:50	31	NA	NA	NA	NA	NA	NA	3240	1780	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-041	8/10/2010	16:30	41	NA	NA	NA	NA	NA	NA	35300	36100	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-051	8/10/2010	17:30	51	NA	NA	NA	NA	NA	NA	7580	5010	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-061	8/10/2010	18:30	61	NA	NA	NA	NA	NA	NA	6750	4490	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-23	GP-10-23-017	8/5/2010	11:00	17	0.33 J	0.2 J	NA	NA	NA	NA	1110	1040	0.12 J	0.06 J	1450	1450	23	21.1	NA	NA
	DUP-080510	8/5/2010	11:00	17	0.46 J	0.22 J	NA	0.37 J	NA	0.49 J	1180	1070	0.11 J	< 0.050	1540	1530	23.9	21.8	NA	0.1147 J
	GP-10-23-027	8/5/2010	11:45	27	5.24	< 0.372	NA	NA	NA	NA	2170	701	1.62	< 0.100	1760	1640	189	172	NA	NA
	GP-10-23-037	8/5/2010	12:25	37	NA	NA	NA	NA	NA	NA	5400	1890	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-23-047	8/5/2010	14:20	47	NA	NA	NA	NA	NA	NA	38500	38400	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-23-057	8/5/2010	16:05	57	32.4	0.930	NA	NA	NA	NA	75200	68400	3.15	< 0.250	15700	15400	3660	3730	NA	NA
	DUP2-080510	8/5/2010	16:05	57	45	0.95 J	NA	27.5	NA	< 0.590	82000	70000	4.25	< 0.250	17300	15600	4050	3820	NA	0.07912 J
GP-10-24	GP-10-24-015	8/9/2010	15:44	15	0.57 J	< 0.372	NA	NA	NA	NA	928	758	0.16 J	< 0.100	2220	2090	28.1	24.9	NA	NA
	DUP-080910	8/9/2010	15:44	15	0.51 J	< 0.372	NA	0.42 J	NA	0.62 J	880	765	0.16 J	< 0.100	2200	2210	26.7	30.6	NA	< 0.0120
	GP-10-24-025	8/9/2010	16:30	25	NA	NA	NA	NA	NA	NA	2260	1180	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-24-035	8/9/2010	17:05	35	NA	NA	NA	NA	NA	NA	5550	2630	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-24-045	8/9/2010	17:45	45	NA	NA	NA	NA	NA	NA	99000	100000	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-24-055	8/9/2010	18:30	55	NA	NA	NA	NA	NA	NA	91100	81500	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-25	GP-10-25-025	8/10/2010	10:00	25	NA	NA	NA	NA	NA	NA	35700	1770 J	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-25-035	8/10/2010	10:45	35	74.3	1.08	NA	NA	NA	NA	15600	2250	25.5	0.15 J	3420	2200	801	618	NA	NA
	DUP-081010	8/10/2010	10:45	35	74.1	0.94 J	NA	1.15	NA	0.72 J	15300	2320	25.7	< 0.1	3350	2280	772	658	NA	< 0.012
	GP-10-25-045	8/10/2010	11:50	45	55	0.78 J	NA	NA	NA	NA	76700	71000	13.8	< 0.2	5530	5170	4540	4550	NA	NA
	DUP2-081010	8/10/2010	11:50	45	57.4	< 0.744	NA	45.2	NA	< 0.472	76700	69000	12.5	< 0.2	5510	5070	4460	4430	NA	< 0.012
GP-10-26	GP-10-26-011	8/11/2010	9:20	11	NA	< 0.186	NA	NA	NA	NA	854	716 J	0.14 J	0.08 J	1240	1190	67.1	59.8	NA	NA
	GP-10-26-021	8/11/2010	10:20	21	NA	0.32 J	NA	NA	NA	NA	2090	1170	0.63	0.13 J	1960	1990	129	103	NA	NA
	DUP-081110	8/11/2010	10:20	21	3.99	0.22 J	NA	1.31	NA	0.63	1800	1140	0.54	< 0.050	1820	1900	120	103	NA	< 0.0120
	GP-10-26-031	8/11/2010	10:35	31	NA	NA	NA	NA	NA	NA	4180	1350	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-041	8/11/2010	11:05	41	NA	NA	NA	NA	NA	NA	6290	1940	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-051	8/11/2010	12:15	51	NA	NA	NA	NA	NA	NA	7180	3140	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-061	8/11/2010	13:40	61	NA	NA	NA	NA	NA	NA	11900	3840	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-071	8/11/2010	14:10	71	NA	NA	NA	NA	NA	NA	6430	3310	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-27	GP-10-27-025	8/11/2010	16:05	25	3.71	0.34 J	NA	NA	NA	NA	1640	773	2.03	0.08 J	1140	960	56.2	44.9	NA	NA
	DUP2-081110	8/11/2010	16:05	25	3.16	0.33 J	NA	0.56	NA	0.44 J	1510	804	1.73	0.06 J	1120	984	53	45.5	NA	< 0.0120
	GP-10-27-035	8/11/2010	17:00	35	NA	NA	NA	NA	NA	NA	15000	1100	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-27-045	8/11/2010	17:25	45	NA	NA	NA	NA	NA	NA	88800	83800	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-27-055	8/11/2010	17:50	55	NA	NA	NA	NA	NA	NA	84100	91300	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-27-065	8/11/2010	18:45	65	NA	NA	NA	NA	NA	NA	73400	61300	NA	NA	NA	NA	NA	NA	NA	NA

Notes: NA - Not Applicable      mg/L - milligrams per liter      J indicates that analyte was detected in the associated method blank  
ug/L is micrograms per liter      J means estimated results



**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Nickel		Potassium		Selenium		Silver		Sodium		Thallium		Vanadium		Zinc	
					Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
GP-10-11	GP-10-11-039	8/3/2010	14:10	39	9.34	NA	3070	NA	NA	NA	NA	NA	8650	NA	NA	NA	NA	NA	NA	NA
	GP-10-11-049	8/3/2010	15:15	49	134	NA	11900	NA	NA	NA	NA	NA	16600	NA	NA	NA	NA	NA	NA	NA
	DUP3-080310	8/3/2010	15:15	49	112	NA	10700	NA	NA	NA	NA	NA	16000	NA	NA	NA	NA	NA	NA	NA
	GP-10-11-059	8/3/2010	19:00	55	142	5.81	10500	4240	NA	< 1.62	NA	< 0.340	25300	20000	NA	< 0.124	NA	< 0.308	NA	8.81 J
	GP-10-11-064	8/4/2010	11:30	64	207	7.33	40200	25400 J	NA	0.42 J	NA	< 0.085	61200	49200 J	NA	< 0.031	NA	0.2 J	NA	1.81 J
GP-10-12	GP-10-12-044	8/5/2010	13:05	44	56.1	20.3	7630	4670	NA	< 4.06	NA	< 0.850	5160	3650	NA	< 0.310	NA	< 0.770	NA	44.4 J
	GP-10-12-054	8/5/2010	15:00	54	NA	10.6	NA	3340	NA	4.06	NA	< 0.850	NA	8450	NA	< 0.310	NA	< 0.770	NA	38.2 J
	GP-10-12-065	8/9/2010	8:20	65	NA	8.34	NA	17200	NA	< 1.62	NA	< 0.340	NA	31000	NA	< 0.124	NA	< 0.308	NA	24.5
GP-10-13	GP-10-13-039	8/9/2010	14:45	39	72.1	4.85	19000	14300	NA	0.57 J	NA	< 0.085	19400	16800	NA	< 0.031	NA	0.71	NA	4.39 J
	GP-10-13-049	8/9/2010	17:00	49	NA	6.88	NA	19200	NA	< 2.03	NA	< 0.425	NA	51600	NA	< 0.155	NA	< 0.385	NA	12.9 J
	GP-10-13-059	8/10/2010	9:05	59	35.4	4.75	18400	17400	NA	0.57 J	NA	< 0.085	26900	24600	NA	< 0.031	NA	0.34 J	NA	1.98 J
	GP-10-13-069	8/10/2010	11:15	69	NA	9.15	NA	9000	NA	< 4.06	NA	< 0.85	NA	13900	NA	< 0.31	NA	< 0.77	NA	26.6 J
	GP-10-13-079	8/10/2010	13:10	79	NA	4.42	NA	4700	NA	< 0.406	NA	< 0.085	NA	35900	NA	< 0.031	NA	0.14 J	NA	7.59
GP-10-14	GP-10-14-039	8/16/2010	09:50	39	11.2	3	4860	4160	NA	0.54 J	NA	< 0.085	16800	17800	NA	< 0.031	NA	0.36 J	NA	4.59 J
	GP-10-14-049	8/16/2010	11:20	49	9.25	3.05	7640	7140	NA	< 1.62	NA	< 0.340	7280	7780	NA	< 0.124	NA	1.81 J	NA	< 6.50
	DUP-081610	8/16/2010	11:20	49	18.1	2.95	8080	6940	NA	< 1.62	NA	< 0.340	7600	7390	NA	< 0.124	NA	1.62 J	NA	< 6.50
	GP-10-14-059	8/16/2010	13:00	59	NA	4.75 J	NA	6940	NA	< 4.06	NA	< 0.850	NA	14000	NA	< 0.310	NA	< 0.770	NA	23.6 J
	GP-10-14-069	8/16/2010	14:35	69	21.2	8.73	7860	6680	NA	< 4.06	NA	< 0.850	5580	5180	NA	< 0.310	NA	< 0.770	NA	< 16.2
	GP-10-14-079	8/17/2010	07:45	79	27.6	14	5480	3780	< 4.06	< 4.06	< 0.850	< 0.850	6270	5720	< 0.310	< 0.310	10.1	< 0.770	73.2	40.2 J
GP-10-15	GP-10-15-039	8/11/2010	9:30	39	NA	8.06	NA	8240	NA	< 1.62	NA	< 0.340	NA	7280	NA	< 0.124	NA	< 0.308	NA	9.26 J
	GP-10-15-049	8/11/2010	11:25	49	23.5	19.5	8130	7520	NA	< 4.06	NA	< 0.850	12200	12000	NA	< 0.310	NA	< 0.770	NA	18.7 J
	GP-10-15-059	8/11/2010	14:45	59	NA	2.19	NA	6110	NA	0.406	NA	< 0.085	NA	32300	NA	0.04 J	NA	2.23	NA	3.05 J
GP-10-16	GP-10-16-024	8/17/2010	16:15	24	130	4.82	8990	2520	3.17 J	< 0.406	0.38 J	< 0.085	4950	2960	0.64 J	0.04 J	46.6	0.13 J	157	3.53 J
	DUP-081710	8/17/2010	16:15	24	136	5.22	9420	2700	2.9 J	< 0.406	< 0.34	< 0.085	4880	3060	0.61 J	< 0.031	50.2	0.14 J	160	3.36 J
	GP-10-16-034	8/18/2010	07:55	34	229	2.93	17100	6630	6.39 J	< 0.406	0.58 J	< 0.085	17600	9100	1.91 J	0.1 J	109	0.2 J	298	3.37 J
	GP-10-16-054	8/18/2010	11:20	54	14.4	2.21	5840	4810	0.82 J	0.43 J	0.29 J	< 0.085	35600	36000	0.1 J	0.04 J	7.83	0.29 J	40.2	6.01
	DUP-081810	8/18/2010	11:20	54	18	2.27	6060	5040	0.93 J	< 0.406	< 0.085	< 0.085	35800	36700	0.1 J	< 0.031	10.4	0.42 J	47.5	4.15 J
	GP-10-16-064	8/18/2010	13:40	64	NA	12.8	NA	12000	NA	< 0.406	NA	< 0.085	NA	16600	NA	< 0.031	NA	0.21 J	NA	3.97 J
	GP-10-16-074	8/19/2010	07:45	74	24.6	16.6	21500 J	20400 J	0.64 J	0.47 J	< 0.085	< 0.085	33000 J	31700 J	0.06 J	< 0.031	3.08	0.1 J	24	6.87
	GP-10-16-084	8/19/2010	09:40	84	12.2	7.8	6240	5370	< 1.62	< 1.62	< 0.34	< 0.34	45200	42200	< 0.124	< 0.124	1.71 J	< 0.308	13.9 J	14.2 J
	DUP-081910	8/19/2010	09:40	84	13.7	8.2	6570	5500	< 1.62	< 1.62	< 0.34	< 0.34	45200	42100	< 0.124	< 0.124	2.54	< 0.308	13.9 J	14.4 J
	GP-10-16-094	8/19/2010	12:35	94	23.3	8.07	6660	5210	0.58 J	< 0.406	< 0.085	< 0.085	36600	34200	0.07 J	< 0.031	3.78	0.22 J	24.7	4.84 J
	GP-10-17-009	8/2/2010	11:40	9	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-17	GP-10-17-019	8/2/2010	12:20	19	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	DUP-080210	8/2/2010	12:20	19	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-029	8/2/2010	16:00	29	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-039	8/2/2010	16:45	39	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-049	8/2/2010	17:30	49	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-056	8/2/2010	17:45	56	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-18	GP-10-18-007	8/2/2010	18:34	7	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-017	8/3/2010	8:25	17	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-027	8/3/2010	9:00	27	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	DUP-080310	8/3/2010	9:00	27	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-037	8/3/2010	11:00	37	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-19	GP-10-19-009	8/3/2010	14:35	9	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	DUP2-080310	8/3/2010	14:35	9	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-019	8/3/2010	15:15	19	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-029	8/3/2010	16:05	29	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-039	8/3/2010	17:00	39	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-046	8/3/2010	18:15	46	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA



**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Nickel		Potassium		Selenium		Silver		Sodium		Thallium		Vanadium		Zinc	
					Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
GP-10-20	GP-10-20-009	8/4/2010	9:30	9	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-20-019	8/4/2010	10:10	19	8.04	4.71	4290	3700	NA	NA	NA	NA	129000	119000	NA	NA	NA	NA	NA	NA
	DUP-080410	8/4/2010	10:10	19	7.24	5.21	1170	3700	NA	0.59 J	NA	< 0.085	128000	122000	NA	0.07 J	NA	0.15 J	NA	5.18
	GP-10-20-029	8/4/2010	11:00	29	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-20-039	8/4/2010	13:00	39	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-21	GP-10-21-011	8/4/2010	15:05	11	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-021	8/4/2010	15:45	21	8.51	7.25	4690	4520	NA	NA	NA	NA	155000	153000	NA	NA	NA	NA	NA	NA
	DUP2-080410	8/4/2010	15:45	21	8.01	7.48	4540	4790	NA	NA	NA	NA	147000	149000	NA	NA	NA	NA	NA	NA
	GP-10-21-031	8/4/2010	16:30	31	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-041	8/4/2010	17:00	41	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-051	8/4/2010	18:05	51	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-060	8/4/2010	19:00	60	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-22	GP-10-22-011	8/10/2010	14:40	11	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-021	8/10/2010	15:00	21	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-031	8/10/2010	15:50	31	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-041	8/10/2010	16:30	41	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-051	8/10/2010	17:30	51	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-22-061	8/10/2010	18:30	61	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-23	GP-10-23-017	8/5/2010	11:00	17	1.94	1.83	2260	2130	NA	NA	NA	NA	67100	65000	NA	NA	NA	NA	NA	NA
	DUP-080510	8/5/2010	11:00	17	2.04	1.87	2330	2300	NA	<0.406	NA	<0.085	71000	69100	NA	<0.031	NA	0.12 J	NA	1.95 J
	GP-10-23-027	8/5/2010	11:45	27	3.88	2.13	4670	4640	NA	NA	NA	NA	218000	217000 J	NA	NA	NA	NA	NA	NA
	GP-10-23-037	8/5/2010	12:25	37	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-23-047	8/5/2010	13:20	47	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-23-057	8/5/2010	16:05	57	14.6	24.4	12000	11300	NA	NA	NA	NA	36600	36100	NA	NA	NA	NA	NA	NA
	DUP2-080510	8/5/2010	16:05	57	39.9	25	13300	11500	NA	<2.03	NA	<0.425	38000	37200	NA	<0.155	NA	<0.385	NA	32.6
GP-10-24	GP-10-24-015	8/9/2010	15:44	15	1.5	1.34	3890	3690	NA	NA	NA	NA	147000	135000	NA	NA	NA	NA	NA	NA
	DUP-080910	8/9/2010	15:44	15	1.52	1.37	3810	3920	NA	<0.812	NA	<0.170	147000	143000	NA	<0.062	NA	<0.154	NA	6.33 J
	GP-10-24-025	8/9/2010	16:30	25	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-24-035	8/9/2010	17:05	35	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-24-045	8/9/2010	17:45	45	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-24-055	8/9/2010	18:30	55	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-25	GP-10-25-025	8/10/2010	10:00	25	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-25-035	8/10/2010	10:45	35	28.2	6.42	6650	5240	NA	NA	NA	NA	198000	186000	NA	NA	NA	NA	NA	NA
	DUP-081010	8/10/2010	10:45	35	27.4	6.51	6500	5590	NA	<0.812	NA	<0.17	196000	202000	NA	0.11 J	NA	<0.154	NA	15.7
	GP-10-25-045	8/10/2010	11:50	45	23.5	9.54	7680	7120	NA	NA	NA	NA	52500	51900	NA	NA	NA	NA	NA	NA
	DUP2-081010	8/10/2010	11:50	45	24.5	9.69	7790	7040	NA	<1.62	NA	<0.34	50700	52600	NA	0.21 J	NA	<0.308	NA	35.9
GP-10-26	GP-10-26-011	8/11/2010	9:20	11	3.15	2.99	3570	3390	NA	NA	NA	NA	13100	14300	NA	NA	NA	NA	NA	NA
	GP-10-26-021	8/11/2010	10:20	21	5.68	4.15	3160	3280	NA	NA	NA	NA	33100	35000	NA	NA	NA	NA	NA	NA
	DUP-081110	8/11/2010	10:20	21	4.99	3.98	3020	3210	NA	0.79 J	NA	<0.085	37300	34200	NA	<0.031	NA	0.19 J	NA	11.8
	GP-10-26-031	8/11/2010	10:35	31	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-041	8/11/2010	11:05	41	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-051	8/11/2010	12:15	51	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-061	8/11/2010	13:40	61	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-27	GP-10-27-025	8/11/2010	16:05	25	3.71	2.37	3180	3260	NA	NA	NA	NA	55200	52600	NA	NA	NA	NA	NA	NA
	DUP2-081110	8/11/2010	16:05	25	3.48	2.17	3160	3210	NA	<0.406	NA	<0.085	57400	53000	NA	<0.031	NA	0.21 J	NA	3.27 J
	GP-10-27-035	8/11/2010	17:00	35	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-27-045	8/11/2010	17:25	45	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-27-055	8/11/2010	17:50	55	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-27-065	8/11/2010	18:45	65	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA

Notes

NA - Not Applicable  
ug/L is micrograms per liter

mg/l - milligrams per liter  
J means estimated results

B indicates that analyte was detected in the associated method blank



**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Turbidity NTU	DO mg/L	pH	Temp Celsius	Spec Cond uS/cm	ORP mV	Color	Hardness mg/l	Alkalinity mg CaCO3/L	TDS mg/l	TSS mg/l	Chloride mg/l	Ammonia mg/l	Nitrite mg/l	Nitrate mg/l
GP-10-11	GP-10-11-039	8/3/2010	14:10	39	14.5	0.44	5.61	16.26	302	56.2	Clear	NA	170	NA	200	21	2.29	< 0.002	0.031 J
	GP-10-11-049	8/3/2010	15:15	49	5373	0.27	6.2	18.09	278	-43.7	Cloudy	NA	180	NA	7700	13	3.36	< 0.002	0.046 J
	DUP3-080310	8/3/2010	15:15	49	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-11-059	8/3/2010	19:00	55	203	0.78	6.3	24.09	354	-46.3	Cloudy	NA	210	NA	13000	25	0.0281 J	< 0.002	0.04 J
	GP-10-11-064	8/4/2010	11:30	64	Max	0.11	7.74	20.99	439	-150.4	Silty	NA	380	NA	55000	22	1.29	< 0.002	0.045 J
GP-10-12	GP-10-12-044	8/5/2010	13:05	44	203	0.43	5.97	18.23	385	17.6	Sl Cloudy	NA	230	NA	1300	3.3	3.6	< 0.002	0.028 J
	GP-10-12-054	8/5/2010	15:00	54	Max	0.16	6.11	21.93	368	-17.1	Silty	NA	220	NA	NA	7.6	3.14	< 0.002	0.05
	GP-10-12-065	8/9/2010	8:20	65	Max	0.13	6.79	12.95	543	-103.3	Silty	NA	240	NA	NA	26	1.09	0.01 J	0.14
GP-10-13	GP-10-13-039	8/9/2010	14:45	39	1409	0.18	5.36	21.58	740	101.2	Cloudy	NA	460	NA	2500	11	14.2	< 0.002	0.03 J
	GP-10-13-049	8/9/2010	17:00	49	144	0.48	6.17	21.68	858	45.5	Cloudy	NA	490	NA	NA	46	17.3	< 0.002	0.024 J
	GP-10-13-059	8/10/2010	9:05	59	565	0.16	6.4	18.34	800	-33.3	Cloudy	NA	470	NA	890	17	14.3	< 0.002	0.06
	GP-10-13-069	8/10/2010	11:15	69	151	0.81	6.09	21.32	545	-2.1	Cloudy	NA	310	NA	NA	20	5.91	< 0.002	0.07
	GP-10-13-079	8/10/2010	13:10	79	128	8.68	6.37	21.89	338	15.9	Cloudy	NA	77	NA	NA	66	0.384	0.01 J	0.37
GP-10-14	GP-10-14-039	8/16/2010	09:50	39	49.9	0.36	5.54	15.86	510	50.8	Cloudy	NA	300	NA	270	11	11.5	< 0.002	0.04 J
	GP-10-14-049	8/16/2010	11:20	49	22.5	0.41	5.86	15.99	474	14.9	Clear	NA	290	NA	320	4.6	7.44	< 0.002	0.028 J
	DUP-081610	8/16/2010	11:20	49	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-14-059	8/16/2010	13:00	59	1129	0.17	5.86	16.31	553	-0.9	Silty	NA	340	NA	NA	9.6	6.46	< 0.002	0.03 J
	GP-10-14-069	8/16/2010	14:35	69	111	0.18	5.82	17.71	444	-8.7	Cloudy	NA	270	NA	620	3.3	4.65	< 0.002	0.014 J
	GP-10-14-079	8/17/2010	07:45	79	38.8	0.31	6.18	14.71	395	34.2	Clear	NA	210	NA	170	5.7	2.67	0.01 J	< 0.01
GP-10-15	GP-10-15-039	8/11/2010	9:30	39	25.52	0.25	5.81	17.99	543	-6.4	Silty	NA	340	NA	NA	5	7.52	< 0.002	0.06
	GP-10-15-049	8/11/2010	11:25	49	41.3	0.45	6	20.68	589	-40.5	Clear	NA	330	NA	190	12	2.61	< 0.002	0.05
	GP-10-15-059	8/11/2010	11:45	59	207	5.11	8.3	21.89	313	181.1	Cloudy	NA	89	NA	NA	59	0.508	0.01 J	0.18
GP-10-16	GP-10-16-024	8/17/2010	16:15	24	1235	3.06	6.27	12.58	107	101.1	Silty	NA	33	NA	3900	3.6	0.0455 J	< 0.002	0.65
	DUP-081710	8/17/2010	16:15	24	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-16-034	8/18/2010	07:55	34	609	12.11	8.25	13.91	350	78.3	Silty	NA	51	NA	3000	15	0.079	< 0.002	0.24
	GP-10-16-054	8/18/2010	11:20	54	101.4	12.62	7.43	16.85	398	27.4	Cloudy	NA	74	NA	160	64	0.173	0.01 J	0.44
	DUP-081810	8/18/2010	11:20	54	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-16-064	8/18/2010	13:40	64	21.5	2.45	6.57	14.73	492	-78.8	Clear	210	210	NA	NA	7.1	6.98	< 0.002	< 0.01
	GP-10-16-074	8/19/2010	07:45	74	122	0.66	6.94	11.26	720	-140.3	Cloudy	NA	160	NA	390	56	1.71	0.01 J	0.43
	GP-10-16-084	8/19/2010	09:40	84	16.6	0.9	6.95	14.92	837	-104.8	Clear	NA	420	NA	290	43	0.224	0.01 J	< 0.01
	DUP-081910	8/19/2010	09:40	84	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-16-094	8/19/2010	12:35	94	180	5.06	6.9	17.45	382	-21.4	Cloudy	NA	110	NA	170	68	0.159	0.02	0.48
GP-10-17	GP-10-17-009	8/2/2010	11:40	9	20.1	4.91	1.65	14.07	1035	178.2	Clear	NA	NA	NA	9.8	NA	NA	NA	NA
	GP-10-17-019	8/2/2010	12:20	19	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	43	NA	NA	NA	NA
	DUP-080210	8/2/2010	12:20	19	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	11	NA	NA	NA	NA
	GP-10-17-029	8/2/2010	16:00	29	6.06	2.17	6.01	13.72	747	63.4	Clear	NA	NA	NA	8.5	NA	NA	NA	NA
	GP-10-17-039	8/2/2010	16:45	39	37.9	0.26	6.83	13.9	542	-138.2	Clear	NA	NA	NA	95	NA	NA	NA	NA
	GP-10-17-049	8/2/2010	17:30	49	65.6	1.4	6.52	14.8	670	-28.3	Little Cloudy	NA	NA	NA	290	NA	NA	NA	NA
	GP-10-17-056	8/2/2010	17:45	56	660	0.24	6.73	14.68	666	-84.3	Cloudy	NA	NA	NA	1700	NA	NA	NA	NA
GP-10-18	GP-10-18-007	8/2/2010	18:34	7	18.3	0.27	6.06	17.64	729	58.7	Clear	NA	NA	NA	13	NA	NA	NA	NA
	GP-10-18-017	8/3/2010	8:25	17	10.6	0.44	6.14	12.87	673	55.8	Clear	NA	NA	NA	7.5	NA	NA	NA	NA
	GP-10-18-027	8/3/2010	9:00	27	199	0.44	6.3	13.55	681	-45.1	Little Cloudy	NA	NA	NA	65	NA	NA	NA	NA
	DUP-080310	8/3/2010	9:00	27	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-037	8/3/2010	11:00	37	84.7	0.44	6.4	13.61	628	-45.5	Little Cloudy	NA	NA	NA	48	NA	NA	NA	NA
	GP-10-18-047	8/3/2010	12:10	47	127	0.45	6.54	14.6	809	-80.7	Little Cloudy	NA	NA	NA	160	NA	NA	NA	NA
GP-10-19	GP-10-19-009	8/3/2010	14:35	9	1.1	3.55	5.85	17.73	174	98.5	Clear	NA	NA	NA	< 5.0	NA	NA	NA	NA
	DUP2-080310	8/3/2010	14:35	9	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-019	8/3/2010	15:15	19	141	2.19	6.01	14.88	759	90.4	Clear	NA	NA	NA	70	NA	NA	NA	NA
	GP-10-19-029	8/3/2010	16:05	29	66.6	0.53	6.64	13.88	682	-111	Clear	NA	NA	NA	160	NA	NA	NA	NA
	GP-10-19-039	8/3/2010	17:00	39	36.6	1.65	6.6	15.59	736	-77.7	Clear	NA	NA	NA	89	NA	NA	NA	NA
	GP-10-19-046	8/3/2010	18:15	46	< 1000	1.88	6.50	14.58	737	-44.1	Cloudy	NA	NA	NA	440	NA	NA	NA	NA



**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Turbidity NTU	DO mg/L	pH	Temp Celsius	Spec Cond uS/cm	ORP mV	Color	Hardness mg/l	Alkalinity mg CaCO3/L	TDS mg/l	TSS mg/l	Chloride mg/l	Ammonia mg/l	Nitrite mg/l	Nitrate mg/l
GP-10-20	GP-10-20-009	8/4/2010	9:30	9	12.5	6.46	6.22	16.7	262	60.4	Clear	NA	NA	NA	150	NA	NA	NA	NA
	GP-10-20-019	8/4/2010	10:10	19	17.2	0.67	6.09	14.35	609	50.6	Clear	NA	NA	NA	16	NA	NA	NA	NA
	DUP-080410	8/4/2010	10:10	19	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-20-029	8/4/2010	11:00	29	139	0.33	6.7	13.44	521	-92.8	sl. Cloudy	NA	NA	NA	180	NA	NA	NA	NA
	GP-10-20-039	8/4/2010	13:00	39	91.6	0.37	6.49	13.51	649	-38.8	Clear	NA	NA	NA	120	NA	NA	NA	NA
GP-10-21	GP-10-21-011	8/4/2010	15:05	11	54.1	6.33	6.14	15.57	182	101.5	Clear	NA	NA	NA	88	NA	NA	NA	NA
	GP-10-21-021	8/4/2010	15:45	21	134	1.43	6.07	14.29	728	97.5	Little Cloudy	NA	NA	NA	53	NA	NA	NA	NA
	DUP2-080410	8/4/2010	15:45	21	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-21-031	8/4/2010	16:30	31	34.7	1.54	6.35	13.78	503	44.9	Clear	NA	NA	NA	50	NA	NA	NA	NA
	GP-10-21-041	8/4/2010	17:00	41	83.7	0.42	6.66	14.14	627	-80.2	Clear	NA	NA	NA	130	NA	NA	NA	NA
	GP-10-21-051	8/4/2010	18:05	51	315	0.32	6.56	16.8	277	60.9	Silty	NA	NA	NA	240	NA	NA	NA	NA
	GP-10-21-060	8/4/2010	19:00	60	<1000	0.72	6.68	16.59	828	-64.2	Silty	NA	NA	NA	240	NA	NA	NA	NA
GP-10-22	GP-10-22-011	8/10/2010	14:40	11	6.27	7.43	5.92	14.7	306	115.8	Clear	NA	NA	NA	<5	NA	NA	NA	NA
	GP-10-22-021	8/10/2010	15:00	21	45	0.63	6.19	13.42	440	75.5	Clear	NA	NA	NA	48	NA	NA	NA	NA
	GP-10-22-031	8/10/2010	15:50	31	54	0.72	6.22	13.22	766	68.1	Clear	NA	NA	NA	51	NA	NA	NA	NA
	GP-10-22-041	8/10/2010	16:30	41	85.4	0.99	6.38	13.3	434	-32.9	Clear	NA	NA	NA	68	NA	NA	NA	NA
	GP-10-22-051	8/10/2010	17:30	51	83.5	0.88	6.55	13.57	585	-20.9	Clear	NA	NA	NA	160	NA	NA	NA	NA
	GP-10-22-061	8/10/2010	18:30	61	29.9	1.02	6.77	13.28	75	-51.1	Clear	NA	NA	NA	670	NA	NA	NA	NA
GP-10-23	GP-10-23-017	8/5/2010	11:00	17	5.37	4.03	5.99	14.46	380	76.2	Clear	NA	NA	NA	<5.0	NA	NA	NA	NA
	DUP-080510	8/5/2010	11:00	17	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-23-027	8/5/2010	11:45	27	58.5	3.35	6.08	13.1	1060	94.3	Clear	NA	NA	NA	24	NA	NA	NA	NA
	GP-10-23-037	8/5/2010	12:25	37	58.4	3.41	5.96	13.75	961	90.9	Clear	NA	NA	NA	95	NA	NA	NA	NA
	GP-10-23-047	8/5/2010	14:20	47	374	1.31	6.44	15.59	490	-95.1	Cloudy	NA	NA	NA	200	NA	NA	NA	NA
	GP-10-23-057	8/5/2010	16:05	57	254	0.86	6.65	14.51	713	-100.2	Little Cloudy	NA	NA	NA	300	NA	NA	NA	NA
	DUP2-080510	8/5/2010	16:05	57	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-24	GP-10-24-015	8/9/2010	15:44	15	37.4	3.1	5.94	14.28	762	116.3	Clear	NA	NA	NA	7.4	NA	NA	NA	NA
	DUP-080910	8/9/2010	15:44	15	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-24-025	8/9/2010	16:30	25	44.9	5.21	6.05	13.23	710	104.8	Clear	NA	NA	NA	36	NA	NA	NA	NA
	GP-10-24-035	8/9/2010	17:05	35	45.3	1.12	5.94	14.08	914	92.4	Clear	NA	NA	NA	64	NA	NA	NA	NA
	GP-10-24-045	8/9/2010	17:45	45	98.6	1.07	6.54	13.61	1332	-71.5	Clear	NA	NA	NA	96	NA	NA	NA	NA
	GP-10-24-055	8/9/2010	18:30	55	<1000	0.77	6.61	13.41	914	-95.3	Cloudy	NA	NA	NA	440	NA	NA	NA	NA
GP-10-25	GP-10-25-025	8/10/2010	10:00	25	889	3.57	6.03	13.07	506	69.3	Cloudy	NA	NA	NA	730	NA	NA	NA	NA
	GP-10-25-035	8/10/2010	10:45	35	223	1.69	5.94	13.1	745	69.3	Little Cloudy	NA	NA	NA	240	NA	NA	NA	NA
	DUP-081010	8/10/2010	10:45	35	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-25-045	8/10/2010	11:50	45	137	1.13	6.56	12.86	622	-74.4	Little Cloudy	NA	NA	NA	160	NA	NA	NA	NA
	DUP2-081010	8/10/2010	11:50	45	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
GP-10-26	GP-10-26-011	8/11/2010	9:20	11	9.11	6.78	5.59	14.08	123	139.4	Clear	NA	NA	NA	13	NA	NA	NA	NA
	GP-10-26-021	8/11/2010	10:20	21	33.7	3.01	6.05	12.5	275	84.4	Clear	NA	NA	NA	22	NA	NA	NA	NA
	DUP-081110	8/11/2010	10:20	21	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-26-031	8/11/2010	10:35	31	84.8	2.67	6.04	11.74	652	84.5	Clear	NA	NA	NA	56	NA	NA	NA	NA
	GP-10-26-041	8/11/2010	11:05	41	207	0.72	6.05	12.11	631	61.5	Little Cloudy	NA	NA	NA	320	NA	NA	NA	NA
	GP-10-26-051	8/11/2010	12:15	51	76.1	1.02	6.27	12.65	485	36.3	Clear	NA	NA	NA	120	NA	NA	NA	NA
	GP-10-26-061	8/11/2010	13:40	61	376	1.49	6.45	12.74	741	-6.8	Little Cloudy	NA	NA	NA	2300	NA	NA	NA	NA
	GP-10-26-071	8/11/2010	14:10	71	<1000	0.95	6.58	13.96	860	-36.1	Cloudy	NA	NA	NA	160	NA	NA	NA	NA
GP-10-27	GP-10-27-025	8/11/2010	16:05	25	21.6	1.33	6.46	14.8	332	47.7	Clear	NA	NA	NA	40	NA	NA	NA	NA
	DUP2-081110	8/11/2010	16:05	25	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-27-035	8/11/2010	17:00	35	101.1	1.07	5.87	13.44	1022	76.8	Clear	NA	NA	NA	470	NA	NA	NA	NA
	GP-10-27-045	8/11/2010	17:25	45	339	0.71	6.58	13.58	647	-93.6	Cloudy	NA	NA	NA	620	NA	NA	NA	NA
	GP-10-27-055	8/11/2010	17:50	55	294	0.95	6.65	13.28	644	-108.8	Little Cloudy	NA	NA	NA	2300	NA	NA	NA	NA
	GP-10-27-065	8/11/2010	18:45	65	<1000	1.1	6.66	13.37	766	-93.3		NA	NA	NA	980	NA	NA	NA	NA

Notes

NA - Not Applicable  
 ug/l, is micrograms per liter

mg/l - milligrams per liter  
 I means estimated results

B indicates that analyte was detected in the associated method blank

TDS - Total Dissolved Solids  
 TSS - Total Suspended Solids

DO - Dissolved Oxygen  
 ORP - Oxygen Reduction Potential



**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Sulfide mg/l	Sulfate mg/l	COD mg/l	TOC mg/l	DOC mg/l	DIC mg/l	Notes
GP-10-11	GP-10-11-039	8/3/2010	14:10	39	<0.10	6.5	<7	NA	3.6	63	
	GP-10-11-049	8/3/2010	15:15	49	<0.1	19	160	NA	2.8	52	
	DUP3-080310	8/3/2010	15:15	49	NA	NA	NA	NA	NA	NA	
	GP-10-11-059	8/3/2010	19:00	55	<0.10	49	180	NA	3.1	37	
	GP-10-11-064	8/4/2010	11:30	64	<0.10	32	160	NA	2.8	44	
GP-10-12	GP-10-12-044	8/5/2010	13:05	44	<0.10	1.6	13 J	NA	4.1	72	
	GP-10-12-054	8/5/2010	15:00	54	<0.10	3.1	7.0	NA	4.7	66	
	GP-10-12-065	8/9/2010	8:20	65	<0.10	9.2	38	NA	7.1	56	
GP-10-13	GP-10-13-039	8/9/2010	14:45	39	<0.10	<0.12	40	NA	6.8	160	
	GP-10-13-049	8/9/2010	17:00	49	<0.1	0.58 J	36	NA	7.7	170	
	GP-10-13-059	8/10/2010	9:05	59	<0.1	<0.12	38	NA	7.8	130	
	GP-10-13-069	8/10/2010	11:15	69	<0.1	0.56 J	47	NA	5.2	100	
	GP-10-13-079	8/10/2010	13:10	79	<0.1	8.7	13 J	NA	1.7	20	
GP-10-14	GP-10-14-039	8/16/2010	09:50	39	<0.10	<0.12	26	NA	6.1	78	
	GP-10-14-049	8/16/2010	11:20	49	<0.10	0.51 J	38	NA	6	77	
	DUP-081610	8/16/2010	11:20	49	NA	NA	NA	NA	NA	NA	
	GP-10-14-059	8/16/2010	13:00	59	<0.10	2	43	NA	4.7	82	
	GP-10-14-069	8/16/2010	14:35	69	<0.10	1.4	41	NA	3.9	76	
	GP-10-14-079	8/17/2010	07:45	79	<0.10	3.8	33	NA	4.2	53	
GP-10-15	GP-10-15-039	8/11/2010	9:30	39	<0.10	0.58 J	25	NA	4.9	150	
	GP-10-15-049	8/11/2010	11:25	49	<0.1	4.2	40	NA	3	64	
	GP-10-15-059	8/11/2010	14:15	59	<0.10	15	22	NA	1	20	
GP-10-16	GP-10-16-024	8/17/2010	16:15	24	<0.10	8.8	9.7 J	NA	<1.0	12	
	DUP-081710	8/17/2010	16:15	24	NA	NA	NA	NA	NA	NA	
	GP-10-16-034	8/18/2010	07:55	34	<0.10	11	19 J	NA	4.2	12	
	GP-10-16-054	8/18/2010	11:20	54	<0.10	12	22	NA	2.1	14	
	DUP-081810	8/18/2010	11:20	54	NA	NA	NA	NA	NA	NA	
	GP-10-16-064	8/18/2010	13:40	64	<0.01	7.3	24	NA	3.7	46	
	GP-10-16-074	8/19/2010	07:45	74	<0.1	9.7	790	NA	15	47	
	GP-10-16-084	8/19/2010	09:40	84	<0.1	0.59 J	43	NA	5.6	86	
	DUP-081910	8/19/2010	09:40	84	NA	NA	NA	NA	NA	NA	
GP-10-17	GP-10-17-009	8/2/2010	11:40	9	NA	NA	NA	NA	2.8	13	
	GP-10-17-019	8/2/2010	12:20	19	NA	NA	NA	NA	1.2	14	
	DUP-080210	8/2/2010	12:20	19	NA	NA	NA	NA	1.2	13	
	GP-10-17-029	8/2/2010	16:00	29	NA	NA	NA	NA	1.1	12	
	GP-10-17-039	8/2/2010	16:45	39	NA	NA	NA	NA	4.1	72	
	GP-10-17-049	8/2/2010	17:30	49	NA	NA	NA	NA	3.6	72	
	GP-10-17-056	8/2/2010	17:45	56	NA	NA	NA	NA	3.7	77	
GP-10-18	GP-10-18-007	8/2/2010	18:34	7	NA	NA	NA	NA	1.4	24	
	GP-10-18-017	8/3/2010	8:25	17	NA	NA	NA	NA	1.6	32	
	GP-10-18-027	8/3/2010	9:00	27	NA	NA	NA	NA	3.6	76	
	DUP-080310	8/3/2010	9:00	27	NA	NA	NA	NA			
	GP-10-18-037	8/3/2010	11:00	37	NA	NA	NA	NA	5	57	
	GP-10-18-047	8/3/2010	12:10	47	NA	NA	NA	NA	6.6	98	
GP-10-19	GP-10-19-009	8/3/2010	14:35	9	NA	NA	NA	NA	1.1	6.4	
	DUP2-080310	8/3/2010	14:35	9	NA	NA	NA	NA	NA	NA	
	GP-10-19-019	8/3/2010	15:15	19	NA	NA	NA	NA	1	26	
	GP-10-19-029	8/3/2010	16:05	29	NA	NA	NA	NA	4.7	62	
	GP-10-19-039	8/3/2010	17:00	39	NA	NA	NA	NA	5.1	71	
	GP-10-19-046	8/3/2010	18:15	46	NA	NA	NA	NA	4.9	85	

**TABLE 2**  
**Groundwater Profile Results**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Sulfide mg/l	Sulfate mg/l	COD mg/l	TOC mg/l	DOC mg/l	DIC mg/l	Notes
GP-10-20	GP-10-20-009	8/4/2010	9:30	9	NA	NA	NA	NA	1.2	9.8	
	GP-10-20-019	8/4/2010	10:10	19	NA	NA	NA	NA	1.6	37	
	DUP-080410	8/4/2010	10:10	19	NA	NA	NA	NA	NA	NA	
	GP-10-20-029	8/4/2010	11:00	29	NA	NA	NA	NA	4.2	61	
	GP-10-20-039	8/4/2010	13:00	39	NA	NA	NA	NA	4.9	82	
GP-10-21	GP-10-21-011	8/4/2010	15:05	11	NA	NA	NA	NA	< 1	9.1	
	GP-10-21-021	8/4/2010	15:45	21	NA	NA	NA	NA	1.2	27	
	DUP2-080410	8/4/2010	15:45	21	NA	NA	NA	NA	NA	NA	
	GP-10-21-031	8/4/2010	16:30	31	NA	NA	NA	NA	3.9	65	
	GP-10-21-041	8/4/2010	17:00	41	NA	NA	NA	NA	5.2	79	
	GP-10-21-051	8/4/2010	18:05	51	NA	NA	NA	NA	4.7	100	
	GP-10-21-060	8/4/2010	19:00	60	NA	NA	NA	NA	4.4	84	
GP-10-22	GP-10-22-011	8/10/2010	14:40	11	NA	NA	NA	NA	1.4	15	
	GP-10-22-021	8/10/2010	15:00	21	NA	NA	NA	NA	2.4	24	
	GP-10-22-031	8/10/2010	15:50	31	NA	NA	NA	NA	1.5	26	
	GP-10-22-041	8/10/2010	16:30	41	NA	NA	NA	NA	2.8	36	
	GP-10-22-051	8/10/2010	17:30	51	NA	NA	NA	NA	3	68	
	GP-10-22-061	8/10/2010	18:30	61	NA	NA	NA	NA	2.3	63	
GP-10-23	GP-10-23-017	8/5/2010	11:00	17	NA	NA	NA	NA	1.9	22	
	DUP-080510	8/5/2010	11:00	17	NA	NA	NA	NA	NA	NA	
	GP-10-23-027	8/5/2010	11:45	27	NA	NA	NA	NA	2.1	20	
	GP-10-23-037	8/5/2010	12:25	37	NA	NA	NA	NA	1.1	26	
	GP-10-23-047	8/5/2010	14:20	47	NA	NA	NA	NA	4.1	52	
	GP-10-23-057	8/5/2010	16:05	57	NA	NA	NA	NA	6	87	
	DUP2-080510	8/5/2010	16:05	57	NA	NA	NA	NA	NA	NA	
GP-10-24	GP-10-24-015	8/9/2010	15:44	15	NA	NA	NA	NA	<1.0	20	
	DUP-080910	8/9/2010	15:44	15	NA	NA	NA	NA	NA	NA	
	GP-10-24-025	8/9/2010	16:30	25	NA	NA	NA	NA	< 1	15	
	GP-10-24-035	8/9/2010	17:05	35	NA	NA	NA	NA	1.5	37	
	GP-10-24-045	8/9/2010	17:45	45	NA	NA	NA	NA	4.4	60	
	GP-10-24-055	8/9/2010	18:30	55	NA	NA	NA	NA	5.9	96	
GP-10-25	GP-10-25-025	8/10/2010	10:00	25	NA	NA	NA	NA	1.4	13	
	GP-10-25-035	8/10/2010	10:45	35	NA	NA	NA	NA	1.6	43	
	DUP-081010	8/10/2010	10:45	35	NA	NA	NA	NA	NA	NA	
	GP-10-25-045	8/10/2010	11:50	45	NA	NA	NA	NA	3.6	61	
	DUP2-081010	8/10/2010	11:50	45	NA	NA	NA	NA	NA	NA	
GP-10-26	GP-10-26-011	8/11/2010	9:20	11	NA	NA	NA	NA	< 1	14	
	GP-10-26-021	8/11/2010	10:20	21	NA	NA	NA	NA	< 1	17	
	DUP-081110	8/11/2010	10:20	21	NA	NA	NA	NA	NA	NA	
	GP-10-26-031	8/11/2010	10:35	31	NA	NA	NA	NA	< 1	22	
	GP-10-26-041	8/11/2010	11:05	41	NA	NA	NA	NA	1.7	26	
	GP-10-26-051	8/11/2010	12:15	51	NA	NA	NA	NA	2.4	48	
	GP-10-26-061	8/11/2010	13:40	61	NA	NA	NA	NA	4.5	98	
	GP-10-26-071	8/11/2010	14:10	71	NA	NA	NA	NA	3.9	110	
GP-10-27	GP-10-27-025	8/11/2010	16:05	25	NA	NA	NA	NA	< 1	12	
	DUP2-081110	8/11/2010	16:05	25	NA	NA	NA	NA	NA	NA	
	GP-10-27-035	8/11/2010	17:00	35	NA	NA	NA	NA	1.3	25	
	GP-10-27-045	8/11/2010	17:25	45	NA	NA	NA	NA	4.4	64	
	GP-10-27-055	8/11/2010	17:50	55	NA	NA	NA	NA	4.5	60	
	GP-10-27-065	8/11/2010	18:45	65	NA	NA	NA	NA	5.7	71	

Notes

NA - Not Applicable  
 ug/l. is micrograms per liter

mg/l - milligrams per liter  
 J means estimated results

COD - Chemical Oxygen Demand  
 TOC - Total Organic Carbon

DOC - Dissolved Organic Carbon  
 DIC - Dissolved Inorganic Carbon



**TABLE 3**  
**GROUNDWATER MONITORING WELL RESULTS**  
**Sheple'y Hill Landfill, Devens Massachusetts**

Boring Location	Sample ID	Date	Aluminum		Antimony		Arsenic		Barium		Beryllium		Cadmium		Calcium	
			Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
SHM-10-01	SHM-10-01-071310	7/13/2010	76.2	< 7.64	NA	NA	1.16 J	0.68 J	NA	NA	NA	NA	NA	NA	42400	42700
	SHM-10-01	8/12/2010	NA	< 19.1	NA	NA	NA	3.51 J	NA	NA	NA	NA	NA	NA	NA	41600
	SHM-10-01-090810	9/8/2010	33.3 J	< 19.1	NA	NA	8.15	7.87	NA	NA	NA	NA	NA	NA	43100	43500
SHM-10-02	SHM-10-02-071510	7/15/2010	236	2.09 J	NA	NA	0.74	0.43 J	NA	NA	NA	NA	NA	NA	113000	117000
	DUP-071510	7/15/2010	189	2.02 J	NA	NA	0.59	0.45 J	NA	NA	NA	NA	NA	NA	114000	117000
	SHM10-02-090710	9/7/2010	85.3	4.15 J	NA	NA	1.11	1.07	NA	NA	NA	NA	NA	NA	115000 J	114000 J
SHM-10-03	SHM-10-03-071410	7/14/2010	388	< 7.64	NA	NA	2.36	0.78 J	NA	NA	NA	NA	NA	NA	112000	109000
	DUP-071410	7/14/2010	810	< 7.64	NA	NA	4.59	0.5 J	NA	NA	NA	NA	NA	NA	112000	111000
	SHM-10-03-090710	9/7/2010	168	< 7.64	NA	NA	1.47 J	0.51 J	NA	NA	NA	NA	NA	NA	153000	157000
	DUP-090710	9/7/2010	208	< 7.64	NA	NA	1.51 J	0.71 J	NA	NA	NA	NA	NA	NA	149000	154000
SHM-10-04	SHM-10-04-071410	7/14/2010	473	3.21 J	NA	NA	1.62	0.64	NA	NA	NA	NA	NA	NA	60300 J	57800
	SHM-10-04-090710	9/7/2010	87.2	< 7.64	NA	NA	1 J	0.79 J	NA	NA	NA	NA	NA	NA	72100	72800
SHM-10-05A	SHM-10-05A-071510	7/15/2010	35	2.83 J	NA	NA	4.7	4.6	NA	NA	NA	NA	NA	NA	14200	14500
	SHM-10-05A-090810	9/8/2010	43.2	3.8 J	NA	NA	5.68	5.21	NA	NA	NA	NA	NA	NA	14100	14200
SHM-10-06	SHM-10-06-070810	7/8/2010	1150	3.44 J	NA	NA	2210 J	1680 J	NA	NA	NA	NA	NA	NA	40900	41000 J
	DUP-070810	7/8/2010	1270	2.13 J	NA	NA	2520	1520	NA	NA	NA	NA	NA	NA	46500	41100
	SHM-10-06-090810	9/8/2010	< 19.1	< 19.1	NA	NA	2580	2710	NA	NA	NA	NA	NA	NA	48200	50300
SHM-10-06A	SHM-10-06A-070710	7/7/2010	38.7 J	12.2	NA	NA	64.8	61	NA	NA	NA	NA	NA	NA	15700	15300 J
	DUP-070710	7/7/2010	27.7	12.4	NA	NA	65.1	60.1	NA	NA	NA	NA	NA	NA	15800	15500
	SHM-10-06A-090910	9/9/2010	1910	11.6 J	NA	NA	102	94.2	NA	NA	NA	NA	NA	NA	33000	33300
	DUP-090910	9/9/2010	1990	8.97 J	NA	NA	102	83	NA	NA	NA	NA	NA	NA	31800	25300
SHM-10-07	SHM-10-07-052710	5/27/2010	3870	< 19.1	NA	NA	816 J	818 J	NA	NA	NA	NA	NA	NA	62200 J	60600 J
	DUP-052710	5/27/2010	3640	< 19.1	NA	NA	827	825	NA	NA	NA	NA	NA	NA	62600	61100
	SHM-10-07-090910	9/9/2010	538	4.17 J	NA	NA	979	918	NA	NA	NA	NA	NA	NA	47400	43200
SHM-10-08	SHM-10-08-071510	7/15/2010	591	< 3.82	NA	NA	2.72	0.73 J	NA	NA	NA	NA	NA	NA	160000	152000
	SHM-10-08-090710	9/7/2010	33.2	< 3.82	NA	NA	1.4	1.55	NA	NA	NA	NA	NA	NA	182000	195000
SHM-10-10	SHM-10-10-071310	7/13/2010	88 J	< 19.1	NA	NA	2 J	1.25 J	NA	NA	NA	NA	NA	NA	95100	92800
	DUP-071310	7/13/2010	79 J	< 19.1	NA	NA	1.34 J	1.13 J	NA	NA	NA	NA	NA	NA	92400	94600
	SHM-10-10	8/12/2010		< 19.1	NA	NA		3.62 J	NA	NA	NA	NA	NA	NA		83800
	SHM-10-10-090810	9/8/2010	27.6 J	< 19.1	NA	NA	2.57 J	2.4 J	NA	NA	NA	NA	NA	NA	107000	96800
	DUP-090810	9/8/2010	86.6 J	< 19.1	NA	NA	2.58 J	6.66	NA	NA	NA	NA	NA	NA	96300	101000



**TABLE 3**  
**GROUNDWATER MONITORING WELL RESULTS**  
**Shepley Hill Landfill, Devens Massachusetts**

Boring Location	Sample ID	Date	Aluminum		Antimony		Arsenic		Barium		Beryllium		Cadmium		Calcium	
			Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
SHM-10-11	SHM-10-11	8/30/2010	113	10.2 J	0.26 J	0.53 J	356	342 J	40.3	36.5	<0.118	<0.118	<0.118	<0.118	23900	21200 J
	SHM-10-11-101910	10/19/2010	111	< 7.64	0.68 J	0.78 J	470	463	43.2	42.6	< 0.236	< 0.236	< 0.236	< 0.236	21900	22200
SHM-10-12	SHM-10-12	8/30/2010	50.2 J	27.6 J	1.38 J	2.99 J	2880	3560	44.1	55.7	<0.590	<0.590	<0.590	<0.590	25000	33000
	DUP-083010	8/30/2010	112	27.5 J	<1.20	1.56 J	3210	3410	50.6	53.7	<0.590	<0.590	<0.590	<0.590	27900	30600
	SHM-10-12-102010	10/20/2010	10.8 J	57.4	< 0.6	0.6	2980	3120	42.4	42.6	< 0.295	< 0.295	< 0.295	< 0.295	29000	29000
	DUP-102010	10/20/2010	50.2	< 9.56	< 0.600	< 0.600	3160	3000	42.8	41.9	< 0.295	< 0.295	< 0.295	< 0.295	29200	28300
SHM-10-13	GP-10-13-090110	9/1/2010	233	6.02 J	0.19 J	0.17 J	619 J	575	160	153	<0.059	<0.059	<0.059	<0.059	68000	61400
	SHM-10-13-101910	10/19/2010	305	< 7.64	< 0.48	< 0.48	700	672	154	154	< 0.236	< 0.236	< 0.236	< 0.236	67200	65000
	DUP-101910	10/19/2010	343	< 7.64	0.480	0.48 J	648	674	138	154	< 0.236	< 0.236	< 0.236	< 0.236	60300	64200
SHM-10-14	SHM-10-14-090210	9/2/2010	262	< 19.1	< 1.2	< 1.2	4280	4100	80.5	53.8	< 0.59	< 0.059	< 0.59	< 0.059	69300	55300
	SHM-10-14-101910	10/19/10	811	< 9.56	0.67 J	< 0.600	5990 J	5860	87.5	43.4	< 0.295	< 0.295	< 0.295	< 0.295	70800	57900
SHM-10-15	GP-10-15-090110	9/1/2010	125	<19.1	1.93 J	1.87 J	7930	8110	55	52.4	<0.590	<0.590	<0.590	<0.590	61300	61500
	SHM-10-15-090110		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	DUP-090110	9/1/2010	284	<19.1	<1.20	1.25 J	7610	6460	50.7	39.1	<0.590	<0.590	<0.590	<0.590	58500	46800
	SHM-10-15-102010	10/20/2010	312	< 19.1	< 1.20	< 1.20	6090	6230	42.4	43	< 0.59	< 0.59	< 0.59	< 0.59	51200	51800
SHM-10-16	SHM-10-16-090210	9/2/2010	1180	3.59 J	0.37 J	0.24 J	487	495	72.8	73.4	0.07 J	< 0.059	< 0.059	< 0.059	69700	73900
	DUP-090210	9/2/2010	1360	3.27 J	0.32 J	0.17 J	542	489	82.1	69.4	0.07 J	0.059	0.059	0.059	68800	70700
	SHM-10-16-102010	10/20/2010	487	2.53 J	< 0.120	0.16 J	1180	1090	59.2	51.6	< 0.059	0.06 J	< 0.059	0.06 J	73200	68100
SHM-23	SHM-23	8/12/2010	NA	20.8	NA	NA	NA	0.14 J	NA	NA	NA	NA	NA	NA	NA	2230
SHM-05-39A	SHM-05-39A	8/12/2010	NA	3.57 J	NA	NA	NA	236	NA	NA	NA	NA	NA	NA	NA	16600
SHM-07-03	SHM-07-03	8/12/2010	NA	11	NA	NA	NA	0.29 J	NA	NA	NA	NA	NA	NA	NA	6580
	DUP2-081210	8/12/2010	NA	9.63 J	NA	NA	NA	0.77	NA	NA	NA	NA	NA	NA	NA	6860
SHM-07-05	SHM-07-05	8/12/2010	NA	<9.56	NA	NA	NA	3180	NA	NA	NA	NA	NA	NA	NA	21500
	DUP-081210	8/12/2010	NA	< 9.56	NA	NA	NA	3220	NA	NA	NA	NA	NA	NA	NA	21700
SHM-99-31B	SHM-99-31B	8/12/2010	NA	35.8	NA	NA	NA	28.8	NA	NA	NA	NA	NA	NA	NA	16500
SHM-05-041B	SHM-05-041B	8/9/2010	147	2.59 J	NA	NA	1440	1130	NA	NA	NA	NA	NA	NA	16000	14500 J
SHM-05-42A	SHM-05-42A	8/12/2010	NA	6.06 J	NA	NA	NA	1.25	NA	NA	NA	NA	NA	NA	NA	6700
SHP-05-045A	SHP-05-045A	8/9/2010	NA	NA	NA	NA	36.4	33.7	NA	NA	NA	NA	NA	NA	NA	NA
SHP-05-046B	SHP-05-046B	8/9/2010	NA	NA	NA	NA	50.6	81.4	NA	NA	NA	NA	NA	NA	NA	NA

Notes: NA - Not Applicable  
ug/L is micrograms per liter  
mg/L - milligrams per liter  
J means estimated results  
B indicates that analyte was detected in the associated method blank



**TABLE 3**  
**GROUNDWATER MONITORING WELL RESULTS**  
**Shepley Hill Landfill, Devens Massachusetts**

Boring Location	Sample ID	Date	Chromium		Cobalt		Copper		Iron		Lead		Magnesium		Manganese	
			Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
SHM-10-01	SHM-10-01-071310	7/13/2010	< 0.744	< 0.744	NA	NA	NA	NA	508	373	0.2 J	< 0.2	3700	3680	10500 J	10600
	SHM-10-01	8/12/2010	NA	< 1.86	NA	NA	NA	NA	NA	886	NA	< 0.500	NA	3530	NA	10700
	SHM-10-01-090810	9/8/2010	< 1.86	< 1.86	NA	NA	NA	NA	1740	1680	< 0.500	< 0.500	3680	3780	10200	10300
SHM-10-02	SHM-10-02-071510	7/15/2010	1.54	0.31 J	NA	NA	NA	NA	1190	881	0.42 J	0.05 J	15700	16100	2110	2180
	Dup-071510	7/15/2010	1.28	0.32 J	NA	NA	NA	NA	1170	890	0.35 J	0.05 J	15600	16100	2130	2170
	SHM10-02-090710	9/7/2010	0.68 J	< 0.372	NA	NA	NA	NA	973	843	0.18 J	< 0.1	16000	16000	2190	2190
SHM-10-03	SHM-10-03-071410	7/14/2010	2.97	< 0.744	NA	NA	NA	NA	1630	866	3.43	1.12 J	12900	12600	122	153
	DUP-071410	7/14/2010	4.68	< 0.744	NA	NA	NA	NA	2440	843	4.04	2.08	13000	127000	151	134
	SHM-10-03-090710	9/7/2010	2.01	< 0.744	NA	NA	NA	NA	1420	1030	0.49 J	< 0.200	18200	18500	72.8	44
	DUP-090710	9/7/2010	1.99 J	< 0.744	NA	NA	NA	NA	1480	1040	0.58 J	< 0.200	17700	18000	70.2	51.7
SHM-10-04	SHM-10-04-071410	7/14/2010	4.77	0.49 J	NA	NA	NA	NA	3800 J	5190	0.59	< 0.05	12300 J	11800	2190	2500
	SHM-10-04-090710	9/7/2010	0.95 J	< 0.744	NA	NA	NA	NA	1880	1650	0.2 J	< 0.200	14500	14600	3210	3100
SHM-10-05A	SHM-10-05A-071510	7/15/2010	0.38 J	0.24 J	NA	NA	NA	NA	1970	1880	0.07 J	< 0.05	1660	1670	590	620
	SHM-10-05A-090810	9/8/2010	0.59	< 0.186	NA	NA	NA	NA	790	677	0.14 J	0.09 J	1600	1600	105	122
SHM-10-06	SHM-10-06-070810	7/8/2010	4.65	0.21	NA	NA	NA	NA	130000 J	117000	1.76 J	< 0.05	7360	7140	724	699
	DUP-070810	7/8/2010	5.33	0.25 J	NA	NA	NA	NA	149000	117000	3.34	< 0.05	8400	7200	829	712
	SHM-10-06-090810	9/8/2010	1.86	1.86	NA	NA	NA	NA	144000	145000	0.500	0.37 J	8270	8800	9.54	9.63
SHM-10-06A	SHM-10-06A-070710	7/7/2010	0.58	0.31 J	NA	NA	NA	NA	20900 J	19900 J	0.22 J	0.06 J	2090	2030	1650 J	1620
	DUP-070710	7/7/2010	0.59	0.38 J	NA	NA	NA	NA	21200	20200	0.13 J	0.07 J	2080	2070	1660	1650
	SHM-10-06A-090910	9/9/2010	6.92	< 0.744	NA	NA	NA	NA	44600	42900	2.7	< 0.200	4940	4640	3940	4080
	DUP-090910	9/9/2010	7.16	< 0.744	NA	NA	NA	NA	42700	32300	2.69	< 0.200	4810	3280	3820	3130
SHM-10-07	SHM-10-07-052710	5/27/2010	15.8	< 1.86	NA	NA	NA	NA	75800 J	70600 J	4.72	0.74 J	12200	9590	3230 J	3110 J
	DUP-052710	5/27/2010	15.9	< 1.86	NA	NA	NA	NA	75800	71800	4.62	< 0.5	12100	9660	3280	3130
	SHM-10-07-090910	9/9/2010	2.82	< 0.372	NA	NA	NA	NA	62300	56800	0.95 J	< 0.100	6360	5610	2050	1940
SHM-10-08	SHM-10-08-071510	7/15/2010	4.56	< 0.372	NA	NA	NA	NA	2610	1310 J	0.8 J	0.18 J	21100	19900 J	910	885 J
	SHM-10-08-090710	9/7/2010	0.43 J	< 0.372	NA	NA	NA	NA	1270	1260	< 0.100	< 0.100	23600	25000	359	376
SHM-10-10	SHM-10-10-071310	7/13/2010	< 1.86	< 1.86	NA	NA	NA	NA	1020	799	< 0.5	< 0.5	12100	11900	24600	24200
	DUP-071310	7/13/2010	< 1.86	< 1.86	NA	NA	NA	NA	925	804	< 0.5	< 0.5	11800	12100	24100	24800
	SHM-10-10	8/12/2010	NA	< 1.86	NA	NA	NA	NA	NA	1180	NA	< 0.500	NA	10700	NA	22000
	SHM-10-10-090810	9/8/2010	< 1.86	< 1.86	NA	NA	NA	NA	833	700	1.6 J	< 0.500	13200	12000	27400	25200
	DUP-090810	9/8/2010	< 1.86	< 1.86	NA	NA	NA	NA	825	929	< 0.500	< 0.500	11900	12600	27400	25800

TABLE 3  
GROUNDWATER MONITORING WELL RESULTS  
Shepley Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Chromium		Cobalt		Copper		Iron		Lead		Magnesium		Manganese	
			Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
SHM-10-11	SHM-10-11	8/30/2010	1.44	0.52 J	6.28	5.94	0.75 J	0.45 J	60600	55700	0.34 J	0.15 J	2770	2530	2490	2320
	SHM-10-11-101910	10/19/2010	1.15 J	< 0.744	11	10.9	0.64 J	< 0.472	60500	61000	0.36 J	0.2 J	2840	2900	2160	2260
SHM-10-12	SHM-10-12	8/30/2010	<1.86	<1.86	6.36	8.34	<1.18	<1.18	78600	104000	<0.500	<0.500	1940	2500	5400	7000
	DUP-083010	8/30/2010	<1.86	<1.86	6.88	7.64	<1.18	<1.18	89700	96000	0.59 J	<0.500	2190	2360	6120	6520
	SHM-10-12-102010	10/20/2010	<0.93	1.19 J	7.08	7.38	<0.59	0.73 J	88700	90000	<0.25	0.79 J	2180	2200	6070	6200
	DUP-102010	10/20/2010	0.97 J	<0.93	7.33	6.98	0.62 J	<0.59	90900	87400	0.7 J	0.27 J	2240	2120	6320	6030
SHM-10-13	GP-10-13-090110	9/1/2010	2.66	0.73	0.84	0.73	0.74	0.34 J	88600	84100	0.13 J	<0.05	10500	9900	1900	1850 J
	SHM-10-13-101910	10/19/2010	4.17	<0.744	0.87 J	0.75 J	1.17 J	<0.472	95500	94600	0.42 J	0.32 J	9840	10100	2100	2060
	DUP-101910	10/19/2010	4.15	<0.744	0.89 J	0.74 J	1.27 J	2.06	87500	94700	0.44 J	<0.200	8720	9920	1960	2090
SHM-10-14	SHM-10-14-090210	9/2/2010	<1.86	<1.86	16	15.6	1.53 J	1.3 J	75200	73000	0.76 J	<0.5	4310	4150	4700	4720
	SHM-10-14-101910	10/19/10	3.25	<0.930	23.8	20	4.67	<0.590	98300	92700	2.27 J	<0.250	3980	3720	4350 J	4180
SHM-10-15	GP-10-15-090110	9/1/2010	<1.86	<1.86	28.6	29.3	<1.18	<1.18	62500	63300	0.79 J	<0.500	7700	7880	10400	10700
	SHM-10-15-090110		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
	DUP-090110	9/1/2010	<1.86	<1.86	27	22.4	1.37 J	<1.18	58700	48900	1.09 J	<0.500	7470	6050	9900	8240
	SHM-10-15-102010	10/20/2010	<1.86	<1.86	22.3	23.3	1.2 J	<1.18	50400	52000	1.48 J	0.7 J	6440	6530	8440	8680
SHM-10-16	SHM-10-16-090210	9/2/2010	7.12	0.32 J	5.27	4.97	5.87	0.36 J	50200	53100	1.65	<0.05	13800	14100	1710	1790
	DUP-090210	9/2/2010	8.28	0.3 J	5.81	4.85	6.88	0.34 J	55100	51100	1.97	0.05	15000	13500	1800	1680
	SHM-10-16-102010	10/20/2010	3.5	0.28 J	6.56	5.51	2.73	0.54	51800	46900	0.91	0.08 J	13100	12000	1250	1150
SHL-23	SHL-23	8/12/2010	NA	<0.186	NA	NA	NA	NA	NA	16.9 J	NA	<0.050	NA	163	NA	6.87
SHM-05-39A	SHM-05-39A	8/12/2010	NA	<0.186	NA	NA	NA	NA	NA	24500	NA	<0.050	NA	1860	NA	680
SHM-07-03	SHM-07-03	8/12/2010	NA	<0.186	NA	NA	NA	NA	NA	53.8	NA	0.05 J	NA	550	NA	9.68
	DUP2-081210	8/12/2010	NA	<0.186	NA	NA	NA	NA	NA	58	NA	0.05 J	NA	568	NA	9.66
SHM-07-05	SHM-07-05	8/12/2010	NA	<0.930	NA	NA	NA	NA	NA	22500	NA	<0.250	NA	2990	NA	544
	DUP-081210	8/12/2010	NA	<0.930	NA	NA	NA	NA	NA	22700	NA	<0.250	NA	2960	NA	545
SHM-99-31B	SHM-99-31B	8/12/2010	NA	0.56	NA	NA	NA	NA	NA	14600	NA	0.09 J	NA	1930	NA	478
SHM-05-041B	SHM-05-041B	8/9/2010	0.5	<0.186	NA	NA	NA	NA	35200	28000	0.6	<0.050	2400	2080	736	656 J
SHM-05-42A	SHM-05-42A	8/12/2010	NA	<0.186	NA	NA	NA	NA	NA	388	NA	<0.050	NA	1160	NA	140
SHP-05-045A	SHP-05-045A	8/9/2010	NA	NA	NA	NA	NA	NA	21600	22100	NA	NA	NA	NA	NA	NA
SHP-05-046B	SHP-05-046B	8/9/2010	NA	NA	NA	NA	NA	NA	26800	34800	NA	NA	NA	NA	NA	NA

Notes  
NA - Not Applicable  
ug/L is micrograms per liter  
mg/l - milligrams per liter  
J means estimated results  
B indicates that analyte was detected in the a



**TABLE 3**  
**GROUNDWATER MONITORING WELL RESULTS**  
**Shepley Hill Landfill, Devens Massachusetts**

Boring Location	Sample ID	Date	Mercury		Nickel		Potassium		Selenium		Silver		Sodium		Thallium	
			Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
SHM-10-01	SHM-10-01-071310	7/13/2010	NA	NA	6.07	5.77	2300	2290	NA	NA	NA	NA	9340	9160	NA	NA
	SHM-10-01	8/12/2010	NA	NA	NA	5.75	NA	2230	NA	NA	NA	NA	NA	11100	NA	NA
	SHM-10-01-090810	9/8/2010	NA	NA	4.09 J	4.31 J	2220	2280	NA	NA	NA	NA	8880	8770	NA	NA
SHM-10-02	SHM-10-02-071510	7/15/2010	NA	NA	9.98	9.79	3880	4010	NA	NA	NA	NA	49500	53300	NA	NA
	DUP-071510	7/15/2010	NA	NA	10.2	9.71	3980	4000	NA	NA	NA	NA	51400	53100	NA	NA
	SHM-10-02-090710	9/7/2010	NA	NA	9.58	9.3	4020	4040	NA	NA	NA	NA	48100	50700	NA	NA
SHM-10-03	SHM-10-03-071410	7/14/2010	NA	NA	6.24	5.36	6490	6000	NA	NA	NA	NA	474000	473000	NA	NA
	DUP-071410	7/14/2010	NA	NA	7.44	5.18	6580	6060	NA	NA	NA	NA	483000	474000	NA	NA
	SHM-10-03-090710	9/7/2010	NA	NA	6.6	5.67	6920	6880	NA	NA	NA	NA	536000	536000	NA	NA
	DUP-090710	9/7/2010	NA	NA	6.35	5.68	6670	6840	NA	NA	NA	NA	510000	526000	NA	NA
SHM-10-04	SHM-10-04-071410	7/14/2010	NA	NA	9.98	11.6	4230	5220	NA	NA	NA	NA	33400 J	35400	NA	NA
	SHM-10-04-090710	9/7/2010	NA	NA	8.1	7.66	4050	3990	NA	NA	NA	NA	35800	35200	NA	NA
SHM-10-05A	SHM-10-05A-071510	7/15/2010	NA	NA	4.02	4.43	1990	1990	NA	NA	NA	NA	22800	23900	NA	NA
	SHM-10-05A-090810	9/8/2010	NA	NA	1.68	1.72	1770	1830	NA	NA	NA	NA	19600	19700	NA	NA
SHM-10-06	SHM-10-06-070810	7/8/2010	NA	NA	11.6	8.11	11700	11800	NA	NA	NA	NA	18200	17900	NA	NA
	DUP-070810	7/8/2010	NA	NA	12.6	8.27	13100	12300	NA	NA	NA	NA	20700	19000	NA	NA
	SHM-10-06-090810	9/8/2010	NA	NA	9.11	9.4	13500	13800	NA	NA	NA	NA	22800	23700	NA	NA
SHM-10-06A	SHM-10-06A-070710	7/7/2010	NA	NA	2.22	1.13	4700	4520	NA	NA	NA	NA	7490	7260	NA	NA
	DUP-070710	7/7/2010	NA	NA	1.16	1.12	4740	4680	NA	NA	NA	NA	7640	7560	NA	NA
	SHM-10-06A-090910	9/9/2010	NA	NA	7.73	2.34	8130	7640	NA	NA	NA	NA	13200	13200	NA	NA
	DUP-090910	9/9/2010	NA	NA	7.97	1.68 J	7970	5990	NA	NA	NA	NA	12900	9240	NA	NA
SHM-10-07	SHM-10-07-052710	5/27/2010	NA	NA	18.5	6.4	17900	16000	NA	NA	NA	NA	36400	35100 J	NA	NA
	DUP-052710	5/27/2010	NA	NA	17.5	6.3	18100	16100	NA	NA	NA	NA	36900	35700	NA	NA
	SHM-10-07-090910	9/9/2010	NA	NA	7.34	5.28	13200	11400	NA	NA	NA	NA	26400	24400	NA	NA
SHM-10-08	SHM-10-08-071510	7/15/2010	NA	NA	11.3	9.55	5370	4590	NA	NA	NA	NA	44300 J	44500	NA	NA
	SHM-10-08-090710	9/7/2010	NA	NA	8.27	8.57	5240	5470	NA	NA	NA	NA	46400	NA	NA	NA
SHM-10-10	SHM-10-10-071310	7/13/2010	NA	NA	21.5	21.2	3580	3600	NA	NA	NA	NA	26500	26100	NA	NA
	DUP-071310	7/13/2010	NA	NA	21	21.5	3490	3610	NA	NA	NA	NA	26500	27500	NA	NA
	SHM-10-10	8/12/2010	NA	NA		20.8		3590	NA	NA	NA	NA		28500	NA	NA
	SHM-10-10-090810	9/8/2010	NA	NA	23.5	21.5	3750	3410	NA	NA	NA	NA	29600	27100	NA	NA
	DUP-090810	9/8/2010	NA	NA	21.4	22.2	3380	3560	NA	NA	NA	NA	26600	28500	NA	NA

**TABLE 3**  
**GROUNDWATER MONITORING WELL RESULTS**  
Shepley Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Mercury		Nickel		Potassium		Selenium		Silver		Sodium		Thallium	
			Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)
SHM-10-11	SHM-10-11	8/30/2010	<0.0120	0.01443 J	5.92	5.43	5410	5150	<0.812	<0.812	<0.170	<0.170	12400	11800	<0.062	<0.062
	SHM-10-11-101910	10/19/2010	0.09993 J	0.1268 J	6.62	6.8	5310	5390	< 1.62	< 1.62	< 0.340	< 0.340	12700	13000	< 0.124	< 0.124
SHM-10-12	SHM-10-12	8/30/2010	<0.0120	<0.0120	11	13.9	5480	7040	<4.06	<4.06	<0.850	<0.850	7090	8780	<0.310	<0.310
	DUP-083010	8/30/2010	0.03627 J	0.01933 J	12.3	12.4	6190	6480	<4.06	<4.06	<0.850	<0.850	7880	8610	<0.310	<0.310
	SHM-10-12-102010	10/20/2010	0.06204 J	0.09511 J	11.7	12.3	4820	4900	< 2.03	< 2.03	< 0.425	< 0.425	5220	5060	< 0.155	< 0.155
	DUP-102010	10/20/2010	0.1153 J	0.0624 J	12.3	11.4	4940	4670	< 2.03	< 2.03	< 0.425	< 0.425	5210	4870	< 0.155	< 0.155
SHM-10-13	GP-10-13-090110	9/1/2010	<0.0120	<0.0120	3	2.6	12500	12200	0.54 J	<0.406	<0.085	<0.085	15300	14500	<0.031	<0.031
	SHM-10-13-101910	10/19/2010	0.07162 J	0.07162 J	2.95	2.54	12300	12500	< 1.62	< 1.62	< 0.340	< 0.340	15600	15900	< 0.124	< 0.124
	DUP-101910	10/19/2010	0.1218 J	0.1059 J	2.87	2.48	11000	12200	< 1.62	< 1.62	< 0.340	< 0.340	13900	16100	< 0.124	< 0.124
SHM-10-14	SHM-10-14-090210	9/2/2010	< 0.012	< 0.012	8.07	9.16	18800	17600 J	< 4.06	< 4.06	< 0.85	< 0.85	15500	15200	< 0.31	< 0.31
	SHM-10-14-101910	10/19/10	0.0965 J	0.1246 J	11.2	7.62	11400	101000	< 2.03	< 2.03	< 0.425	< 0.425	8500	8080	< 0.155	< 0.155
SHM-10-15	GP-10-15-090110	9/1/2010	<0.0120	<0.0120	20	20.3	6910	6880	<4.06	<4.06	<0.850	<0.850	13700	13900	<0.310	<0.310
	SHM-10-15-090110															
	DUP-090110	9/1/2010	<0.0120	<0.0120	18.5	15.3	6390	5200	<4.06	<4.06	<0.850	<0.850	13100	11200	< 0.310	<0.310
	SHM-10-15-102010	10/20/2010	0.07762 J	0.0551 J	16.2	15.8	5350	5500	<4.06	<4.06	< 0.850	< 0.850	11600	12400	< 0.310	< 0.31
SHM-10-16	SHM-10-16-090210	9/2/2010	0.102776 J	< 0.012	6.39	3.54	14600	15500	0.59 J	0.7 J	< 0.85	< 0.085	30800	31400	0.05 J	0.05 J
	DUP-090210	9/2/2010	0.01466 J	0.012	7.06	3.37	15800	14700	0.71 J	0.61 J	< 0.85	< 0.085	32400	3105	0.05 J	1.85
	SHM-10-16-102010	10/20/2010	0.09046 J	0.03837 J	5.28	3.06	12500	11800	0.43 J	0.44 J	< 0.85	< 0.085	31500	30700	< 0.031	0.06 J
SHM-23	SHM-23	8/12/2010	NA	NA	NA	1.13	NA	990	NA	NA	NA	NA	NA	1400	NA	NA
SHM-05-39A	SHM-05-39A	8/12/2010	NA	NA	NA	2.46	NA	6530	NA	NA	NA	NA	NA	12300	NA	NA
SHM-07-03	SHM-07-03	8/12/2010	NA	NA	NA	0.28 J	NA	841	NA	NA	NA	NA	NA	11600	NA	NA
	DUP2-081210	8/12/2010	NA	NA	NA	0.27 J	NA	893	NA	NA	NA	NA	NA	12100	NA	NA
SHM-07-05	SHM-07-05	8/12/2010	NA	NA	NA	9.23	NA	4530	NA	NA	NA	NA	NA	11500	NA	NA
	DUP-081210	8/12/2010	NA	NA	NA	9.53	NA	4540	NA	NA	NA	NA	NA	11500	NA	NA
SHM-99-31B	SHM-99-31B	8/12/2010	NA	NA	NA	0.93	NA	3860	NA	NA	NA	NA	NA	8460	NA	NA
SHM-05-041B	SHM-05-041B	8/9/2010	NA	NA	4.83	3.78	10000	8770 J	NA	NA	NA	NA	14900	12800 J	NA	NA
SHM-05-42A	SHM-05-42A	8/12/2010	NA	NA	NA	0.88	NA	1470	NA	NA	NA	NA	NA	2040	NA	NA
SHP-05-045A	SHP-05-045A	8/9/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
SHP-05-046B	SHP-05-046B	8/9/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA

Notes  
NA - Not Applicable  
ug/L is micrograms per liter  
mg/l - milligrams per liter  
J means estimated results  
B indicates that analyte was detected in the a



**TABLE 3**  
**GROUNDWATER MONITORING WELL RESULTS**  
**Shepley Hill Landfill, Devens Massachusetts**

Boring Location	Sample ID	Date	Vanadium		Zinc		Turbidity NTU	DO mg/L	pH	Temp Celcius	Spec Cond uS/cm	ORP mV	Color	Hardness mg/l	Alkalinity mg CaCO3/L	TDS mg/l	TSS mg/l
			Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)											
SHM-10-01	SHM-10-01-071310	7/13/2010	NA	NA	NA	NA	3.34	0.18	6.19	12.38	297	63.5	Clear	120	130	190	< 5
	SHM-10-01	8/12/2010	NA	NA	NA	NA	NA	0.49	6.61	11.86	291	42.2	NA	NA	130	NA	NA
	SHM-10-01-090810	9/8/2010	NA	NA	NA	NA	0.15	0.12	6.31	12.68	299	11.3	Clear	120	140	210	< 5
SHM-10-02	SHM-10-02-071510	7/15/2010	NA	NA	NA	NA	3.47	0.45	6.42	12.24	836	80.8	Clear	370	250	570	< 5
	Dup-071510	7/15/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	360	250	610	5.2
	SHM-10-02-090710	9/7/2010	NA	NA	NA	NA	0.64	0.87	5.94	12.45	881	-258.3	Clear	330	260	480	< 5
SHM-10-03	SHM-10-03-071410	7/14/2010	NA	NA	NA	NA	31.7	1.47	6.60	16.09	3331	75.7	Clear	310	96	1,900	28
	DUP-071410	7/14/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	320	95	1,900	17
	SHM-10-03-090710	9/7/2010	NA	NA	NA	NA	13.4	1.72	6.31	11.93	3341	148.1	Clear	420	78	1,900	28
	DUP-090710	9/7/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	410	75	1,900	7.8
SHM-10-04	SHM-10-04-071410	7/14/2010	NA	NA	NA	NA	17.7	0.23	6.37	10.82	630	9.9	Clear	200	99	380	34
	SHM-10-04-090710	9/7/2010	NA	NA	NA	NA	4.28	0.23	5.99	12.1	656	43.7	Clear	220	100	390	5.2
SHM-10-05A	SHM-10-05A-071510	7/15/2010	NA	NA	NA	NA	5.12	1.42	6.29	19.06	186	31.7	Clear	43	43	120	< 5
	SHM-10-05A-090810	9/8/2010	NA	NA	NA	NA	8.92	3.2	5.27	20.2	200	-29	Clear	41	36	110	< 5
SHM-10-06	SHM-10-06-070810	7/8/2010	NA	NA	NA	NA	21.4	0.55	6.62	21.74	754	-93.8	Cloudy	130	360	310	94
	DUP-070810	7/8/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	130	370	320	90
	SHM-10-06-090810	9/8/2010	NA	NA	NA	NA	3.22	2.83	6.16	11.59	783	-64.3	Clear	130	300	330	62
SHM-10-06A	SHM-10-06A-070710	7/7/2010	NA	NA	NA	NA	5.38	1.49	6.51	19.74	209	-22.6	Clear	48	100	120	< 5
	DUP-070710	7/7/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	52	97	130	< 5
	SHM-10-06A-090910	9/9/2010	NA	NA	NA	NA	40.6	0.39	5.94	10.65	431	-157.3	Cloudy	97	190	200	330
	DUP-090910	9/9/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	94	150	180	270
SHM-10-07	SHM-10-07-052710	5/27/2010	NA	NA	NA	NA	237	0.15	6.97	13.43	751	-195	Cloudy	210	300	320	120
	DUP-052710	5/27/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	210	280	370	640
	SHM-10-07-090910	9/9/2010	NA	NA	NA	NA	15.4	0.43	6.54	12.39	635	-105.6	Clear	130	240	300	53
SHM-10-08	SHM-10-08-071510	7/15/2010	NA	NA	NA	NA	7.15	0.21	6.73	10.95	917	33.7	Clear	480	480	630	12
	SHM-10-08-090710	9/7/2010	NA	NA	NA	NA	1.37	3.61	6.19	12.1	1079	-233	Clear	490	500	630	< 5
SHM-10-10	SHM-10-10-071310	7/13/2010	NA	NA	NA	NA	4.52	0.85	6.61	12.10	658	28.7	Clear	270	350	400	< 5
	DUP-071310	7/13/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	270	350	400	< 5
	SHM-10-10	8/12/2010	NA	NA	NA	NA	NA	0.76	6.57	11.27	622	-9.1	NA	NA	320	NA	NA
	SHM-10-10-090810	9/8/2010	NA	NA	NA	NA	0.71	0.16	6.55	13.13	617	63.3	Clear	260	320	380	< 5
	DUP-090810	9/8/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	260	330	350	< 5



**TABLE 3**  
**GROUNDWATER MONITORING WELL RESULTS**  
**Sheple'y Hill Landfill, Devens Massachusetts**

Boring Location	Sample ID	Date	Vanadium		Zinc		Turbidity NTU	DO mg/L	pH	Temp Celcius	Spec Cond uS/cm	ORP mV	Color	Hardness mg/l	Alkalinity mg CaCO3/L	TDS mg/l	TSS mg/l
			Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)											
SHM-10-11	SHM-10-11	8/30/2010	0.31 J	<0.154	10.9	13.8	4.05	1.68	6.12	13.19	419	-32	Clear	NA	160	NA	15
	SHM-10-11-101910	10/19/2010	< 0.308	< 0.308	17.6 J	17.9 J	4.28	0.41	6.28	11.57	4.14	-42.1	Cloudy		140		17
SHM-10-12	SHM-10-12	8/30/2010	<0.770	<0.770	35.2 J	37.7 J	8.43	3.55	6.04	14.41	460	-34.9	Clear	NA	240	NA	12
	DUP-083010	8/30/2010	<0.770	<0.770	46.8 J	36.5 J	NA	NA	NA	NA	NA	NA	NA	NA			
	SHM-10-12-102010	10/20/2010	0.385	0.385	26.7	29.2	1.6	0.32	5.93	10.92	432	-14.5	Clear	NA	240	NA	16
	DUP-102010	10/20/2010	<0.385	< 0.385	25.2	27.8	NA	NA	NA	NA	NA	NA	NA	NA	230	NA	14
SHM-10-13	GP-10-13-090110	9/1/2010	0.62	0.22 J	3.49 J	4.66 J	18.8	2.76	6.32	13.57	782	-68.6	Clear		380		43
	SHM-10-13-101910	10/19/2010	0.75 J	< 0.308	14.9 J	17.9 J	12	0.12	6.27	12.48	743	-52.5	Clear		360		62
	DUP-101910	10/19/2010	0.64 J	< 0.308	14.7 J	17.8 J	NA	NA	NA	NA	NA	NA	NA		360		56
SHM-10-14	SHM-10-14-090210	9/2/2010	< 0.77	< 0.77	54.6	30.6 J	34.7	0.18	6.35	14.48	645	-87.4	Clear	NA	360	NA	72
	SHM-10-14-101910	10/19/10	0.81 J	< 0.385	41	26.9	34.5	0.36	6.35	11.99	693	-38.6	Little Cloudy		320		130
SHM-10-15	GP-10-15-090110	9/1/2010	<0.770	<0.770	29.7 J	26.4 J	16.3	0.25	6.21	16.02	503	-52.7	Clear	NA	210	NA	170
	SHM-10-15-090110						16.3	0.25	6.21	16.02	503	-52.7	Clear	NA	240	NA	36
	DUP-090110	9/1/2010	<0.770	<0.770	22.7 J	20.1 J	NA	NA	NA	NA	NA	NA	NA				
	SHM-10-15-102010	10/20/2010	< 0.770	< 0.77	33.6 J	42.8 J	59.5	0.36	5.94	11.95	510	-10.9	Cloudy	NA	230	NA	140
SHM-10-16	SHM-10-16-090210	9/2/2010	1.65	0.08 J	7.99	5.39	78.5	0.17	6.98	11.4	784	-233.8	Little Cloudy	NA	330	NA	150
	DUP-090210	9/2/2010	1.85	0.08 J	9.34	3.91 J	NA	NA	NA	NA	NA	NA	NA				
	SHM-10-16-102010	10/20/2010	0.81	0.13 J	36.7	13	34.6	0.34	6.77	10.63	793	-129.2	Cloudy	NA	320	NA	170
SHL-23	SHL-23	8/12/2010	NA	NA	NA	NA	NA	10.06	6.45	10.42	25	209.8	NA	NA	4.3	NA	NA
SHM-05-39A	SHM-05-39A	8/12/2010	NA	NA	NA	NA	NA	0.35	6.45	11.37	263	-52.9	NA	NA	100	NA	NA
SHM-07-03	SHM-07-03	8/12/2010	NA	NA	NA	NA	NA	6.61	5.81	12.25	81	133.9	NA	NA	18	NA	NA
	DUP2-081210	8/12/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA				
SHM-07-05	SHM-07-05	8/12/2010	NA	NA	NA	NA	NA	0.40	6.45	11.43	256	-21.5	NA	NA	94	NA	NA
	DUP-081210	8/12/2010	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA				
SHM-99-31B	SHM-99-31B	8/12/2010	NA	NA	NA	NA	NA	0.19	6.03	10.74	186	33.9	NA	NA	86	NA	NA
SHM-05-041B	SHM-05-041B	8/9/2010	NA	NA	NA	NA	NA	0.32	6.43	11.75	310	42.6	NA	NA	NA	NA	45
SHM-05-42A	SHM-05-42A	8/12/2010	NA	NA	NA	NA	NA	1.20	6.50	10.39	61	89.5	NA	NA	18	NA	NA
SHP-05-045A	SHP-05-045A	8/9/2010	NA	NA	NA	NA	NA	0.30	6.20	13.97	294	-32.2	NA	NA	NA	NA	15
SHP-05-046B	SHP-05-046B	8/9/2010	NA	NA	NA	NA	NA	0.81	5.71	12.93	662	3	NA	NA	NA	NA	11

Notes  
 NA - Not Applicable  
 ug/L is micrograms per liter  
 mg/l - miligrams per liter  
 J means estimated results  
 B indicates that analyte was detected in the u

DO - Dissolved Oxygen  
 ORP - Oxygen Reduction Potential

TDS - Total Dissolved Solids  
 TSS - Total Suspended Solids



**TABLE 3  
GROUNDWATER MONITORING WELL RESULTS  
Shepley Hill Landfill, Devens Massachusetts**

Boring Location	Sample ID	Date	Ammonia mg/l	Nitrite mg/l	Sulfide mg/l	COD mg/l	TOC mg/l	Chloride mg/l	Nitrate mg/l	Sulfate mg/l	DOC mg/l	DIC mg/l	Notes
SHM-10-01	SHM-10-01-071310	7/13/2010	0.264	< 0.002	< 0.1	11 J	1.3	12	< 0.01	6.8	NA	NA	Test Kit (Filtered) < 5
	SHM-10-01	8/12/2010	0.241	< 0.002	< 0.10	< 7.0	NA	14	< 0.01	7.0	1.5	31	
	SHM-10-01-090810	9/8/2010	0.344	< 0.002	< 0.1	12 J	1.6	11	< 0.01	8.7	1.6	37	
SHM-10-02	SHM-10-02-071510	7/15/2010	0.248	< 0.002	< 0.1	< 7	2.4	160	< 0.01	20	NA	NA	
	Dup-071510	7/15/2010	0.231	< 0.002	< 0.1	< 7	2.5	160	< 0.01	21	NA	NA	
	SHM10-02-090710	9/7/2010	0.238	< 0.002	< 0.1	< 7	2.6	120	< 0.01	19	2.5	62	
SHM-10-03	SHM-10-03-071410	7/14/2010	0.035 J	0.02	< 0.1	25	0.64	1000	0.52	38	NA	NA	
	DUP-071410	7/14/2010	0.0269 J	0.02	< 0.1	47	0.73	1000	0.51	36	NA	NA	
	SHM-10-03-090710	9/7/2010	0.0392 J	< 0.002	< 0.1	43	0.66	1100	0.55	39	< 1	26	
	DUP-090710	9/7/2010	0.0204 J	< 0.002	< 0.1	31	0.66	1100	0.6	39	NA	NA	
SHM-10-04	SHM-10-04-071410	7/14/2010	0.0666 J	0.11	< 0.1	13 J	2.7	74	3.8	84	NA	NA	
	SHM-10-04-090710	9/7/2010	0.0585 J	0.5	< 0.1	< 7	2.6	92	3.7	87	2.7	43	
SHM-10-05A	SHM-10-05A-071510	7/15/2010	0.0184 J	0.01 J	< 0.1	< 7	0.93	34	0.38	10	NA	NA	
	SHM-10-05A-090810	9/8/2010	0.0335 J	< 0.002	< 0.1	55	0.96	29	0.46	11	< 1	20	
SHM-10-06	SHM-10-06-070810	7/8/2010	5.5	< 0.002	< 0.1	29	4.8	17	0.03	0.89	NA	NA	
	DUP-070810	7/8/2010	5.58	< 0.002	< 0.1	25	4.7	17	0.033	0.84	NA	NA	
	SHM-10-06-090810	9/8/2010	5.13	< 0.002	< 0.1	33	4.2	15	0.13	0.49 J	5	93	
SHM-10-06A	SHM-10-06A-070710	7/7/2010	2.69	< 0.002	< 0.1	16 J	3.4	3.4	0.03 J	2.5 B	NA	NA	
	DUP-070710	7/7/2010	2.59	< 0.002	< 0.1	20	3.3	3.4	0.032 J	2.9 B	NA	NA	
	SHM-10-06A-090910	9/9/2010	3.4	< 0.002	< 0.1	17 J	4	11	< 0.01	3.2	3.3	58	
	DUP-090910	9/9/2010	5.05	< 0.002	< 0.1	19 J	4.4	11	< 0.01	3.2	NA	NA	
SHM-10-07	SHM-10-07-052710	5/27/2010	6.02	< 0.002	< 0.1	45	3.6	48	0.008 J	8.6	NA	NA	
	DUP-052710	5/27/2010	5.78	< 0.002	< 0.1	58	3.5	48	0.013 J	9.3	NA	NA	
	SHM-10-07-090910	9/9/2010	5.6	< 0.002	< 0.1	29	3.8	41	< 0.01	2.3	3.5	52	
SHM-10-08	SHM-10-08-071510	7/15/2010	< 0.017	< 0.002	< 0.1	< 7	4	71	< 0.01	15	NA	NA	
	SHM-10-08-090710	9/7/2010	0.084	< 0.002	< 0.1	17 J	4.1	79	< 0.01	15	3.8	110	
SHM-10-10	SHM-10-10-071310	7/13/2010	0.155	< 0.002	< 0.1	29	3.6	19	< 0.01	0.56 J	NA	NA	
	DUP-071310	7/13/2010	0.145	< 0.002	< 0.1	40	3.6	18	< 0.01	0.38 J	NA	NA	
	SHM-10-10	8/12/2010	0.201	< 0.002	< 0.10	25		23	< 0.01	0.79 J	3.9	70	
	SHM-10-10-090810	9/8/2010	0.148	< 0.002	< 0.1	55	3.7	17	< 0.01	0.34 J	3.8	76	
	DUP-090810	9/8/2010	0.168	< 0.02	< 0.1	45	3.9	17	0.019 J	0.26 J	NA	NA	



**TABLE 3**  
**GROUNDWATER MONITORING WELL RESULTS**  
Sheple'y Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Ammonia mg/l	Nitrite mg/l	Sulfide mg/l	COD mg/l	TOC mg/l	Chloride mg/l	Nitrate mg/l	Sulfate mg/l	DOC mg/l	DIC mg/l	Notes
SHM-10-11	SHM-10-11	8/30/2010	2.79	<0.002	<0.10	22	NA	24	0.019 J	19	3.3	62	
	SHM-10-11-101910	10/19/2010	3.13	0.01 J	< 0.10	19		23	< 0.01	19 J	3.4	71	
SHM-10-12	SHM-10-12	8/30/2010	3.7	<0.002	<0.10	31	NA	3.7	0.035 J	1.7	4.1	110	
	DUP-083010	8/30/2010											
	SHM-10-12-102010	10/20/2010	3.8	< 0.02	< 0.10	33	NA	4.4	0.01	1.4	4.3	130	
	DUP-102010	10/20/2010	3.61	< 0.002	< 0.10	41	NA	4.4	< 0.01	1.3	4.5	140	
SHM-10-13	GP-10-13-090110	9/1/2010	9.7	< 0.002	< 0.1	33	NA	18	0.01 J	< 0.12	5.6	140	
	SHM-10-13-101910	10/19/2010	9.36	0.01 J	< 0.10	36		21	< 0.01	< 0.12	8.7	140	
	DUP-101910	10/19/2010	9.13	< 0.002	< 0.10	36		20	< 0.01	0.25 J	6.8	150	
SHM-10-14	SHM-10-14-090210	9/2/2010	3.96	< 0.002	< 0.10	43	NA	6.3	< 0.01	3.7	8.7	120	
	SHM-10-14-101910	10/19/10	5.28	0.01 J	< 0.10	62		4.8	0.08	0.67 J	62	140	
SHM-10-15	GP-10-15-090110	9/1/2010	2.67	0.01	< 0.10	33	NA	5.7	< 0.01	3.8	4.2	82	
	SHM-10-15-090110		2.26	< 0.002	< 0.10	22	NA	11	< 0.01	8.4	3.2	NA	
	DUP-090110	9/1/2010											
	SHM-10-15-102010	10/20/2010	2.15	0.01 J	< 0.10	64	NA	12	< 0.01	10	4	95	
SHM-10-16	SHM-10-16-090210	9/2/2010	3.31	< 0.002	< 0.1	36	NA	31	< 0.01	2.9	5.3	91	
	SHM-10-16-102010	10/20/2010	3.34	< 0.002	< 0.10	57	NA	28	< 0.01	3.2	10	100	
SHL-23	SHL-23	8/12/2010	0.0496 J	<0.002	<0.10	<7.0	NA	1.3	0.07	4.9	<1.0	< 8	Test Kit (Filtered) < 5
SHM-05-39A	SHM-05-39A	8/12/2010	4.01	<0.002	<0.10	11 J	NA	7.1	0.009 J	6	2.9	27	Test Kit (Filtered) 100
SHM-07-03	SHM-07-03	8/12/2010	0.0239 J	<0.002	<0.10	<7.0	NA	8.2	0.59	10	<1.0	12	Test Kit (Filtered) < 5
	DUP2-081210	8/12/2010											
SHM-07-05	SHM-07-05	8/12/2010	2.42	0.01 J	<0.10	<7.0	NA	8.9	0.06	8.1	2	24	Test Kit (Filtered) > 500
	DUP-081210	8/12/2010											
SHM-99-31B	SHM-99-31B	8/12/2010	4.1	<0.002	<0.10	11 J	NA	4	<0.01	3	6.5	28	Test Kit (Filtered) 5
SHM-05-041B	SHM-05-041B	8/9/2010	NA	NA	NA	NA	NA	NA	NA	NA	2.6	32	Test Kit (Filtered) 500
SHM-05-42A	SHM-05-42A	8/12/2010	0.0189 J	<0.002	<0.10	<7.0	NA	1.6	<0.01	5.6	<1.0	9.4	Test Kit (Filtered) < 5
SHP-05-045A	SHP-05-045A	8/9/2010	NA	NA	NA	NA	NA	NA	NA	NA	3.6	48	Test Kit (Filtered) 10
SHP-05-046B	SHP-05-046B	8/9/2010	NA	NA	NA	NA	NA	NA	NA	NA	14	150	Test Kit (Filtered) 80

Notes

NA - Not Applicable  
ug/L is micrograms per liter  
mg/l - milligrams per liter  
J means estimated results  
B indicates that analyte was detected in the a

COD - Chemical Oxygen Demand  
TOC - Total Organic Carbon

DOC - Dissolved Organic Carbon  
DIC - Dissolved Inorganic Carbon



**TABLE 4**  
**SOIL SAMPLING RESULTS**  
Shepley's Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Depth	Silver (mg/kg)	Sodium (mg/kg)	Thallium (mg/kg)	Vanadium (mg/kg)	Zinc (mg/kg)	TOC % Replicate 1	TOC % Replicate 2	Total Solids %
SP-10-07	SP-10-07-029	5/21/2010	29	< 0.092	48 J	< 0.262	5.33	14.2	0.01	0.011	83
	SDUP-052110	5/21/2010	29	< 0.086	45 J	< 0.246	4.57	13.6	0.012	< 0.01	84
	SP-10-07-041	5/21/2010	41	< 0.083	120	< 0.238	10.1	28.8	0.012	0.02	91
	SP-10-07-053	5/21/2010	53	< 0.766	510 J	< 2.19	49	109	0.032	0.032	99
SP-10-11	SP-10-11-003	8/12/2010	3	3.5	<24	<0.26	5.3	13	0.055	0.065	92
	SP-10-11-005	8/12/2010	5	1	120	<0.25	10	66	0.45	0.618	94
	SP-10-11-007	8/12/2010	7	2.2	61 J	<0.27	7.9	33	0.904	0.805	88
	SP-10-11-012	8/12/2010	12	0.24 J	92	<0.25	6.9	27	0.469	0.397	96
	SP-10-11-015	8/12/2010	15	14	85	<0.25	7.8	48	1.2	1.12	95
	SP-10-11-020	8/12/2010	20	0.84	73 J	<0.24	9.4	25 J	1.52	1.55	99
	SDUP-081210	8/12/2010	20	0.3 J	59 J	<0.24	9.2	22	--	--	98
	SP-10-11-023	8/12/2010	23	0.24 J	66 J	<0.25	7.1	18	0.03	0.043	95
	SP-10-11-025	8/12/2010	25	0.063 J	43 J	<0.27	5.6	12	0.025	0.025	89
	SDUP8-081210	8/12/2010	25	0.67	24 J	<0.25	8.2	14	--	--	94
	SP-10-11-033	8/12/2010	33	0.041 J	44 J	<0.30	4.7	11	<0.01	<0.01	79
	SP-10-11-040	8/12/2010	40	0.063 J	57 J	<0.27	5	10	0.036	0.036	90
	SP-10-11-055	8/12/2010	55	0.1 J	59 J	<0.27	5	11	<0.01	0.014	90
	SP-10-11-062	8/12/2010	62	6.4	180	<0.25	25	48	0.017	0.018	96
SP-10-12	SP-10-12-001	8/12/2010	1	0.2 J	61 J	<0.25	6.2	95	3.83	3.97	97
	SP-10-12-005	8/12/2010	5	0.82	240	<0.27	16	210	5.87	7.56	89
	SP-10-12-009	8/12/2010	9	0.23 J	<23	<0.25	8.4	16	0.744	0.714	98
	SP-10-12-015	8/12/2010	15	0.59	32 J	<0.26	5.3	12	0.185	0.129	94
	SP-10-12-017	8/12/2010	17	0.13 J	51 J	<0.26	3.8	8.5	0.094	0.058	91
	SP-10-12-025	8/12/2010	25	0.13 J	30 J	<0.26	4.7	12	<0.010	<0.010	91
	SP-10-12-035	8/12/2010	35	0.041 J	40 J	<0.30	4.9	17	0.062	0.152	81
	SDUP2-081210	8/12/2010	35	0.038 J	48 J	<0.29	4.9	17	--	--	84
	SP-10-12-040	8/12/2010	40	<0.03	50 J	<0.26	4.6	15	0.117	0.089	91
	SDUP3-081210	8/12/2010	40	0.032 J	28 J	<0.26	4.6	16	--	--	90
	SP-10-12-042	8/12/2010	42	<0.03	<26	<0.28	5	12	<0.010	<0.010	86
	SP-10-12-052	8/12/2010	52	<0.03	66 J	<0.26	4.3	11	0.019	<0.010	89
	SP-10-12-055	8/12/2010	55	0.029 J	<27	<0.29	4.6	11	<0.010	<0.010	81

**TABLE 4**  
**SOIL SAMPLING RESULTS**  
Shepley's Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Depth	Silver (mg/kg)	Sodium (mg/kg)	Thallium (mg/kg)	Vanadium (mg/kg)	Zinc (mg/kg)	TOC % Replicate 1	TOC % Replicate 2	Total Solids %
SP-10-13	SP-10-13-001	8/12/2010	1	0.091 J	<21	<0.23	5.7	11	0.057	0.061	100
	SP-10-13-005	8/12/2010	5	0.16 J	130	<0.26	10	22	0.332	0.320	93
	SP-10-13-008	8/12/2010	8	0.12 J	<24	<0.26	13	29	0.570	0.396	94
	SP-10-13-010	8/12/2010	10	0.15 J	42 J	<0.25	4.8	13	0.075	0.090	93
	SP-10-13-011	8/12/2010	11	0.026 J	<23	<0.25	4.4	9.7	<0.010	0.014	99
	SP-10-13-015	8/12/2010	15	0.22 J	44 J	<0.26	4.6	9	0.020	0.023	93
	SP-10-13-017	8/12/2010	17	0.027 J	27 J	<0.23	4.8	11	0.036	0.039	99
	SP-10-13-020	8/12/2010	20	0.1 J	38 J	<0.25	5.6	13	0.061	0.073	95
	SP-10-13-023	8/12/2010	23	0.68	3200	<0.52	14	13000	5.37	5.5	90
	SP-10-13-025	8/12/2010	25	0.051 J	<25	<0.27	7.2	20	0.343	0.324	89
	SP-10-13-027	8/12/2010	27	0.35 J	700	<0.44	4.3	2000	12.5	12.2	55
	SP-10-13-030	8/12/2010	30	0.042 J	<24	<0.26	3.4	10	9.48	7.37	93
	SP-10-13-032	8/12/2010	32	0.074 J	<23	<0.25	3.6	9.8	0.102	0.082	96
	SDUP4-081210	0812/2010	32	<0.03	<23	<0.25	3.4	9.1	--	--	94
	SP-10-13-035	8/12/2010	35	<0.03	43 J	<0.29	3.7	9.5	0.225	0.166	79
	SP-10-13-040	8/12/2010	40	0.08 J	150	<0.33	14	34	0.412	0.410	73
	SP-10-13-050	8/12/2010	50	<0.03	<24	<0.26	5	12	<0.010	<0.010	90
	SP-10-13-065	8/12/2010	65	<0.03	<24	<0.26	3.8	8.1	<0.010	<0.010	92
	SP-10-13-067	8/12/2010	67	<0.03	25 J	<0.27	4.8	10	<0.010	<0.010	84
	SDUP5-081210	8/12/2010	67	<0.03	<26	<0.28	4.5	9.8	--	--	85
	SP-10-13-070	8/12/2010	70	0.13 J	<22	<0.24	8.1	15	<0.010	0.017	96
	SP-10-13-072	8/12/2010	72	0.1 J	47 J	<0.25	6	13	<0.010	<0.010	94
	SP-10-13-075	8/12/2010	75	0.28 J	52 J	<0.27	7.2	16	<0.010	<0.010	90
	SP-10-13-077	8/12/2010	77	0.093 J	52 J	<0.27	4.5	22	<0.010	<0.010	89
	SP-10-13-083	8/12/2010	83	2.2	420	<0.26	2.1	85	<0.010	<0.010	91
SP-10-14	SP-10-14-005	8/17/2010	5	0.067 J	40 J	<0.26	6.1	14	0.077	0.073	93
	SP-10-14-010	8/17/2010	10	0.37 J	100	<0.25	13	91	0.752	0.858	93
	SP-10-14-015	8/17/2010	15	0.15 J	130	<0.30	5.7	160	0.293	0.287	80
	SP-10-14-020	8/17/2010	20	0.31 J	84 J	<0.26	39	120	5.11	4.63	91
	SP-10-14-023	8/17/2010	23	0.034 J	28 J	<0.28	5.6	36	0.160	0.127	86
	SP-10-14-027	8/17/2010	27	<0.09	260 J	<0.90	2	56	23.9	25.0	27
	SP-10-14-030	8/17/2010	30	<0.03	34 J	<0.32	4.8	11	4.76	5.41	72
	SDUP-081710	8/17/2010	30	<0.03	<27	<0.29	6.1	16	--	--	81
	SP-10-14-031	8/17/2010	31	<0.10	150 J	<0.98	4.4	12	14.7	14.3	24
	SP-10-14-035	8/17/2010	35	<0.05	82 J	<0.51	7.1	26	5.63	5.58	46
	SP-10-14-040	8/17/2010	40	<0.03	41 J	<0.34	7.2	27	1.26	1.23	70
	SP-10-14-044	8/17/2010	44	0.044 J	<25	<0.27	4.8	13	0.039	0.043	85
	SP-10-14-046	8/17/2010	46	<0.03	<25	<0.28	4.6	12	0.046	0.073	87
	SP-10-14-055	8/17/2010	55	<0.03	<26	<0.28	4.7	12	0.013	0.016	85
	SDUP2-081710	8/17/2010	55	<0.03	32 J	<0.28	4	11	--	--	85
	SP-10-14-060	8/17/2010	60	<0.03	<27	<0.29	6.8	15	<0.010	0.017	81
	SP-10-14-070	8/17/2010	70	<0.03	<26	<0.29	7.2	15	<0.010	<0.010	80
	SP-10-14-075	8/17/2010	75	<0.03	28 J	<0.28	5.3	16	0.011	0.013	84
	SP-10-14-080	8/17/2010	80	0.54	350	<0.25	6.5	31	0.032	0.025	93



TABLE 4  
SOIL SAMPLING RESULTS  
Shepley's Hill Landfill, Devens Massachusetts

[illegible]

Notes:

- mg/kg means milligrams per kilograms
- µg/kg means micrograms per kilograms
- J means estimated results
- B indicates that analyte was detected in the associated method
- < means less than
- > means greater than

TOC - Total Organic Carbon

**TABLE 4**  
**SOIL SAMPLING RESULTS**  
Shepley's Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Depth	Aluminum (mg/kg)	Antimony (mg/kg)	Arsenic (mg/kg)	Barium (mg/kg)	Beryllium (mg/kg)	Cadmium (mg/kg)	Calcium (mg/kg)	Chromium (mg/kg)	Cobalt (mg/kg)
SP-10-15	SP-10-15-001	8/12/2010	1	3,700	<0.17	8.6	10	0.34	<0.03	420	6.8	2.7
	SP-10-15-004	8/12/2010	4	5,500	0.66 J	17	25	0.49	0.7	930	16	2.9
	SP-10-15-005	8/12/2010	5	4,300	0.47 J	12	20	0.34	0.24 J	2,700	9.7	2.6
	SP-10-15-010	8/12/2010	10	4,300	0.35 J	11	16	0.27	0.14 J	920	11	2.7
	SP-10-15-015	8/12/2010	15	3,800	0.41 J	8.9	12	0.24 J	<0.04	830	11	2.4
	SP-10-15-017	8/12/2010	17	4,300	0.64 J	6.2	41	0.3	0.26 J	790	8.4	2.1
	SP-10-15-018	8/12/2010	18	9,300	11 J	25	120	<0.09	<0.24	9,000	69	14
	SP-10-15-020	8/12/2010	20	6,000	5.9	17	38	0.46	0.14 J	3,000	14	3.8
	SP-10-15-025	8/12/2010	25	4,900	4.0	16	170	0.35	0.27 J	4,500	35	4.5
	SDUP6-081210	8/12/2010	25	5,800	2.5 J	18	140	0.54	0.26 J	5,600	36	6.1
	SP-10-15-028	8/12/2010	28	4,800	<0.20	7.9	12	0.27	<0.04	340	10	1.5
	SP-10-15-030	8/12/2010	30	3,600	0.71 J	39	7.6	0.32	<0.04	390	7 J	2.3
	SDUP7-081210	8/12/2010	30	3,000	0.25 J	22	7	0.29	<0.04	490	5	1.9
	SP-10-15-035	8/12/2010	35	2,900	<0.21	15	6.4	0.23 J	<0.04	540	5.9	2
	SP-10-15-040	8/12/2010	40	2,700	0.27 J	15	5.8	0.2 J	<0.04	450	5.4	1.6
	SP-10-15-055	8/12/2010	55	3,600	0.26 J	58	14	0.78	0.19 J	1,500	4.4	1.6
SP-10-16	SP-10-16-036	9/1/2010	36	8,800	0.24 J	4.2	19	0.66	<0.03	920	32	5.7
	SDUP-081910	9/1/2010	36	9,600	0.24 J	6	23	0.76	0.03	770	32	6.5
	SP-10-16-050	9/1/2010	50	3,100	0.24 J	1.1	4.9	0.21 J	<0.04	330	7.6	2.1
	SP-10-16-053	9/1/2010	53	3,100	0.32 J	1.2	6.5	0.24	<0.04	400	8.8	2
	SP-10-16-060	9/1/2010	60	4,800	0.5 J	5	9.2	0.38	<0.04	490	16	3.5
	SP-10-16-065	9/1/2010	65	3,200	0.21 J	1.2	7.3	0.24	<0.03	390	8	2.4
	SDUP2-081910	9/1/2010	65	3,500	0.2 J	1.3	7.1	0.26	<0.04	390	9	2.6
	SP-10-16-070	9/1/2010	70	5,300	0.47 J	8.8	7.5	0.34	<0.03	520 J	16 J	3.4
	SP-10-16-080	9/1/2010	80	3,900	0.21 J	4.8	12	0.39	<0.04	880	12	2.6
	SP-10-16-093	9/1/2010	93	5,300	0.51	J	33	0.92	<0.03	3,700	17	4.3

Notes: mg/kg means milligrams per kilograms  
ug/kg means micrograms per kilograms  
J means estimated results  
B indicates that analyte was detected in the associated method blank  
< means less than                      > means greater than



**TABLE 4**  
**SOIL SAMPLING RESULTS**  
Shepley's Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Depth	Copper (mg/kg)	Iron (mg/kg)	Lead (mg/kg)	Magnesium (mg/kg)	Manganese (mg/kg)	Mercury (mg/kg)	Nickel (mg/kg)	Potassium (mg/kg)	Selenium (mg/kg)
SP-10-07	SP-10-07-029	5/21/2010	29	3.69	4,400	2.1	900 J	47.7	< 0.003	5.6	690	< 0.169
	SDUP-052110	5/21/2010	29	3.6	4,000	2.22	750	42.3	< 0.003	5.11	570	< 0.158
	SP-10-07-041	5/21/2010	41	9.8	9,100	5.36	3,100	129	< 0.003	16.2	1,400	0.175 J
	SP-10-07-053	5/21/2010	53	29.6	41,000	29.3	21,000	740	< 0.002	101	11,000	1.45 J
SP-10-11	SP-10-11-003	8/12/2010	3	6.8	5,300	5.9	1200	89	< 0.02	6.1	500	< 0.12
	SP-10-11-005	8/12/2010	5	8.1	9,700	110	2500	190	0.15	11	880	< 0.12
	SP-10-11-007	8/12/2010	7	9.3	7,700	22	1,900	180	< 0.02	9.7	710	< 0.12
	SP-10-11-012	8/12/2010	12	7.3	6,600	21	1,400	150	< 0.02	8.4	570	0.14 J
	SP-10-11-015	8/12/2010	15	33	12,000	24	1,600	130	0.03 J	16	570	0.12 J
	SP-10-11-020	8/12/2010	20	13 J	9,200	16	2,600	110 J	< 0.02	12	680 J	0.24 J
	SDUP-081210	8/12/2010	20	11	8,400	17	1,800	88	< 0.01	12	720	0.33 J
	SP-10-11-023	8/12/2010	23	7.5	7,900	10	2,000	150	< 0.02	12	660	< 0.12
	SP-10-11-025	8/12/2010	25	5.7	6,300	5.2	1,800	120	< 0.02	9.3	400	< 0.12
	SDUP8-081210	8/12/2010	25	6.2	7,700	6.3	2,500	120	< 0.02	12	490	< 0.12
	SP-10-11-033	8/12/2010	33	4.7	5,000	4.6	940	120	< 0.02	6.9	380	< 0.14
	SP-10-11-040	8/12/2010	40	4.7	5,600	4.9	1,400	100	< 0.02	7.8	350	0.14 J
	SP-10-11-055	8/12/2010	55	5.1	5,200	4.3	1,200	62	< 0.02	7.7	450	< 0.12
	SP-10-11-062	8/12/2010	62	12	19,000	13	11,000	440	< 0.02	45	5,600	< 0.23
SP-10-12	SP-10-12-001	8/12/2010	1	40	7,500	95	980	110	0.068 J	6.6	350	0.32 J
	SP-10-12-005	8/12/2010	5	260	31,000	510	2200	410	0.75	17	890	0.84 J
	SP-10-12-009	8/12/2010	9	7.3	8,500	8.5	1,900	76	< 0.02	9.3	410	0.26 J
	SP-10-12-015	8/12/2010	15	6.6	5,100	7.9	990	62	< 0.01	5.6	620	< 0.12
	SP-10-12-017	8/12/2010	17	7.9	3,700	3.5	660	43	< 0.02	3.2	490	< 0.12
	SP-10-12-025	8/12/2010	25	4.7	5,300	4.6	920	90	< 0.02	5.8	490	< 0.12
	SP-10-12-035	8/12/2010	35	9.7	5,300	16	1,200	80	0.43	5.9	330	0.18 J
	SDUP2-081210	8/12/2010	35	9	5,300	14	1,200	84	0.48	5.9	440	0.14 J
	SP-10-12-040	8/12/2010	40	12	5,200	12	1,100	70	0.22	5.8	360	< 0.12
	SDUP3-081210	8/12/2010	40	14	4,800	16	1,000	70	0.79	5.7	390	0.13 J
	SP-10-12-042	8/12/2010	42	4	4,900	4.4	1,100	84	< 0.02	5.9	480	< 0.13
	SP-10-12-052	8/12/2010	52	5.4	5,200	4.8	970	120	0.017 J	5.9	460	0.13 J
	SP-10-12-055	8/12/2010	55	4.5	4,600	4.1	1,200	57	< 0.02	6.1	330	< 0.13

**TABLE 4**  
**SOIL SAMPLING RESULTS**  
Shepley's Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Depth	Copper (mg/kg)	Iron (mg/kg)	Lead (mg/kg)	Magnesium (mg/kg)	Manganese (mg/kg)	Mercury (mg/kg)	Nickel (mg/kg)	Potassium (mg/kg)	Selenium (mg/kg)
SP-10-13	SP-10-13-001	8/12/2010	1	5	6,000	5.9	1200	97	<0.02	6	470	<0.11
	SP-10-13-005	8/12/2010	5	7.4	7,400	20	2300	120	<0.02	12	1000	<0.12
	SP-10-13-008	8/12/2010	8	7.7	9,000	9.4	2,700	130	1.6	9.6	1,500	0.14 J
	SP-10-13-010	8/12/2010	10	4.9	5,000	5.8	1,200	62	<0.02	6.7	360	0.21 J
	SP-10-13-011	8/12/2010	11	4	4,700	4.3	870	89	<0.02	5.2	430	0.12 J
	SP-10-13-015	8/12/2010	15	3.6	4,200	3.7	880	71	<0.02	4.4	560	<0.12
	SP-10-13-017	8/12/2010	17	4.4	5,100	4.5	1,000	96	<0.02	5.4	520	0.15 J
	SP-10-13-020	8/12/2010	20	5.2	6,000	5.7	1,400	100	<0.02	8.7	440	0.12 J
	SP-10-13-023	8/12/2010	23	33	17,000	49	2,100	3000	0.18	15	1,200	1.5
	SP-10-13-025	8/12/2010	25	5.3	6,100	5.3	1,600	64	<0.02	8.2	480	0.14 J
	SP-10-13-027	8/12/2010	27	15	9,700	53	990	660	0.17	5.5	280	3.0
	SP-10-13-030	8/12/2010	30	0.83	3,100	2.5	940	35	<0.02	3.9	160	0.14 J
	SP-10-13-032	8/12/2010	32	3.1	3,200	3.6	930	34	<0.02	5.6	320	<0.12
	SDUP4-081210	08/12/2010	32	2.7	3,100	3.5	900	34	<0.02	5.3	310	<0.12
	SP-10-13-035	8/12/2010	35	4.5	3,400	3.5	1,000	32	<0.02	5.8	330	<0.14
	SP-10-13-040	8/12/2010	40	71	16,000	13	3,400	150	<0.02	23	1,400	<0.16
	SP-10-13-050	8/12/2010	50	4.5	4,000	3.8	1400 J	44 J	<0.02	6.7	400	<0.12
	SP-10-13-065	8/12/2010	65	3.9	3900 J	3.3	930 J	33 J	<0.02	5.6	320	<0.12
	SP-10-13-067	8/12/2010	67	4.7	5,400	4.5	1,200	42	<0.02	7.2	380	<0.13
	SDUP5-081210	8/12/2010	67	4.5	4,900	4	1,100	39	<0.02	6.7	430	<0.13
	SP-10-13-070	8/12/2010	70	6.2	8,500	7.1	2,200	82	<0.02	9.2	450	<0.11
	SP-10-13-072	8/12/2010	72	5.5	9,200	7.3	1,600	130	<0.02	7.6	390	<0.12
	SP-10-13-075	8/12/2010	75	5.9	7,300	6.6	1,700	170	<0.02	8	600	<0.13
	SP-10-13-077	8/12/2010	77	3.4	4,800	9.4	1,100	230	<0.02	5.2	610	<0.12
	SP-10-13-083	8/12/2010	83	23	5,700	49	510	600	<0.02	2.5	2,000	<0.12
SP-10-14	SP-10-14-005	8/17/2010	5	6.2	6,600	6.0	1600	98	<0.02	8.5	520	0.16 J
	SP-10-14-010	8/17/2010	10	11	9,600	180	2500	140	0.23	14	790	0.16 J
	SP-10-14-015	8/17/2010	15	18	21,000	150	1,300	160	<0.02	16	300	0.44 J
	SP-10-14-020	8/17/2010	20	15	13,000	42	4,100	130	<0.02	23	1,500	0.14 J
	SP-10-14-023	8/17/2010	23	5.9	5,400	6.6	1,400	65	<0.02	8.8	460	<0.13
	SP-10-14-027	8/17/2010	27	6.9	9,300	10	1,500	400	<0.06	3 J	260 J	2.1 J
	SP-10-14-030	8/17/2010	30	4.6	4,100	4.7	1,200	41	<0.02	6.1	260	0.35 J
	SDUP-081710	8/17/2010	30	4.6	5,800	6	1,400	58	<0.02	7.9	280	0.14 J
	SP-10-14-031	8/17/2010	31	6.4	950	1.6 J	430	22	<0.07	4.2	<140	1.4 J
	SP-10-14-035	8/17/2010	35	6.1	4,900	3.9 J	1,200	57	<0.03	8.4	230	0.63 J
	SP-10-14-040	8/17/2010	40	7.3	8,000	6.6	1,400	54	<0.02	15	480	0.8 J
	SP-10-14-044	8/17/2010	44	4.5	4,100	4	1,300	39	<0.02	6.1	400	<0.13
	SP-10-14-046	8/17/2010	46	3.3	4,000	3.2	1,200	46	<0.02	5.5	450	<0.13
	SP-10-14-055	8/17/2010	55	6	4,100	3.7	1,200	44	<0.02	5.6	310	<0.13
	SDUP2-081710	8/17/2010	55	5	3,600	4.1	1,100	37	<0.02	5.5	270	<0.13
	SP-10-14-060	8/17/2010	60	6.3	6,200	5.6	1,400	60	<0.02	8.1	550	<0.14
	SP-10-14-070	8/17/2010	70	5.2	6,000	4.9	1,300	86	<0.02	7.3	850	<0.13
	SP-10-14-075	8/17/2010	75	4.1	5,200	5.3	1,400	170	<0.02	7.3	600	<0.13
	SP-10-14-080	8/17/2010	80	5.3	6,900	17	1,700	230	<0.02	8.7	2,200	<0.12



**TABLE 4**  
**SOIL SAMPLING RESULTS**  
Shepley's Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Depth	Copper (mg/kg)	Iron (mg/kg)	Lead (mg/kg)	Magnesium (mg/kg)	Manganese (mg/kg)	Mercury (mg/kg)	Nickel (mg/kg)	Potassium (mg/kg)	Selenium (mg/kg)
SP-10-15	SP-10-15-001	8/12/2010	1	5.9	5,900	5.7	1400	110	<0.02	7.1	470	<0.11
	SP-10-15-004	8/12/2010	4	24	9,400	110	2100	120	0.33	12	810	0.19 J
	SP-10-15-005	8/12/2010	5	10	11,000	39	1,600	230	0.049 J	9.3	550	0.16 J
	SP-10-15-010	8/12/2010	10	8.2	8,100	21	1,800	100	0.037 J	11	410	0.16 J
	SP-10-15-015	8/12/2010	15	7.1	7,000	12	1,600	81	<0.02	9.6	330	0.17 J
	SP-10-15-017	8/12/2010	17	11	12,000	38	1,400	130	0.17	9.0	420	0.33 J
	SP-10-15-018	8/12/2010	18	310	140,000	1200	600	1100	0.44	75	380 J	2.9 J
	SP-10-15-020	8/12/2010	20	14	9,900	220	1,800	110	0.067 J	12	530	0.39 J
	SP-10-15-025	8/12/2010	25	38	24,000	260	1,900	240	0.32	20	480	0.46 J
	SDUP6-081210	8/12/2010	25	41	23,000	390	2,600	240	0.15	23	930	0.44 J
	SP-10-15-028	8/12/2010	28	3.7	5,800	5.3	2,000	58	<0.02	6.3	320	<0.13
	SP-10-15-030	8/12/2010	30	5.6	7,800	5.8	1400 J	64 J	<0.02	7.8	360	0.27 J
	SDUP7-081210	8/12/2010	30	4.4	5,600	4.6	1,100	50	<0.02	6.3	350	<0.14
	SP-10-15-035	8/12/2010	35	5	5,100	4.6	1,200	62	<0.02	6.6	300	<0.14
	SP-10-15-040	8/12/2010	40	4.1	6,300	4.8	1,200	310	<0.02	5.9	270	<0.14
	SP-10-15-055	8/12/2010	55	4.3	4,100	21	590	680	<0.02	2.5	1,200	<0.12
SP-10-16	SP-10-16-036	9/1/2010	36	13	12,000	9.6	5700	100	<0.02	20	1400	<0.12
	SDUP-081910	9/1/2010	36	13	13,000	12	6400	120	<0.02	24	2000	<0.12
	SP-10-16-050	9/1/2010	50	3.1	4,300	3.9	1500	40	<0.02	8.7	330	<0.14
	SP-10-16-053	9/1/2010	53	3.8	4,100	4	1,600	40	<0.02	9.6	420	<0.12
	SP-10-16-060	9/1/2010	60	18	8,800	8.2	2,700	72	<0.02	15	520	<0.12
	SP-10-16-065	9/1/2010	65	4.3	4,000	3.8	1,500	37	<0.02	9.7	420	<0.12
	SDUP2-081910	9/1/2010	65	5.2	4,500	5.2	1,800	43	<0.02	11	430	<0.12
	SP-10-16-070	9/1/2010	70	6.6	9,400	8.2	3,100	82 J	<0.02	14.0	500	<0.12
	SP-10-16-080	9/1/2010	80	4.8	7,100	6.4	2,200	100	<0.02	9.4	900	<0.13
	SP-10-16-093	9/1/2010	93	12	12,000	14	2,700	310	<0.02	7.9	2,300	<0.12

Notes: mg/kg means milligrams per kilograms  
ug/kg means micrograms per kilograms  
J means estimated results  
B indicates that analyte was detected in the associated meth  
< means less than                      > means greater than

**TABLE 4**  
**SOIL SAMPLING RESULTS**  
Shepley's Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Depth	Silver (mg/kg)	Sodium (mg/kg)	Thallium (mg/kg)	Vanadium (mg/kg)	Zinc (mg/kg)	TOC %	TOC %	Total Solids %
SP-10-07	SP-10-07-029	5/21/2010	29	< 0.092	48 J	< 0.262	5.33	14.2	0.01	0.011	83
	SDUP-052110	5/21/2010	29	< 0.086	45 J	< 0.246	4.57	13.6	0.012	< 0.01	84
	SP-10-07-041	5/21/2010	41	< 0.083	120	< 0.238	10.1	28.8	0.012	0.02	91
	SP-10-07-053	5/21/2010	53	< 0.766	510 J	< 2.19	49	109	0.032	0.032	99
SP-10-11	SP-10-11-003	8/12/2010	3	3.5	<24	<0.26	5.3	13	0.055	0.065	92
	SP-10-11-005	8/12/2010	5	1	120	<0.25	10	66	0.45	0.618	94
	SP-10-11-007	8/12/2010	7	2.2	61 J	<0.27	7.9	33	0.904	0.805	88
	SP-10-11-012	8/12/2010	12	0.24 J	92	<0.25	6.9	27	0.469	0.397	96
	SP-10-11-015	8/12/2010	15	14	85	<0.25	7.8	48	1.2	1.12	95
	SP-10-11-020	8/12/2010	20	0.84	73 J	<0.24	9.4	25 J	1.52	1.55	99
	SDUP-081210	8/12/2010	20	0.3 J	59 J	<0.24	9.2	22	--	--	98
	SP-10-11-023	8/12/2010	23	0.24 J	66 J	<0.25	7.1	18	0.03	0.043	95
	SP-10-11-025	8/12/2010	25	0.063 J	43 J	<0.27	5.6	12	0.025	0.025	89
	SDUP8-081210	8/12/2010	25	0.67	24 J	<0.25	8.2	14	--	--	94
	SP-10-11-033	8/12/2010	33	0.041 J	44 J	<0.30	4.7	11	<0.01	<0.01	79
	SP-10-11-040	8/12/2010	40	0.063 J	57 J	<0.27	5	10	0.036	0.036	90
	SP-10-11-055	8/12/2010	55	0.1 J	59 J	<0.27	5	11	<0.01	0.014	90
	SP-10-11-062	8/12/2010	62	6.4	180	0.25	25	48	0.017	0.018	96
SP-10-12	SP-10-12-001	8/12/2010	1	0.2 J	61 J	<0.25	6.2	95	3.83	3.97	97
	SP-10-12-005	8/12/2010	5	0.82	240	<0.27	16	210	5.87	7.56	89
	SP-10-12-009	8/12/2010	9	0.23 J	<23	<0.25	8.4	16	0.744	0.714	98
	SP-10-12-015	8/12/2010	15	0.59	32 J	<0.26	5.3	12	0.185	0.129	94
	SP-10-12-017	8/12/2010	17	0.13 J	51 J	<0.26	3.8	8.5	0.094	0.058	91
	SP-10-12-025	8/12/2010	25	0.13 J	30 J	<0.26	4.7	12	<0.010	<0.010	91
	SP-10-12-035	8/12/2010	35	0.041 J	40 J	<0.30	4.9	17	0.062	0.152	81
	SDUP2-081210	8/12/2010	35	0.038 J	48 J	<0.29	4.9	17	--	--	84
	SP-10-12-040	8/12/2010	40	<0.03	50 J	<0.26	4.6	15	0.117	0.089	91
	SDUP3-081210	8/12/2010	40	0.032 J	28 J	<0.26	4.6	16	--	--	90
	SP-10-12-042	8/12/2010	42	<0.03	<26	<0.28	5	12	<0.010	<0.010	86
	SP-10-12-052	8/12/2010	52	<0.03	66 J	<0.26	4.3	11	0.019	<0.010	89
	SP-10-12-055	8/12/2010	55	0.029 J	<27	<0.29	4.6	11	<0.010	<0.010	81



**TABLE 4**  
**SOIL SAMPLING RESULTS**  
Shepley's Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Depth	Silver (mg/kg)	Sodium (mg/kg)	Thallium (mg/kg)	Vanadium (mg/kg)	Zinc (mg/kg)	TOC %	TOC %	Total Solids %
SP-10-13	SP-10-13-001	8/12/2010	1	0.091 J	<21	<0.23	5.7	11	0.057	0.061	100
	SP-10-13-005	8/12/2010	5	0.16 J	130	<0.26	10	22	0.332	0.320	93
	SP-10-13-008	8/12/2010	8	0.12 J	<24	<0.26	13	29	0.570	0.396	94
	SP-10-13-010	8/12/2010	10	0.15 J	12 J	<0.25	4.8	13	0.075	0.090	93
	SP-10-13-011	8/12/2010	11	0.026 J	<23	<0.25	4.4	9.7	<0.010	0.014	99
	SP-10-13-015	8/12/2010	15	0.22 J	44 J	<0.26	4.6	9	0.020	0.023	93
	SP-10-13-017	8/12/2010	17	0.027 J	27 J	<0.23	4.8	11	0.036	0.039	99
	SP-10-13-020	8/12/2010	20	0.1 J	38 J	<0.25	5.6	13	0.061	0.073	95
	SP-10-13-023	8/12/2010	23	0.68	3200	<0.52	14	13000	5.37	5.5	90
	SP-10-13-025	8/12/2010	25	0.051 J	<25	<0.27	7.2	20	0.343	0.324	89
	SP-10-13-027	8/12/2010	27	0.35 J	700	<0.44	4.3	2000	12.5	12.2	55
	SP-10-13-030	8/12/2010	30	0.042 J	<24	<0.26	3.4	10	9.48	7.37	93
	SP-10-13-032	8/12/2010	32	0.074 J	<23	<0.25	3.6	9.8	0.102	0.082	96
	SDUP4-081210	08/12/2010	32	<0.03	<23	<0.25	3.4	9.1	--	--	94
	SP-10-13-035	8/12/2010	35	<0.03	43 J	<0.29	3.7	9.5	0.225	0.166	79
	SP-10-13-040	8/12/2010	40	0.08 J	150	<0.33	14	34	0.412	0.410	73
	SP-10-13-050	8/12/2010	50	<0.03	<24	<0.26	5	12	<0.010	<0.010	90
	SP-10-13-065	8/12/2010	65	0.03	24	<0.26	3.8	8.1	0.010	0.010	92
	SP-10-13-067	8/12/2010	67	<0.03	25 J	<0.27	4.8	10	<0.010	<0.010	84
	SDUP5-081210	8/12/2010	67	<0.03	<26	<0.28	4.5	9.8	--	--	85
	SP-10-13-070	8/12/2010	70	0.13 J	<22	<0.24	8.1	15	<0.010	0.017	96
	SP-10-13-072	8/12/2010	72	0.1 J	47 J	<0.25	6	13	<0.010	<0.010	94
	SP-10-13-075	8/12/2010	75	0.28 J	52 J	<0.27	7.2	16	<0.010	<0.010	90
	SP-10-13-077	8/12/2010	77	0.093 J	52 J	<0.27	4.5	22	<0.010	<0.010	89
	SP-10-13-083	8/12/2010	83	2.2	420	<0.26	2.1	85	<0.010	<0.010	91
SP-10-14	SP-10-14-005	8/17/2010	5	0.067 J	40 J	<0.26	6.1	14	0.077	0.073	93
	SP-10-14-010	8/17/2010	10	0.37 J	100	<0.25	13	91	0.752	0.858	93
	SP-10-14-015	8/17/2010	15	0.15 J	130	<0.30	5.7	160	0.293	0.287	80
	SP-10-14-020	8/17/2010	20	0.31 J	84 J	<0.26	39	120	5.11	4.63	91
	SP-10-14-023	8/17/2010	23	0.034 J	28 J	<0.28	5.6	36	0.160	0.127	86
	SP-10-14-027	8/17/2010	27	<0.09	260 J	<0.90	2	56	23.9	25.0	27
	SP-10-14-030	8/17/2010	30	<0.03	34 J	<0.32	4.8	11	4.76	5.41	72
	SDUP-081710	8/17/2010	30	<0.03	<27	<0.29	6.1	16	--	--	81
	SP-10-14-031	8/17/2010	31	<0.10	150 J	<0.98	4.4	12	14.7	14.3	24
	SP-10-14-035	8/17/2010	35	<0.05	82 J	<0.51	7.1	26	5.63	5.58	46
	SP-10-14-040	8/17/2010	40	<0.03	41 J	<0.34	7.2	27	1.26	1.23	70
	SP-10-14-044	8/17/2010	44	0.044 J	<25	<0.27	4.8	13	0.039	0.043	85
	SP-10-14-046	8/17/2010	46	<0.03	<25	<0.28	4.6	12	0.046	0.073	87
	SP-10-14-055	8/17/2010	55	<0.03	<26	<0.28	4.7	12	0.013	0.016	85
	SDUP2-081710	8/17/2010	55	<0.03	32 J	<0.28	4	11	--	--	85
	SP-10-14-060	8/17/2010	60	<0.03	<27	<0.29	6.8	15	<0.010	0.017	81
	SP-10-14-070	8/17/2010	70	<0.03	<26	<0.29	7.2	15	<0.010	<0.010	80
	SP-10-14-075	8/17/2010	75	<0.03	28 J	<0.28	5.3	16	0.011	0.013	84
	SP-10-14-080	8/17/2010	80	0.54	350	<0.25	6.5	31	0.032	0.025	93

**TABLE 4**  
**SOIL SAMPLING RESULTS**  
Shepley's Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Depth	Aluminum (mg/kg)	Antimony (mg/kg)	Arsenic (mg/kg)	Barium (mg/kg)	Beryllium (mg/kg)	Cadmium (mg/kg)	Calcium (mg/kg)	Chromium (mg/kg)	Cobalt (mg/kg)
SP-10-07	SP-10-07-029	5/21/2010	29	2,800	< 0.381	5.61	14.2	0.183 J	< 0.039	640 J	4.7	2.1
	SDUP-052110	5/21/2010	29	2,500	< 0.357	5.15	12	0.172 J	< 0.036	700	4	1.92
	SP-10-07-041	5/21/2010	41	5,900	0.469 J	12.2	19.3	0.298	0.0613 J	1,400	15	4.15
	SP-10-07-053	5/21/2010	53	30,000	< 3.18	32.4	74.6	1.01 J	< 0.322	25,000	68	21.2
SP-10-11	SP-10-11-003	8/12/2010	3	3,300	< 0.19	6.6	8.9	0.32	< 0.04	320	6.4	2.1
	SP-10-11-005	8/12/2010	5	5,600	0.3 J	11	86	0.52	0.21 J	1000	14	3.5
	SP-10-11-007	8/12/2010	7	4,800	< 0.19	10	14	0.39	< 0.04	760	12	2.8
	SP-10-11-012	8/12/2010	12	4,400	< 0.18	12	14	0.38	< 0.03	610	8.4	2.5
	SP-10-11-015	8/12/2010	15	4,500	0.43 J	12	15	0.44	220	860	42	3
	SP-10-11-020	8/12/2010	20	5,400	0.25 J	11	38 J	0.44	2.1 J	680 J	12 J	2.7
	SDUP-081210	8/12/2010	20	4,700	< 0.17	13	20	0.42	0.16 J	580	9.7	2.8
	SP-10-11-023	8/12/2010	23	4,500	< 0.18	12	12	0.36	0.05 J	430	9.1	4.9
	SP-10-11-025	8/12/2010	25	3,200	< 0.19	7.8	7.2	0.25	< 0.04	490	10	2.1
	SDUP8-081210	8/12/2010	25	4,300	< 0.18	8	8.6	0.35	0.17 J	700	22	2.9
	SP-10-11-033	8/12/2010	33	3,000	< 0.22	9.7	11	0.31	< 0.04	800	5.1	1.8
	SP-10-11-040	8/12/2010	40	3,100	< 0.19	9.8	8.9	0.26	< 0.04	410	8.1	1.8
	SP-10-11-055	8/12/2010	55	3,000	< 0.19	10	8.4	0.28	< 0.04	520	6.7	2.0
	SP-10-11-062	8/12/2010	62	17,000	< 0.18	9.4	58	1.8	0.03	24,000	59	9.6
SP-10-12	SP-10-12-001	8/12/2010	1	3,200	0.35 J	5.4	13	0.24	< 0.03	630	6.4	2.5
	SP-10-12-005	8/12/2010	5	6,900	2.2 J	12	78	0.59	< 0.04	4200	18	5.8
	SP-10-12-009	8/12/2010	9	7,100	0.22 J	13	9.5	0.42	< 0.03	560	9.8	2.6
	SP-10-12-015	8/12/2010	15	3,400	< 0.18	9.6	10	0.35	< 0.03	690	5.6	2.2
	SP-10-12-017	8/12/2010	17	2,200	< 0.19	6.2	9.3	0.25	< 0.04	700	3.8	1.5
	SP-10-12-025	8/12/2010	25	2,600	< 0.19	9.0	9.2	0.25	< 0.04	760	4.8	2.4
	SP-10-12-035	8/12/2010	35	3,100	< 0.22	9.4	8.1	0.2 J	< 0.04	480	6.3	1.7
	SDUP2-081210	8/12/2010	35	3,200	< 0.21	9.2	9	0.24	< 0.04	580	6.1	1.7
	SP-10-12-040	8/12/2010	40	3,000	0.2 J	14	7.7	0.21 J	< 0.04	660	7	1.8
	SDUP3-081210	8/12/2010	40	2,800	< 0.19	15	8.7	0.24	< 0.04	640	7.4	1.8
	SP-10-12-042	8/12/2010	42	3,100	< 0.20	29	8.6	0.31	< 0.04	560	5.7	1.7
	SP-10-12-052	8/12/2010	52	2,800	< 0.19	26	8.4	0.28	< 0.04	480	10	2
	SP-10-12-055	8/12/2010	55	2,900	< 0.21	34	6.3	0.28	< 0.04	330	6.7	1.6



**TABLE 4**  
**SOIL SAMPLING RESULTS**  
Shepley's Hill Landfill, Devens Massachusetts

Boring Location	Sample ID	Date	Depth	Aluminum (mg/kg)	Antimony (mg/kg)	Arsenic (mg/kg)	Barium (mg/kg)	Beryllium (mg/kg)	Cadmium (mg/kg)	Calcium (mg/kg)	Chromium (mg/kg)	Cobalt (mg/kg)
SP-10-13	SP-10-13-001	8/12/2010	1	3,500	0.2 J	8.4	9.4	0.28	<0.03	500	5.6	2.3
	SP-10-13-005	8/12/2010	5	5,100	<0.18	8.8	18	0.45	<0.03	1100	16	3.2
	SP-10-13-008	8/12/2010	8	6,200	<0.19	9.1	18	0.66	<0.04	490	18	2.9
	SP-10-13-010	8/12/2010	10	3,400	<0.18	5.3	7.2	0.28	<0.03	570	6.4	1.9
	SP-10-13-011	8/12/2010	11	2,700	<0.18	7.4	8.5	0.27	<0.03	560	4.4	2
	SP-10-13-015	8/12/2010	15	2,800	<0.18	6.2	11	0.29	<0.03	560	5.2	1.8
	SP-10-13-017	8/12/2010	17	3,000	<0.17	6.7	10	0.28	<0.03	520	4.8	1.9
	SP-10-13-020	8/12/2010	20	3,300	<0.18	5.6	12	0.26	<0.03	490	7.6	3.3
	SP-10-13-023	8/12/2010	23	5,600	4.4	31	43	0.49	3.5	2,100	52	4.5
	SP-10-13-025	8/12/2010	25	4,200	<0.19	7.5	12	0.31	<0.04	460	8.6	2.5
	SP-10-13-027	8/12/2010	27	1,900	0.9 J	7	81	0.26 J	0.65 J	14,000	3.9	1.6
	SP-10-13-030	8/12/2010	30	2,600	<0.19	0.8	5.3	0.13 J	<0.04	390	4.7	1.4
	SP-10-13-032	8/12/2010	32	2,600	<0.18	1.5	5.4	0.19 J	<0.03	550	4.6	1.4
	SDUP4-081210	08/12/2010	32	2,500	<0.18	1.6	5.2	0.19 J	<0.03	600	4.4	1.3
	SP-10-13-035	8/12/2010	35	2,800	<0.21	1.7	5.9	0.19 J	<0.04	380	5.4	1.4
	SP-10-13-040	8/12/2010	40	9,300	<0.24	5.9	27	0.84	<0.05	2,500	48	5.9
	SP-10-13-050	8/12/2010	50	3,200	<0.19	1.3	8.5	0.27	<0.04	480 J	6.9	2.3
	SP-10-13-065	8/12/2010	65	2500 J	0.18	3.8	9.1	0.19 J	0.03	420	4.6 J	1.4
	SP-10-13-067	8/12/2010	67	3,200	<0.20	5.6	12	0.23	<0.04	450	5.9	1.7
	SDUP5-081210	8/12/2010	67	3,000	<0.20	5.4	13	0.24	<0.04	500	5.3	1.8
	SP-10-13-070	8/12/2010	70	4,900	<0.17	9.4	12	0.33	<0.03	360	13	4.3
	SP-10-13-072	8/12/2010	72	3,600	0.22 J	7.6	8.6	0.26	<0.03	680	8.2	1.8
	SP-10-13-075	8/12/2010	75	4,000	<0.20	13	10	0.34	<0.04	560	9.3	2.3
	SP-10-13-077	8/12/2010	77	2,700	<0.19	14	9.9	0.49	<0.04	1,100	6.2	1.7
	SP-10-13-083	8/12/2010	83	3,800	<0.19	23	15	0.94	0.3 J	1,600	6	1.4
SP-10-14	SP-10-14-005	8/17/2010	5	4,100	0.28 J	8.5	10	0.32	<0.03	250	8.6	2.7
	SP-10-14-010	8/17/2010	10	7,400	0.64 J	18	27	0.55	0.059 J	3900	16	4.1
	SP-10-14-015	8/17/2010	15	4,800	1.5 j	12	200	0.29	<0.04	1,400	14	4.6
	SP-10-14-020	8/17/2010	20	8,000	0.43 J	18	32	0.72	<0.04	1,100	26	4.6
	SP-10-14-023	8/17/2010	23	3,300	0.46 J	6.0	13	0.28	<0.04	770	6.8	2.4
	SP-10-14-027	8/17/2010	27	1,400	0.88 J	3.8	63	0.24 J	<0.12	19,000	1.5	1.2 J
	SP-10-14-030	8/17/2010	30	4,200	0.25 J	9.5	12	0.33	<0.04	1,800	6.2	1.4
	SDUP-081710	8/17/2010	30	5,200	0.35 J	11	9.8	0.37	<0.04	550	7.6	1.7
	SP-10-14-031	8/17/2010	31	3,000	<0.70	8.5	35	0.35 J	<0.13	6,300	4.8	0.95 J
	SP-10-14-035	8/17/2010	35	3,600	0.38 J	60	13	0.33 J	<0.07	1,700	8.4	4.9
	SP-10-14-040	8/17/2010	40	3,400	0.59 J	34	10	0.37	<0.05	1,100	7.6	4.3
	SP-10-14-044	8/17/2010	44	3,100	0.41 J	2.8	7.5	0.22	<0.04	440	5.9	2
	SP-10-14-046	8/17/2010	46	2,900	0.3 J	2.6	6.8	0.23	<0.04	760	5.8	1.6
	SP-10-14-055	8/17/2010	55	3,000	0.25 J	4.8	5.8	0.24	<0.04	490	6	1.4
	SDUP2-081710	8/17/2010	55	2,700	0.22 J	5	5.4	0.22 J	<0.04	540	5.6	1.3
	SP-10-14-060	8/17/2010	60	4,800	0.22 J	13	11	0.51	<0.04	890	7.7	3
	SP-10-14-070	8/17/2010	70	4,400	<0.21	35	15	0.5	<0.04	1,100	7.2	2.1
	SP-10-14-075	8/17/2010	75	3,400	0.32 J	51	11	0.37	<0.04	760	6.7	2.2
	SP-10-14-080	8/17/2010	80	5,700	0.26 J	62	20	0.86	<0.03	1,300	15	2.7

TABLE 4  
SOIL SAMPLING RESULTS

Boring Location	Sample ID	Date	Depth	Silver (mg/kg)	Sodium (mg/kg)	Thallium (mg/kg)	Vanadium (mg/kg)	Zinc (mg/kg)	TOC %	TOC %	Total Solids %
SP-10-15	SP-10-15-001	8/12/2010	1	0.1 J	<22	<0.24	6	13	0.034	0.027	99
	SP-10-15-004	8/12/2010	4	1.3	95	<0.25	12	83	1.50	1.81	96
	SP-10-15-005	8/12/2010	5	0.71	85	<0.25	8.8	55	0.742	0.618	98
	SP-10-15-010	8/12/2010	10	12	100	<0.30	6.2	53	1.24	1.53	83
	SP-10-15-015	8/12/2010	15	1.1	120	<0.30	5.6	140	0.341	0.499	80
	SP-10-15-017	8/12/2010	17	0.32 J	100	<0.26	10	86	1.52	2.45	93
	SP-10-15-018	8/12/2010	18	1.2 J	940	<1.8	6.4	1000	9.38	7.54	65
	SP-10-15-020	8/12/2010	20	3	93	<0.27	17	110	4.47	7.27	88
	SP-10-15-025	8/12/2010	25	0.8	210	<0.31	37	220	5.45	4.80	76
	SDUP6-081210	8/12/2010	25	0.72	210	<0.32	30	380	--	--	76
	SP-10-15-028	8/12/2010	28	0.037 J	27 J	<0.29	8.5	11	0.473	0.358	80
	SP-10-15-030	8/12/2010	30	0.15 J	51 J	<0.31	5.6	13	0.188	0.038	78
	SDUP7-081210	8/12/2010	30	0.074 J	40 J	<0.30	4.6	11	--	--	80
	SP-10-15-035	8/12/2010	35	0.034 J	55 J	<0.29	4.4	9.5	0.111	0.074	81
	SP-10-15-040	8/12/2010	40	0.033 J	41 J	<0.31	4	9.7	0.056	0.026	77
SP-10-15-055	8/12/2010	55	1.2	220	<0.26	2.2	48	0.039	0.027	91	
SP-10-16	SP-10-16-036	9/1/2010	36	0.098 J	25 J	<0.26	16	29	0.037	0.036	92
	SDUP-081910	9/1/2010	36	0.098 J	24	0.26	19	34	-	-	93
	SP-10-16-050	9/1/2010	50	<0.03	<27	<0.29	4.8	12	<0.010	0.018	84
	SP-10-16-053	9/1/2010	53	<0.03	36 J	<0.26	4.8	13	0.02	0.014	88
	SP-10-16-060	9/1/2010	60	0.038 J	39 J	<0.27	8.5	18	0.015	0.016	87
	SP-10-16-065	9/1/2010	65	<0.03	39 J	<0.26	4.6	13	<0.010	0.014	90
	SDUP2-081910	9/1/2010	65	0.032 J	34 J	<0.27	5.5	13	-	-	90
	SP-10-16-070	9/1/2010	70	0.041 J	41 J	<0.26	9.7	18	0.022	0.021	93
	SP-10-16-080	9/1/2010	80	0.047 J	64 J	<0.27	7.6	16	<0.01	0.013	85
	SP-10-16-093	9/1/2010	93	0.45	380	<0.26	9.9	33	0.04	0.045	90

Notes:

- mg/kg means milligrams per kilograms
- ug/kg means micrograms per kilograms
- J means estimated results
- B indicates that analyte was detected in the associated method
- < means less than
- > means greater than

TOC - Total Organic Carbon



**TABLE 5**  
**Arsenic Comparison And Field Sampling Parameters**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Arsenic			Iron		Manganese		Turbidity NTU	DO mg/L	pH	Temp Celcius	Spec Cond uS/cm	ORP mV
					Total (ug/L)	Dissolved (ug/L)	Field Kit (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)						
GP-10-01	GP-10-01-009	5/27/2010	10:00	9	0.48 J	0.3 J	<5	NA	827	NA	21.6	10	5.34	6.35	10.08	265	107
	GP-10-01-019	5/27/2010	10:35	19	4.61	0.32 J	<5	NA	548	NA	49.7	90	2.61	5.99	11.36	401	84.3
	GDUP-052710	5/27/2010	10:35	19	NA	0.27 J	NA	NA	525	NA	45.5	See GP-10-01-019					
	GP-10-01-029	5/27/2010	11:20	29	11.4	0.31 J	5	NA	549	NA	196	230	4.49	6.08	11.07	385	83.2
	GP-10-01-039	5/27/2010	11:45	39	9.39	<1.13	5	NA	1,860	NA	14,000	80	0.37	6.00	11.81	671	62.7
	GP-10-01-049	5/27/2010	12:30	49	7.39	<1.13	5	NA	863	NA	6,450	65	0.43	6.38	12.46	218	36.1
	GP-10-01-059	5/27/2010	13:11	59	18.9	<1.13	5	NA	2,150	NA	12,100	170	0.23	6.25	11.68	307	15.5
	GP-10-01-069	5/27/2010	15:20	69	11.3	0.97 J	5	NA	4,600	NA	3,570	200	0.35	6.39	12.36	395	-40.6
	GP-10-01-075	5/27/2010	16:30	75	2.35	0.89 J	5	NA	6,380	NA	3,310	33	1.9	6.54	14.4	469	63.8
GP-10-02	GP-10-02-024	6/7/2010	9:50	24	0.41 J	0.37 J	<5	NA	1,130	NA	560	2.8	0.41	6.29	11.08	776	24.3
	GP-10-02-034	6/7/2010	10:42	34	0.67	0.33 J	<5	NA	1,560	NA	1,440	13.4	0.29	6.39	11.48	818	14.6
	GDUP-060710	6/7/2010	10:42	34	NA	<0.226	NA	NA	1,520	NA	1,380	See GP-10-02-034					
	GP-10-02-044	6/7/2010	11:35	44	1.64	0.74 J	<5	NA	2,140	NA	2,060	41.1	0.28	6.46	11.27	777	11.3
	GP-10-02-054	6/7/2010	12:27	54	2.43	0.41 J	<5	NA	2,150	NA	2,200	85.7	0.29	6.5	12.09	757	2.6
	GP-10-02-064	6/7/2010	13:08	64	5.87	0.41 J	<5	NA	3,500	NA	1,990	454	0.71	6.55	12.01	965	-14.7
	GP-10-02-074	6/7/2010	15:05	74	36.9	0.87 J	<5	NA	4,010	NA	2,910	Max	0.32	6.41	12.07	2550	-5.5
	GP-10-02-084	6/7/2010	18:12	84	24.8	4.64	<5	NA	19,600	NA	2,680	Max	0.31	6.57	12.39	2863	-60.8
	GP-10-02-094	6/8/2010	9:25	94	127	0.61 J	5	NA	4,040	NA	3,100	Max	1.15	5.70	12.54	2831	-97.9
	GP-10-02-102	6/8/2010	10:10	102	84.6	8.68	5	NA	25,300	NA	1,270	Max	0.42	6.26	14.33	2345	-169.9
GP-10-03	GP-10-03-029	6/10/2010	08:25	29	0.89	0.5	<5	NA	582	NA	71	3.2	7.03	6.07	10.01	799	79.5
	GP-10-03-039	6/10/2010	9:20	39	6.79	0.61 J	<5	NA	704	NA	59.8	58	2.63	6.3	10.27	1916	29.8
	GDUP-061010	6/10/2010	9:20	39	NA	<0.452	NA	NA	790	NA	68.4	See GP-10-03-039					
	GP-10-03-049	6/10/2010	10:00	49	14.6	<0.565	<5	NA	1,580	NA	62.9	404	2	6.85	10.36	2563	14.5
	GP-10-03-059	6/10/2010	10:40	59	42.1	0.92 J	<5	NA	5,210	NA	254	Max	0.86	6.53	10.68	3212	-40.4
	GP-10-03-069	6/10/2010	11:20	69	8.74	3.47	<5	NA	7,530	NA	633	68.9	0.52	6.72	10.79	3470	-78.6
	GDUP2-061010	6/10/2010	11:20	69	NA	3.85	NA	NA	8,210	NA	710	See GP-10-03-069					
GP-10-04	GP-10-04-014	6/8/2010	12:40	14	2.26	0.18 J	<5	NA	1170	NA	210	18.7	8.32	6.17	13.34	26	50.1
	GP-10-04-024	6/8/2010	14:00	24	2.19	0.18 J	<5	NA	256	NA	58.1	4.65	6.22	6.07	12.88	34	73.1
	GDUP-060810	6/8/2010	14:00	24	NA	0.16 J	NA	NA	199	NA	63	See GP-10-04-024					
	GP-10-04-034	6/8/2010	14:50	34	1.22	0.18 J	<5	NA	438	NA	84.4	42.1	3.47	5.73	11.22	44	58.5
	GP-10-04-044	6/8/2010	15:10	44	3.37	0.15 J	<5	NA	629	NA	86.6	29.3	1.52	5.13	11.57	224	114.4
	GP-10-04-054	6/8/2010	15:50	54	13.7	0.26 J	<5	NA	3,040	NA	811	784	0.42	5.4	11.29	644	21.9
	GP-10-04-064	6/8/2010	15:25	64	8.02	0.33 J	<5	NA	1,200	NA	510	245	0.57	5.4	11.58	856	30.8
	GP-10-04-074	6/8/2010	17:15	74	24.3	0.33 J	<5	NA	3,000	NA	433	Max	0.38	6.28	11.17	9.35	-91.6
	GP-10-04-084	6/8/2010	17:50	84	26.7	1.27	<5	NA	896	NA	91.4	Max	0.32	6.01	11.53	79.8	-40.7
GP-10-05	GP-10-05-015	6/9/2010	9:50	15	2.08	0.31 J	<5	NA	262	NA	483	1.08	0.74	6.32	12.82	109	102.9
	GP-10-05-025	6/9/2010	10:25	25	1.02 J	0.58 J	<5	NA	1150	NA	11,200	3.54	1.77	5.85	12.55	242	73
	GDUP-060910	6/9/2010	10:25	25	NA	<0.565	NA	NA	572	NA	11,200	See GP-10-05-025					
	GP-10-05-035	6/9/2010	10:53	35	130	112	150	NA	12,600	NA	4,610	17.8	1.45	6.21	13.25	214	-56
	GP-10-05-045	6/9/2010	11:24	45	86.4	84.7	80-100	NA	11,200	NA	2,320	36.9	2.24	6.17	2.76	255	-68

**TABLE 5**  
**Arsenic Comparison And Field Sampling Parameters**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Arsenic			Iron		Manganese		Turbidity NTU	DO mg/L	pH	Temp Celcius	Spec Cond uS/cm	ORP mV
					Total (ug/L)	Dissolved (ug/L)	Field Kit (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)						
GP-10-05A	GP-10-05A-029	6/9/2010	13:20	29	0.93	0.62 J	<5	NA	604	NA	63.8	1.52	992	6	16.24	1194	63.2
	GP-10-05A-039	6/9/2010	14:05	39	13	0.35 J	<5	NA	2,310	NA	221	57.7	2.79	5.22	14.72	209	110
	GDUP2-060910	6/9/2010	14:05	39	NA	0.33 J	NA	NA	2,510	NA	237			See GP-10-05A-039			
	GP-10-05A-049	6/9/2010	14:55	49	4.86	1.12	<5	NA	3,360	NA	203	39	4.87	5.81	14.29	172	76
	GP-10-05A-059	6/9/2010	15:57	59	3.48	0.39 J	<5	NA	1,840	NA	214	32.9	1.73	6.18	13.89	208	39
	GP-10-05A-069	6/9/2010	17:15	69	29.8	0.59	<5	NA	797	NA	466	Hand Pumped					
	GP-10-05A-079	6/9/2010	18:45	79	65	2.18	<5	NA	57.9	NA	114	No Readings, Silted up and Clogged Screen					
	GP-10-05A-089	6/9/2010	19:20	89	24.5	5.09	<5	NA	467	NA	70.3	No Readings, Silted up and Clogged Screen					
	GP-10-05A-099	6/9/2010	19:40	99	364	4.16	<5	NA	558	NA	294	No Readings, Silted up and Clogged Screen					
	GP-10-05A-109	6/9/2010	20:10	109	911	1.92	<5	NA	3,730	NA	1,320	No Readings, Silted up and Clogged Screen					
GP-10-06	GP-10-06-024	5/24/2010	11:50	24	17.2	10	10	NA	641	NA	112	50	0.19	5.57	9.16	26	127.5
	GP-10-06-034	5/24/2010	12:40	34	120	121	150-200	NA	14400 J	NA	763	31	0.39	2.99	12.66	103	-12.3
	GP-10-06-044	5/24/2010	13:35	44	155	129	100	NA	34,400	NA	982	800	0.19	5.65	15.69	194	4.9
	GP-10-06-054	5/26/2010	8:50	54	67.5	42.9	5	NA	75,400	NA	3,000	Max	0.19	6.04	12.89	880	-119.6
	GDUP-052610	5/26/2010	8:50	54	NA	49.1	NA	NA	82,000	NA	3,250			See GP-10-06-054			
	GP-10-06-064	5/26/2010	9:45	64	683	750	150	NA	122,000	NA	2,840	Max	0.14	6	11.63	827	-120
	GP-10-06-074	5/26/2010	11:15	74	2,390	2070	>500	NA	107,000	NA	2,470	Max	0.14	4.08	14.16	725	-124
	GP-10-06-079	5/26/2010	12:00	79	2,600	2540	500	NA	72,200	NA	3,490	Max	0.19	4.34	14.89	669	-109
GP-10-06A	GP-10-06A-034	5/24/2010	15:15	34	0.59	0.37 J	0	NA	66.4	NA	43.2	2.3	10.04	5.66	16.58	24	194.9
	GP-10-06A-044	5/24/2010	16:00	44	595	55.1	40	NA	9,710	NA	2,370	140	1.54	5.79	14.66	76	27
	GP-10-06A-054	5/24/2010	17:40	54	1090	18	10	NA	6,550	NA	6,920	900	1.47	5.8	14.1	166	8.1
	GP-10-06A-064	5/25/2010	9:50	64	170	36.7	20	NA	28,900	NA	2,780	Max	0.1	6.55	15.54	67	-134
	GDUP-052510	5/25/2010	9:50	64	NA	31.4	NA	NA	28,900	NA	2,830	See GP-10-06A-064					
	GP-10-06A-074	5/25/2010	11:10	74	134	58.6	30-40	NA	42,200	NA	2,460	Max	0.14	6.37	14.54	292	-115
	GP-10-06A-084	5/25/2010	13:00	84	186	106	60	NA	42,200	NA	3,050	Max	0.17	6.34	14.83	316	-115
	GP-10-06A-094	5/25/2010	14:40	94	382	< 1.13	5	NA	13,300	NA	17,900	Max	0.21	5.81	16.77	508	-119
	GP-10-06A-104	5/25/2010	16:30	104	405	< 1.13	0	NA	5,950	NA	6,530	900	0.17	6.24	17.17	608	-392
	GP-10-06A-110	5/25/2010	17:35	110	333	1.17 J	20	NA	8,640	NA	6,670	Max	0.11	6.14	14.66	603	-352
GP-10-07	GP-10-07-039	5/19/2010	14:00	39	1,240	1350	>500	96,400	105,000	2,430	2,660	20	1.15	6.49	12.54	757	-69.6
	GP-10-07-049	5/20/2010	13:45	49	283	58	5-10	251000	27800 J	9140 J	5330 J	NA	0.3	7.31	1.32	637	-242.2
	GPDUP-052010	5/20/2010	13:45	49	304	58.2	5-10	276000	26,800	9200	5,250	See GP-10-07-049					
GP-10-08	GP-10-08-011	6/3/2010	12:10	11	2.08	0.64	<5	NA	581	NA	70.7	12.7	6.97	6.78	11.73	189	20.1
	GDUP-060310	6/3/2010	12:10	11	NA	0.67	NA	NA	565	NA	69.7	See GP-10-08-011					
	GP-10-08-021	6/3/2010	13:20	21	3.19	0.76	<5	NA	679	NA	199	17.5	4.68	6.5	10.46	337	31.4
	GP-10-08-031	6/3/2010	14:30	31	3.6	0.31 J	<5	NA	2,040	NA	2,340	44.4	0.31	6.43	12.57	660	-3.9
	GP-10-08-041	6/3/2010	15:00	41	3.77	0.85 J	<5	NA	2,090	NA	949	64.9	0.26	6.44	12.02	764	-8.6
	GP-10-08-051	6/3/2010	17:20	51	19.8	1.06	<5	NA	3,300	NA	777	321	0.24	6.56	11.6	9.64	-42
	GDUP2-060310	6/3/2010	17:20	51	NA	0.92 J	NA	NA	3,180	NA	769	See GP-10-08-051					
	GP-10-08-061	6/3/2010	18:05	61	2.07	0.73 J	<5	NA	4,710	NA	1,060	37.4	0.9	6.54	15	244	-4.3



**TABLE 5**  
**Arsenic Comparison And Field Sampling Parameters**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Arsenic			Iron		Manganese		Turbidity NTU	DO mg/L	pH	Temp Celcius	Spec Cond uS/cm	ORP mV
					Total (ug/L)	Dissolved (ug/L)	Field Kit (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)						
GP-10-09	GP-10-09-021	5/28/2010	9:15	21	0.45 J	0.27 J	<5	NA	88.3	NA	34.6	1.13	10.34	6.82	11.93	62	97.1
	GP-10-09-031	5/28/2010	10:00	31	183	0.15 J	<5	NA	685	NA	82.2	596	6.35	6.11	12.82	223	71.6
	GDUP-052810	5/28/2010	10:00	31	NA	0.17 J	NA	NA	778	NA	102			SS GP-10-09-031			
	GP-10-09-041	6/1/2010	11:30	41	12.6	0.25 J	<5	NA	853	NA	66	178	4.97	6.05	13.05	706	50.4
	GP-10-09-051	6/1/2010	13:00	51	13	0.27 J	<5	NA	1,760	NA	138	333	2.15	6.24	12.56	714	161
	GDUP-060110	6/1/2010	13:00	51	NA	0.23 J	NA	NA	1,580	NA	136			See GP-10-09-051			
	GP-10-09-061	6/1/2010	14:20	61	6.8	0.940	<5	NA	2,200	NA	362	87.1	1.04	6.62	13.19	401	-56.2
	GP-10-09-071	6/1/2010	16:45	71	23.3	0.680	<5	NA	2,070	NA	349	82.2	1.19	6.66	12.92	486	-58.6
	GP-10-09-081	6/1/2010	17:50	81	15.5	0.850	<5	NA	3,430	NA	382	93.2	1.18	6.66	13.3	428	-57.3
GP-10-10	GP-10-10-011	6/2/2010	14:45	11	0.34 J	0.27 J	<5	NA	332	NA	34.5	2.5	10.93	6.73	10.89	130	56.2
	GP-10-10-021	6/2/2010	16:00	21	1.59	0.27 J	<5	NA	728	NA	56.5	11.8	7.45	6.17	11.49	375	53.9
	GDUP-060210	6/2/2010	16:00	21	NA	0.22 J	NA	NA	732	NA	58.2			See GP-10-10-021			
	GP-10-10-031	6/2/2010	16:30	31	1.29 J	<0.565	<5	NA	818	NA	4,370	10.34	0.56	6.1	12.46	561	43.5
	GP-10-10-041	6/2/2010	17:15	41	1.86 J	1.13 J	<5	NA	2,720	NA	10,800	26.3	0.29	6.19	13.26	509	-2.8
	GP-10-10-051	6/2/2010	18:00	51	4.4 J	2.47 J	<5	NA	3,690	NA	14,300	26	0.26	6.32	12.59	594	-35.3
	GP-10-10-061	6/2/2010	19:00	61	11.1	<2.82	<5	NA	5,230	NA	30,700	90.6	0.32	6.34	12.02	87.6	-44.3
	GP-10-10-071	6/3/2010	10:00	71	13.7	<1.13	<5	NA	4,880	NA	15,500	121	0.36	6.41	12.72	737	-85
GP-10-11	GP-10-11-039	8/3/2010	14:10	39	263	264	80	67200	66400	2120	NA	14.5	0.11	5.61	16.26	302	56.2
	GP-10-11-049	8/3/2010	15:15	49	688	375	70	164000	49300	5240	NA	5373	0.27	6.2	18.09	278	-43.7
	DUP3-080310	8/3/2010	15:15	49	641	396	NA	149000	52200	5260	NA	NA	NA	NA	NA	NA	NA
	GP-10-11-059	8/3/2010	19:00	55	760	236	150	148000	28500	7700	5580	203	0.78	6.3	24.09	354	-46.3
	GP-10-11-064	8/4/2010	11:30	64	230	19.8	<5	180000	3440	7160	1100 J	Max	0.11	7.74	20.99	439	-150.4
GP-10-12	GP-10-12-044	8/5/2010	13:05	44	4320	3880	> 500	122000	83700	7180	5860	203	0.43	5.97	18.23	385	17.6
	GP-10-12-054	8/5/2010	15:00	54	NA	2850	> 500	NA	74800	NA	5200	Max	0.16	6.11	21.93	368	-17.1
	GP-10-12-065	8/9/2010	8:20	65	NA	38.9	30	NA	46600	NA	4400	Max	0.13	6.79	12.95	543	-103.3
GP-10-13	GP-10-13-039	8/9/2010	14:45	39	176	124	30	148000	99500	1950	1380	1409	0.18	5.36	21.58	740	101.2
	GP-10-13-049	8/9/2010	17:00	49	NA	12.2	<5	NA	7840	NA	6700	144	0.48	6.17	21.68	858	45.5
	GP-10-13-059	8/10/2010	9:05	59	120	102	100	87100	74500	682	592	565	0.16	6.4	18.34	800	-33.3
	GP-10-13-069	8/10/2010	11:15	69	NA	1060	> 500	NA	79800	NA	3630	151	0.81	6.09	21.32	545	-2.1
	GP-10-13-079	8/10/2010	13:10	79	NA	123	20	NA	5580	NA	218	128	8.68	6.37	21.89	338	15.9
GP-10-14	GP-10-14-039	8/16/2010	09:50	39	39.1	14.4	5	22800	18700	783	670 J	49.9	0.36	5.54	15.86	510	50.8
	GP-10-14-049	8/16/2010	11:20	49	774	772	250	66000	66900	2420	2540	22.5	0.41	5.86	15.99	474	14.9
	DUP-081610	8/16/2010	11:20	49	792	762	NA	69800	64200	2510	2440	NA	NA	NA	NA	NA	NA
	GP-10-14-059	8/16/2010	13:00	59	NA	2400	> 500	NA	88200	NA	6800	1129	0.17	5.86	16.31	553	-0.9
	GP-10-14-069	8/16/2010	14:35	69	5260	5110	> 500	95400	85400	3700	3540	111	0.18	5.82	17.71	444	-8.7
	GP-10-14-079	8/17/2010	07:45	79	17300	15100	> 500	80300	71800	5850	5540	38.8	0.31	6.18	14.71	395	34.2
GP-10-15	GP-10-15-039	8/11/2010	9:30	39	NA	1740	> 500	NA	101000	NA	3410	25.52	0.25	5.81	17.99	543	-6.4
	GP-10-15-049	8/11/2010	11:25	49	17200	16600	70	126000	119000	10500	10500	41.3	0.45	6	20.68	589	-40.5
	GP-10-15-059	8/11/2010	14:45	59	NA	278	80	NA	300	NA	466	207	5.11	8.3	21.89	313	181.1

**TABLE 5**  
**Arsenic Comparison And Field Sampling Parameters**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Arsenic			Iron		Manganese		Turbidity NTU	DO mg/L	pH	Temp Celcius	Spec Cond uS/cm	ORP mV
					Total (ug/L)	Dissolved (ug/L)	Field Kit (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)						
GP-10-16	GP-10-16-024	8/17/2010	16:15	24	170	4.81	5	56700	323	2500	182	1235	3.06	6.27	12.58	107	101.1
	DUP-081710	8/17/2010	16:15	24	164	3.87		59500	349	2650	197	NA	NA	NA	NA	NA	NA
	GP-10-16-034	8/18/2010	07:55	34	333 J	1.97	5	145000	138	5080	580	609	12.11	8.25	13.91	350	78.3
	GP-10-16-054	8/18/2010	11:20	54	19.9	1.89	< 5	8900	277	180	84	101.4	12.62	7.43	16.85	398	27.4
	Dup-081810	8/18/2010	11:20	54	26	2.05	NA	11400	300	200	86	NA	NA	NA	NA	NA	NA
	GP-10-16-064	8/18/2010	13:40	64	NA	445	100	NA	44700	NA	777	21.5	2.45	6.57	14.73	492	-78.8
	GP-10-16-074	8/19/2010	07:45	74	248 J	216 J	100	75900	64200	1420 J	1330 J	122	0.66	6.94	11.26	720	-140.3
	GP-10-16-084	8/19/2010	09:40	84	256	248	100	20600	17200	3120	2920	16.6	0.9	6.95	14.92	837	-104.8
	DUP-081910	8/19/2010	09:40	84	260	249	NA	21500	17400	3130	2990	NA	NA	NA	NA	NA	NA
	GP-10-16-094	8/19/2010	12:35	94	19.3	3.44	< 5	17500	625	620	368	180	5.06	6.9	17.45	382	-21.4
GP-10-17	GP-10-17-009	8/2/2010	11:40	9	0.58	0.46 J	< 5	1800 J	1620	NA	NA	20.1	4.91	1.65	14.07	1036	178.2
	GP-10-17-019	8/2/2010	12:20	19	0.78	0.39 J	< 5	1870	1800	NA	NA	NA	NA	NA	NA	NA	NA
	DUP-080210	8/2/2010	12:20	19	0.66	0.49 J	NA	1840	1870	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-17-029	8/2/2010	16:00	29	0.78	0.25 J	< 5	1810	1240	NA	NA	6.06	2.17	6.01	13.72	747	63.4
	GP-10-17-039	8/2/2010	16:45	39	1950	1860	500	65200	60700	NA	NA	37.9	0.26	6.83	13.9	542	-138.2
	GP-10-17-049	8/2/2010	17:30	49	17.7	20.8	5	10100	5210	NA	NA	65.6	1.4	6.52	14.8	670	-28.3
	GP-10-17-056	8/2/2010	17:45	56	26.4	5.38	5	30600	6100	NA	NA	660	0.24	6.73	14.68	666	-84.3
GP-10-18	GP-10-18-007	8/2/2010	18:34	7	0.93	0.73	NA	1390	1360	NA	NA	18.3	0.27	6.06	17.64	729	58.7
	GP-10-18-017	8/3/2010	8:25	17	1.87 J	1.26 J	< 5	1190	857	NA	NA	10.6	0.44	6.14	12.87	673	55.8
	GP-10-18-027	8/3/2010	9:00	27	117	107	80	35400	32000	NA	NA	199	0.44	6.3	13.55	681	-45.1
	DUP-080310	8/3/2010	9:00	27	118	107		34600	32800	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-18-037	8/3/2010	11:00	37	274	262	60	21300	18800	NA	NA	84.7	0.44	6.4	13.61	628	-45.5
	GP-10-18-047	8/3/2010	12:10	47	373	390	80	35200	32300	NA	NA	127	0.45	6.54	14.6	809	-80.7
GP-10-19	GP-10-19-009	8/3/2010	14:35	9	0.57	0.38 J	< 5	1040	908	NA	NA	1.1	3.55	5.85	17.73	174	98.5
	DUP2-080310	8/3/2010	14:35	9	0.53	0.35 J	NA	1030	982	NA	NA	NA	NA	NA	NA	NA	NA
	GP-10-19-019	8/3/2010	15:15	19	3.07	0.6	< 5	3680	831	NA	NA	141	2.19	6.01	14.88	759	904
	GP-10-19-029	8/3/2010	16:05	29	886	810	100	89800	73300	NA	NA	66.6	0.53	6.64	13.88	682	-111
	GP-10-19-039	8/3/2010	17:00	39	690	677	100	65600	58800	NA	NA	36.6	1.65	6.6	15.59	736	-77.7
	GP-10-19-046	8/3/2010	18:15	46	23.3	3.92	5	14400	4280	NA	NA	< 1000	1.88	6.50	14.58	737	-44.1
GP-10-20	GP-10-20-009	8/4/2010	9:30	9	1.6	0.4 J	< 5	2000	1260	NA	NA	12.5	6.46	6.22	16.7	262	60.4
	GP-10-20-019	8/4/2010	10:10	19	2.94	1.02	< 5	2910	1500	989	920	17.2	0.67	6.09	14.35	609	50.6
	DUP-080410	8/4/2010	10:10	19	3.11	0.066	NA	2630	1630	949	933	NA	NA	NA	NA	NA	NA
	GP-10-20-029	8/4/2010	11:00	29	220	235	40	53000	56800	NA	NA	139	0.33	6.7	13.44	521	-92.8
	GP-10-20-039	8/4/2010	13:00	39	446	429	50	16800	13300	NA	NA	91.6	0.37	6.49	13.51	649	-38.8



**TABLE 5**  
**Arsenic Comparison And Field Sampling Parameters**  
**Shepley's Hill Landfill, Devens, MA**

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Arsenic			Iron		Manganese		Turbidity NTU	DO mg/L	pH	Temp Celcius	Spec Cond uS/cm	ORP mV
					Total (ug/L)	Dissolved (ug/L)	Field Kit (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)						
GP-10-21	GP-10-21-011	8/4/2010	15:05	11	3.98	0.31 J	< 5	2550	501	NA	NA	54.1	6.33	6.14	15.57	182	101.5
	GP-10-21-021	8/4/2010	15:45	21	1.71	0.62 J	< 5	1730	984	1050	1020 J	134	1.43	6.07	14.29	728	97.5
	DUP2-080410	8/4/2010	15:45	21	1.48	0.63 J	NA	1550	1030	1020	1080	NA	NA	NA	NA	NA	NA
	GP-10-21-031	8/4/2010	16:30	31	5.05	3.64	< 5	3100	1840	NA	NA	34.7	1.54	6.35	13.78	503	44.9
	GP-10-21-041	8/4/2010	17:00	41	322	349	60	42500	43700	NA	NA	83.7	0.42	6.66	14.14	627	-80.2
	GP-10-21-051	8/4/2010	18:05	51	18.7	12.3	< 5	11900	6320	NA	NA	315	0.32	6.56	16.8	277	60.9
	GP-10-21-060	8/4/2010	19:00	60	145	146	40	21200	15300	NA	NA	<1000	0.72	6.68	16.59	828	-64.2
GP-10-22	GP-10-22-011	8/10/2010	14:40	11	0.51	0.37 J	< 5	844	753	NA	NA	6.27	7.43	5.92	14.7	306	115.8
	GP-10-22-021	8/10/2010	15:00	21	1.71	0.51	< 5	2310	1120	NA	NA	45	0.63	6.19	13.42	440	75.5
	GP-10-22-031	8/10/2010	15:50	31	2.65	0.75 J	< 5	3240	1780	NA	NA	54	0.72	6.22	13.22	766	68.1
	GP-10-22-041	8/10/2010	16:30	41	15.8	14.5	< 5	35300	36100	NA	NA	85.4	0.99	6.38	13.3	434	-32.9
	GP-10-22-051	8/10/2010	17:30	51	5.02	< 1.13	< 5	7580	5010	NA	NA	83.5	0.88	6.55	13.57	585	-20.9
	GP-10-22-061	8/10/2010	18:30	61	6.56	3.53	< 5	6750	4490	NA	NA	29.9	1.02	6.77	13.28	75	-51.1
GP-10-23	GP-10-23-017	8/5/2010	11:00	17	0.52	0.38 J	< 5	1110	1040	23	21.1	5.37	4.03	5.99	14.46	380	76.2
	DUP-080510	8/5/2010	11:00	17	1.45	1.4	NA	1180	1070	23.9	21.8	NA	NA	NA	NA	NA	NA
	GP-10-23-027	8/5/2010	11:45	27	2.86	0.6 J	5	2170	701	189	172	58.5	3.35	6.08	13.1	1060	94.3
	GP-10-23-037	8/5/2010	12:25	37	5.38	0.28 J	5	5400	1890	NA	NA	58.4	3.41	5.96	13.75	961	90.9
	GP-10-23-047	8/5/2010	14:20	47	610	666	> 500	78500	78400	NA	NA	374	1.34	6.6	15.76	490	-95.1
	GP-10-23-057	8/5/2010	16:05	57	1060	1070	500	72200	68400	3660	3730	254	0.86	6.65	14.51	743	-100.2
	DUP2-080510	8/5/2010	16:05		1160	1100	NA	82000	70000	4050	3820	NA	NA	NA	NA	NA	NA
GP-10-24	GP-10-24-015	8/9/2010	15:44	15	2.06	0.94 J	< 5	928	758	28.1	24.9	37.4	3.1	5.94	14.28	762	116.3
	DUP-080910	8/9/2010	15:44	15	1.52	0.8 J	NA	886	765	26.7	30.6	NA	NA	NA	NA	NA	NA
	GP-10-24-025	8/9/2010	16:30	25	1.61	0.39 J	< 5	2260	1180	NA	NA	44.9	5.21	6.05	13.23	710	104.8
	GP-10-24-035	8/9/2010	17:05	35	5.03	0.89 J	< 5	5550	2630	NA	NA	45.3	1.12	5.94	14.08	9.14	92.4
	GP-10-24-045	8/9/2010	17:45	45	303	310	125	99000	100000	NA	NA	98.6	1.07	6.54	13.61	1332	-71.5
	GP-10-24-055	8/9/2010	18:30	55	629	615	250	91160	81500	NA	NA	< 1000	0.77	6.61	13.41	914	-95.3
GP-10-25	GP-10-25-025	8/10/2010	10:00	25	44	0.4 J	< 5	35700	1770 J	NA	NA	889	3.57	6.03	13.07	506	69.3
	GP-10-25-035	8/10/2010	10:45	35	10.9	0.58 J	< 5	15660	2250	801	618	223	1.69	5.94	13.1	745	69.3
	DUP-081010	8/10/2010	10:45	35	10.9	1.18	NA	15360	2320	772	658	NA	NA	NA	NA	NA	NA
	GP-10-25-045	8/10/2010	11:50	45	37.3	35.1	5	76760	71000	4540	4550	137	1.13	6.56	12.86	6.22	-74.4
	DUP2-081010	8/10/2010	11:50	45	38	34.9	NA	76760	69000	4460	4430	NA	NA	NA	NA	NA	NA
GP-10-26	GP-10-26-011	8/11/2010	9:20	11	0.6	0.18 J	< 5	854	716 J	67.1	59.8	9.11	6.78	5.59	14.08	123	139.4
	GP-10-26-021	8/11/2010	10:20	21	2.07	0.39 J	< 5	2090	1170	129	103	33.7	3.01	6.05	12.5	275	84.4
	DUP-081110	8/11/2010	10:20	21	1.72	0.65	NA	1800	1140	120	103	NA	NA	NA	NA	NA	NA
	GP-10-26-031	8/11/2010	10:35	31	2.86	0.54	< 5	4180	1350	NA	NA	84.8	2.67	6.04	11.74	652	84.5
	GP-10-26-041	8/11/2010	11:05	41	4	0.45 J	< 5	6290	1940	NA	NA	207	0.72	6.05	12.11	631	61.5
	GP-10-26-051	8/11/2010	12:15	51	4.86 J	< 1.13	< 5	7180	3140	NA	NA	76.1	1.02	6.27	12.65	485	36.3
	GP-10-26-061	8/11/2010	13:40	61	6.48	< 1.13	< 5	11900	3840	NA	NA	376	1.49	6.45	12.74	741	-6.8
	GP-10-26-071	8/11/2010	14:10	71	3.58 J	1.96 J	< 5	6430	3310	NA	NA	< 1000	0.95	6.58	13.96	860	-36.1

TABLE 5  
Arsenic Comparison And Field Sampling Parameters  
Shepley's Hill Landfill, Devens, MA

Boring Location	Sample ID	Date	Time (Military Format)	Depth	Arsenic			Iron		Manganese		Turbidity NTU	DO mg/L	pH	Temp Celcius	Spec Cond uS/cm	ORP mV
					Total (ug/L)	Dissolved (ug/L)	Field Kit (ug/L)	Total (ug/L)	Dissolved (ug/L)	Total (ug/L)	Dissolved (ug/L)						
GP-10-27	GP-10-27-025	8/11/2010	16:05	25	2.77	1.03	< 5	1640	773	56.2	44.9	21.6	1.33	6.46	14.8	332	47.7
	DUP2-081110	8/11/2010	16:05	25	1.11	0.38 J	NA	1510	804	53	45.5	NA	NA	NA	NA	NA	NA
	GP-10-27-035	8/11/2010	17:00	35	24.7	0.78 J	< 5	15000	1100	NA	NA	101.1	1.07	5.87	13.44	1022	76.8
	GP-10-27-045	8/11/2010	17:25	45	199	200	70	88800	83800	NA	NA	339	0.71	6.58	13.58	647	-93.6
	GP-10-27-055	8/11/2010	17:50	55	288	328	70	84100	91300	NA	NA	294	0.95	6.65	13.28	644	-108.8
	GP-10-27-065	8/11/2010	18:45	65	1100	1040	> 500	73400	61300	NA	NA	<1000	1.1	6.66	13.37	766	-93.3

Notes

NA - Not Applicable  
ug/L is micrograms per liter.  
mg/l - miligrams per liter  
J means estimated results  
B indicates that analyte was detected in the associated method blank

DO - Dissolved Oxygen  
ORP - Oxygen Reduction Potential



Table 6  
 Water Level Calibration Targets and Residuals  
 Shepley's Hill Landfill  
 Focused Feasibility Study  
 Supplemental Hydrogeologic Assessment

Monitoring Well	Layer	Observed Groundwater Elevation	Computed Groundwater Elevation	Residual
N-3 P-1	3	217.29	217.44	-0.15
N-3 P-2	1	216.67	217.34	-0.67
N-5 P-2	1	220.49	218.91	1.58
N-6 P-1	3	223.42	222.60	0.82
N-7 P-1	3	226.71	226.06	0.65
N-7 P-2	1	227.04	226.00	1.04
SHL-10	1	218.87	218.81	0.06
SHL-11	1	218.14	218.51	-0.37
SHL-13	1	215.37	215.07	0.30
SHL-15	2	243.55	242.52	1.03
SHL-19	1	219.05	219.11	-0.06
SHL-20	1	218.26	218.38	-0.12
SHL-21	1	215.37	215.75	-0.38
SHL-22	3	214.28	214.39	-0.11
SHL-23	3	215.58	215.73	-0.15
SHL-24	3	225.02	224.27	0.75
SHL-3	1	218.65	219.69	-1.04
SHL-4	1	217.99	218.79	-0.80
SHL-5	1	215.54	214.61	0.93
SHL-8D	2	214.84	214.70	0.14
SHL-8S	2	214.91	214.66	0.25
SHL-9	1	214.47	214.48	-0.01
SHM-05-39A	1	211.84	212.35	-0.51
SHM-05-39B	2	210.65	212.40	-1.75
SHM-05-40X	1	211.03	212.16	-1.13
SHM-05-41A	1	213.93	213.63	0.30
SHM-05-41B	3	213.91	213.63	0.28
SHM-05-41C	3	214.00	213.68	0.32
SHM-05-42A	1	213.66	213.44	0.22
SHM-05-42B	2	213.69	213.46	0.23
SHM-93-10C	3	219.51	218.77	0.74
SHM-93-18B	2	220.03	220.83	-0.80
SHM-93-22C	3	214.35	214.40	-0.05
SHM-96-22B	2	213.96	214.36	-0.40
SHM-96-5B	2	214.88	214.60	0.28
SHM-96-5C	2	214.57	214.64	-0.07
SHM-99-31A	1	213.00	212.50	0.50
SHM-99-31B	2	212.23	212.51	-0.28
SHM-99-31C	2	212.26	212.51	-0.25
SHM-99-32X	2	212.90	212.76	0.14
SHP-01-36X	1	217.75	216.85	0.90
SHP-01-37X	1	217.17	217.24	-0.07
SHP-01-38A	1	217.95	218.50	0.55
SHP-01-38B	2	218.09	218.44	-0.35
SHP-05-43	1	217.11	216.36	0.75
SHP-05-44	1	217.40	217.17	0.23
SHP-05-45A	1	214.62	215.34	-0.72
SHP-05-45B	2	214.66	215.29	-0.63
SHP-05-46A	1	215.23	215.40	-0.17
SHP-05-46B	2	214.62	215.36	-0.74
SHP-99-34A	1	213.27	212.96	0.31
SHP-99-34B	2	213.04	213.06	-0.02
SHP-99-35X	3	222.47	223.13	-0.66
SHP-07-03C	1	205.85	207.58	-1.73
SHP-07-03E	1	205.28	207.37	-2.09
SHP-07-03B	1	205.83	207.39	-1.56
SHP-07-01BS	1	210.24	208.97	1.27
SHP-07-01BD	1	207.74	208.97	-1.23
SHP-07-01CS	1	208.52	208.64	-0.12
SHP-07-01CD	1	207.73	208.64	-0.91
SHP-07-01DS	1	206.73	208.31	-1.58
SHP-07-01DD	1	206.75	208.31	-1.56
SHP-07-01 22-27	1	206.71	208.33	-1.62
SHP-07-01 15-20	1	206.80	208.35	-1.55
SHW-07-05	3	209.88	212.14	-2.26
SHW-07-03	1	208.72	211.43	-2.71
RSK12	1	218.35	219.19	-0.84
RSK15	1	218.27	218.63	-0.36
RSK19	1	217.84	218.20	-0.36
RSK24	1	219.29	219.58	-0.29
RSK25	1	218.80	219.03	-0.23
RSK26	1	218.69	219.39	-0.70
RSK27	1	218.80	219.26	-0.46
RSK28	1	218.60	218.99	-0.39
RSK29	1	218.40	218.89	-0.49
RSK30	1	218.18	218.69	-0.51
RSK33	1	217.89	218.13	-0.24
RSK34	1	217.89	217.91	-0.02
RSK35	1	217.67	217.76	-0.09
RSK37	1	217.66	217.44	0.22
RSK48	1	217.84	219.19	-1.35
RSK49	1	218.02	218.41	-0.39
RSK7	1	217.62	217.58	0.04
Residual Mean				-0.29
Res. Std. Dev.				0.81
Sum of Squares				61.29
Abs. Res. Mean				0.64
Min. Residual				-2.71
Max. Residual				1.58
Range				38.27
Std/Range				0.02

**Table 7**  
**Waste Occurrence in Shepley's Hill Landfill Borings**

Boring	Waste	Compound and Concentrations (mg/kg)													
		Arsenic		Cadmium		Copper		Chromium		Nickel		Lead		Zinc	
		High	Low	High	Low	High	Low	High	Low	High	Low	High	Low	High	Low
SHM-10-11	Paper/plastic/ash/wood (5 to 23 ft bgs)	13	10	220	0.05	33	7.3	42	9.1	16	6	110	10	66	18
SHM-10-12	Ash and sand mixed w/ash 5 to 9 ft bgs	13	12	< 0.04	< 0.03	260	7.3	18	9.8	72	9.3	510	8.5	210	16
SHM-10-13	Ash and Sand 23 to 27 ft bgs	31	7	3.5	< 0.04	33	5.3	52	3.9	15	5.5	53	5.3	13,000	20
SHM-10-13	Peat 27 to 35 ft bgs	7	0.8	< 0.03		71	0.8	48	4.6	23	4	13	2.5	34	9.5
SHM-10-14	Waste (paper/minor ash) and waste sand mix 10 to 23 ft bgs	18	6	< 0.04		18	5.9	26	6.8	23	8.8	180	6.6	160	36
SHM-10-14	Peat and sand/peat 30 to 44 ft bgs	60	2.8	< 0.04		7.3	4.5	8.4	4.8	15	4.2	6.6	1.6	27	12
SHM-10-15	Waste (ash/paper/plastic /wood) 5 to 28 ft bgs	25	6.2	0.27	0.04	310	3.7	69	8.4	75	6.3	1,200	5.3	1,000	11

Note: The values in yellow represent enrichment with respect to normal soil ranges  
mg/kg - means milligrams per kilogram  
bgs - below ground surface  
ft - feet



## **ATTACHMENTS**

## ATTACHMENTS




## **Attachment A**

## Attachment A









Sovereign Consulting Inc. 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: SHM-10-01		Sheet 1 of 3		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spinn Type: 3.25" Size: 60" Hammer: Fall NA lbs		
Start Date: 6/15/2010 Completion Date: 6/16/2010							Casing Elevation: 209.88 - NGVD 29' Surface Elevation: 206.3 +/- NGVD 29' Wellhead Type: Standpipe				
Sample Information							Stratum		Test Boring/ Monitoring Well		
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Change (ft.)	Notes	
0	S-1	60/40	0-5	NA	NA			Topsoil (21-inches)	TOPSOIL		
2								Light brown, dry to wet, MEDIUM TO COARSE SAND (well sorted)			
4											
6	S-2	60/26	5-10	NA	NA			Grey, saturated, FINE TO MEDIUM SAND.	SAND		
8								Orange, COARSE SAND, some (angular) gravel			
10								As Field Testing Results			
12	S-3	60/22	10-15	NA	NA			Light brown, saturated, COARSE SAND to FINE TO MEDIUM SAND (gradational layering, well sorted)			
14											
16	S-4	60/29	15-20	NA	NA			Light brown, saturated, COARSE SAND to FINE TO MEDIUM SAND (gradational layering, well sorted)	SAND		
18											
20								As Field Testing Results			
22	S-5	60/28	20-25	NA	NA			Brown, saturated, COARSE SAND, some (angular) gravel	SAND & GRAVEL		
24											
Notes: 1) Direct Push groundwater profile sampling conducted on 5/27/10. 2) Groundwater profile sampler refusal @ 75' 3) 4) 5) 6)							Key				
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L, collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA=Not Applicable. NR=No Recovery. bus=below ground surface. ays=above ground surface.											

 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-01</b>		Sheet 3 of 3		
Client: USACE Project: SHM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610D1 Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Type: Steel Size: 3.25" Hammer: Fall NA lbs		
<b>Sample Information</b> Start Date: 6/15/2010 Completion Date: 6/16/2010							Casing Elevation: 209.88 - NGVD 29' Surface Elevation: 206.3 +/- NGVD 29' Wellhead Type: Standpipe				
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/g"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
52	S-11	60/34	50-55	NA	NA			Brown, saturated, COARSE SAND, some (rounded) gravel	SAND & GRAVEL		1.5" Schedule 40 PVC Riser 0-60.5'
54											Gaug 2'-55.5'
56	S-12	60/32	55-60	NA	NA			Brown, saturated, COARSE SAND, some medium sand, trace fine sand and silt	SAND		Bentonite 55.5'-57.5'
58											
60					5			As Field Testing Results			
62	S-13	60/34	60-65	NA	NA			Light brown, saturated, MEDIUM TO COARSE SAND, with layers of fine sand and silt			
64											
66	S-14	60/28	65-70	NA	NA			Light brown, saturated, FINE TO MEDIUM SAND, some gravel, dense (fill)	GLACIAL TILL		1.5" Schedule 40 PVC Well screen - 0.01" slot 60.5'-70.5'
68											
70					5			As Field Testing Results			
72								Limited recovery SAND & GRAVEL, dense, rock in tip of sampling spoon (fill)			
74								SAMPLER REFUSAL 66-70.5'			CASING REFUSAL 66-70.5'
					5			As Field Testing Results			

**Notes**


- 1) Direct Push groundwater profile sampling conducted on 5/27/10
- 2) Groundwater profile sampler refusal at 75'
- 3)
- 4)
- 5)
- 6)

**Key**

-  Cement
-  Drill Cuttings Native Soils
-  Bentonite Grout
-  Sand
-  Screen
-  Riser

**Remarks:**

- 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made
- 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data
- 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample

 = Approximate water table   
 NA = Not Applicable   
 NR = No Recovery   
 bgs = below ground surface   
 ags = above ground surface



Sovereign Consulting Inc. 905B South Main Street Mansfield, Massachusetts		Boring/Well ID: SHM-10-02		Sheet 2 of 4				
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman Start Date: 6/30/2010 Completion Date: 7/1/2010		Casing: Sampler Type: Steel Geoprobe Spoon Size: 3.25" 60" Hammer: Fall NA lbs NA"				
Sample Information		Stratum		Notes				
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing			
					Sample Type			
					Water Detected			
Sample Description		Change (ft.)		Test Boring/ Monitoring Well Construction				
26	S-6	60/26	25-30	NA	NA	Gray, saturated, FINE SAND, some medium to coarse sand, little (angular) rock fragments. (gradational layering of sands with depth)	SAND	1.5" Schedule 40 PVC Rise 0.53'
28								
30	S-7	60/22	30-35	NA	NA	Gray, saturated, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand		
32								
34					<5	As Field Testing Results		
36	S-8	60/21	35-40	NA	NA	Gray, saturated, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand		
38								
40	S-9	60/22	40-45	NA	NA	Gray, saturated, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand		
42								
44					<5	As Field Testing Results		
46	S-10	60/29	45-50	NA	NA	Gray, saturated, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand	SAND	Ground 2'-48"
48								
50								
Notes		1) Direct Push groundwater profile sampling conducted on 6/7/10 & 6/8/10 2) Groundwater profile sampler refusal @ 102' As = 5 g/L, at 102' 3) 4) 5) 6)		Key				
Remarks		1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA=Not Applicable. NR=No Recovery. bgs= below ground surface. ags= above ground surface.		<div><div><div></div>Concrete</div><div><div></div>Drill Cuttings Native Soils</div><div><div></div>Bentonite Grout</div><div><div></div>Sand</div><div><div></div>Screen</div><div><div></div>Rise</div></div> <div><div></div>Grout 4" x 48"</div>				

**Table 7**  
**Waste Occurrence in Shepley's Hill Landfill Borings**

Boring	Waste	Compound and Concentrations (mg/kg)													
		Arsenic		Cadmium		Copper		Chromium		Nickel		Lead		Zinc	
		High	Low	High	Low	High	Low	High	Low	High	Low	High	Low	High	Low
SHM-10-11	Paper/plastic/ash/wood (5 to 23 ft bgs)	12	6	220	0.04	33	7	42	6	16	6	110	6	48	13
SHM-10-12	Ash and sand mixed w/ ash 5 to 9 ft bgs	13	12	0.03	0.02	260	7	18	9.8	72	9.3	510	8.5	210	16
SHM-10-13	Ash and Sand 23 to 27 ft bgs	31	7	3.5	0.03	33	5.3	52	4	15	5.5	53	5.3	13,000	20
SHM-10-13	Peat 27 to 35 ft bgs	5.9	0.8	< 0.03		71	0.8	48	4.6	23	4	13	2.5	34	9.5
SHM-10-14	Waste (paper/minor ash) and waste sand mix 10 to 23 ft bgs	18	3.8	< 0.04		11	5.9	16	6.8	23	8.5	180	6.6	160	36
SHM-10-14	Peat and sand/peat 30 to 44 ft bgs	60	2.8	< 0.04		7.3	4.6	8.4	5.9	15	4.2	6.6	1.6	27	11
SHM-10-15	Waste (ash/paper/plastic /wood) 5 to 28 ft bgs	25	6.2	0.26	0.04	310	3.7	69	10	75	6.3	1,200	12	1,000	53

Note: The values in yellow represent enrichment with respect to normal soil ranges  
mg/kg - means milligrams per kilogram  
bgs - below ground surface  
ft - feet




## ATTACHMENTS

## Attachment A





 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-01</b>		Sheet 1 of 3		
Client: USACE Project: SHM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spoon Size: 3.25" Hammer: Fall NA lbs: NA"		
<b>Sample Information</b> Start Date: 6/15/2010 Completion Date: 6/16/2010							Casing Elevation: 209.88 - NGVD 29' Surface Elevation: 206.3+/- NGVD 29' Wellhead Type: Standpipe				
Depth	Sample ID	Pen/Rec. (in.)	Interval (Ft.)	Blow/g"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
2	S-1	60/40	0-5	NA	NA			Topsoil (21-inches) Light brown, dry to wet, MEDIUM TO COARSE SAND (well sorted)	TOPSOIL		Standpipe is 3' a/s
4											
6	S-2	60/26	5-10	NA	NA			Grey, saturated, FINE TO MEDIUM SAND Orange, COARSE SAND, some (angular) gravel	SAND		Cement 0-2'
8											
10					<5			As Field Testing Results			
12	S-3	60/22	10-15	NA	NA			Light brown, saturated, COARSE SAND to FINE TO MEDIUM SAND (gradational layering, well sorted)			
14											
16	S-4	60/20	15-20	NA	NA			Light brown, saturated, COARSE SAND to FINE TO MEDIUM SAND (gradational layering, well sorted)	SAND		
18											
20					<5			As Field Testing Results			
22	S-5	60/28	20-25	NA	NA			Brown, saturated, COARSE SAND, some (angular) gravel			
24									SAND & GRAVEL		Grout 2'-5.5'

**Notes:**







- 1) Direct Push groundwater profile sampling conducted on 5/27/10.
- 2) Groundwater profile sample refusal @ 75'
- 3)
- 4)
- 5)
- 6)

**Remarks:**








- 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.
- 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data.
- 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample.


▽ = Approximate water table    NA = Not Applicable    NR = No Recovery    bgs = below ground surface    a/s = above ground surface

**Key:**

-  Cement
-  Drill Cuttings Native Soils
-  Bestonite Grout
-  Sand
-  Screen
-  Riser









<div> Sovereign Consulting Inc.</div> <div>905B South Main Street Mansfield, Massachusetts</div>							Boring/Well ID: SHM-10-01			Sheet 2 of 3																																																																																																																									
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman			Casing: Steel Type: Steel Size: 3.25" Hammer: Fall NA lbs Sampler: Geoprobe Spoon 60" NA"																																																																																																																									
<table><tr><th colspan="7">Sample Information</th></tr><tr><th>Depth</th><th>Sample ID</th><th>Pen./Rec. (in.)</th><th>Interval (ft.)</th><th>Blow/6"</th><th>Field As Testing</th><th>Sample Type</th><th>Water Detected</th></tr><tr><td>26</td><td>S-6</td><td>60/26</td><td>25-30</td><td>NA</td><td>NA</td><td></td><td></td></tr><tr><td>28</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>30</td><td></td><td></td><td></td><td></td><td>5</td><td></td><td></td></tr><tr><td>32</td><td>S-7</td><td>60/22</td><td>30-35</td><td>NA</td><td>NA</td><td></td><td></td></tr><tr><td>34</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>36</td><td>S-8</td><td>60/21</td><td>35-40</td><td>NA</td><td>NA</td><td></td><td></td></tr><tr><td>38</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>40</td><td></td><td></td><td></td><td></td><td>5</td><td></td><td></td></tr><tr><td>42</td><td>S-9</td><td>60/22</td><td>40-45</td><td>NA</td><td>NA</td><td></td><td></td></tr><tr><td>44</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>46</td><td>S-10</td><td>60/20</td><td>45-50</td><td>NA</td><td>NA</td><td></td><td></td></tr><tr><td>48</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>50</td><td></td><td></td><td></td><td></td><td>5</td><td></td><td></td></tr></table>							Sample Information							Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	26	S-6	60/26	25-30	NA	NA			28								30					5			32	S-7	60/22	30-35	NA	NA			34								36	S-8	60/21	35-40	NA	NA			38								40					5			42	S-9	60/22	40-45	NA	NA			44								46	S-10	60/20	45-50	NA	NA			48								50					5			Start Date: 6/15/2010 Completion Date: 6/16/2010			Casing Elevation: 209.88 - NGVD 29' Surface Elevation: 206.3+/- NGVD 29' Wellhead Type: Standpipe		
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							Stratum Change (ft.)		Notes	Test Boring/ Monitoring Well Construction																																																																																																																									
							Brown, saturated, COARSE SAND		SAND & GRAVEL																																																																																																																										
							As Field Testing Results																																																																																																																												
							Brown, saturated, COARSE SAND, some (rounded) gravel																																																																																																																												
							Brown, saturated, COARSE SAND, some (rounded) gravel		SAND & GRAVEL	1" Schedule 40 PVC Bore																																																																																																																									
							As Field Testing Results																																																																																																																												
							Brown, saturated, COARSE SAND, some (rounded) gravel																																																																																																																												
							Brown, saturated, COARSE SAND, some (rounded) gravel		SAND & GRAVEL	Grout 2'-55.5'																																																																																																																									
							As Field Testing Results																																																																																																																												
							Brown, saturated, COARSE SAND, some (rounded) gravel																																																																																																																												
Notes: 1) Direct Push groundwater profile sampling conducted on 5/27/10. 2) Groundwater profile sampler refusal at 75'. 3) 4) 5) 6)									Key	<div> Cement</div> <div> Drill Cuttings Native Soils</div> <div> Bentonite Grout</div> <div> Sand</div> <div> Screen</div> <div> Riser</div>																																																																																																																									
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA: Not Applicable. NR: No Recovery. bgs: below ground surface. ags: above ground surface.																																																																																																																																			

 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-01</b>		Sheet 3 of 3		
Client: USACE Project: SHI, - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spoon Size: 3.25" / 60" Hammer: Fall N/A lbs. / N/A"		
<b>Sample Information</b> Start Date: 6/15/2010 Completion Date: 6/16/2010							Casing Elevation: 209.88 - NGVD 29' Surface Elevation: 206.3 +/- NGVD 29' Wellhead Type: Standpipe				
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
52	S-11	60/34	50-55	NA	NA			Brown, saturated, COARSE SAND, some (rounded) gravel	SAND & GRAVEL		1 5" Schedule 40 PVC Riser 0-60.5'
54											Grout 2'-55.5'
56	S-12	60/32	55-60	NA	NA			Brown, saturated, COARSE SAND, some medium sand, trace fine sand and silt.	SAND		Bentonite 55.5'-57.5'
58											
60					5			As Field Testing Results			
62	S-13	60/31	60-65	NA	NA			Light brown, saturated, MEDIUM TO COARSE SAND, with layers of fine sand and silt.			
64											
66	S-14	60/28	65-70	NA	NA			Light brown, saturated, FINE TO MEDIUM SAND, some gravel, dense (fill)	GLACIAL FILL		1 5" Schedule 40 PVC Well screen - 0.01" slot 60.5'-70.5'
68											
70					5			As Field Testing Results			
72								Limited recovery. SAND & GRAVEL, dense, rock in tip of sampling spoon (fill)			
74								SAMPLER REFUSAL @ 70.5'			CASING REFUSAL @ 70.5'
					5			As Field Testing Results			

**Notes:**


- 1) Direct Push groundwater profile sampling conducted on 5/27/10
- 2) Groundwater profile sampler refusal at 75'
- 3)
- 4)
- 5)
- 6)

**Key**








-  Cement
-  Drill Cuttings Native Soils
-  Bentonite Grout
-  Sand
-  Screen
-  Riser



**Remarks:**

- 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.
- 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data.
- 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample.



 = Approximate water table   
 NA=Not Applicable   
 NR=No Recovery   
 bgs=below ground surface   
 ags=above ground surface


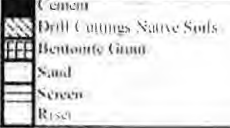


 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-02</b>			Sheet 1 of 4		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman			Casing: Steel Sampler: Geoprobe Spoon Type: 3.25" Size: 60" Hammer: Fall NA lbs. NA"		
<b>Sample Information</b> Start Date: 6/30/2010 Completion Date: 7/1/2010							Casing Elevation: 222.86 - NGVD 29' Surface Elevation: 220.0 +/- NGVD 29' Wellhead Type: Standpipe					
Depth	Sample Information						Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction		
	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type				Water Detected		
2	S-1	60/19	0-5	NA	NA		Topsoil (4-inches)	TOPSOIL			Standpipe is 3' ags	
							Brown, dry, FINE TO MEDIUM SAND, little (angular) rock fragments				Cement 0-2'	
4												
6	S-2	60/12	5-10	NA	NA		Brown, dry, FINE TO MEDIUM SAND, little (angular) rock fragments	SAND				
8												
10												
12	S-3	60/4	10-15	NA	NA		Brown, dry, FINE TO MEDIUM SAND, little (angular) rock fragments					
14												
16	S-4	60/56	15-20	NA	NA		10"-15" Brown, dry, MEDIUM SAND, some (angular) gravel, trace fine sand	SAND				
18							15"-18" Light Brown, dry, FINE SAND, trace silt					
							18"-49" Brown, moist, FINE SAND AND SILT	FINE SAND & SILT				
20							49"-56" Grey, saturated, SILT, trace Clay					
22	S-5	60/2	20-25	NA	NA		Light brown, saturated, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand	SAND			Cement 2'-48"	
24							As Field Testing Results					
Notes: 1) Direct Push groundwater profile sampling conducted on 6/7/10 & 6/8/10 2) Groundwater profile sampler refusal at 102" As - 5 ug/L at 102" 3) 4) 5) 6)							Key:  Cement  Drill Cuttings Native Soils  Bentonite Grout  Sand  Screen  Riser					
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▼ = Approximate water table. NA = Not Applicable. NR = No Recovery. lbs = below ground surface, ags = above ground surface.												

 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts		Boring/Well ID: <b>SHM-10-02</b>		Sheet 2 of 4								
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Geosarch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCL Inspector: Danielle Eastman		Casing Type: Steel Sampler Size: 3.25" Hammer: Fall NA lbs: NA"								
		Start Date: 6/30/2010 Completion Date: 7/1/2010		Casing Elevation: 222.86 - NGVD 29' Surface Elevation: 220.0 +/- NGVD 29' Wellhead Type: Standpipe								
Depth	Sample Information					Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction	
	Sample ID	Pen/Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing							
26	S-6	60/26	25-30	NA	NA			Gray, saturated, FINE SAND, some medium to coarse sand, little (angular) rock fragments (gradational layering of sands with depth)	SAND	1	1.5" Schedule 40 PVC Riser 0-53'	
28												
30												
32	S-7	60/22	30-35	NA	NA			Gray, saturated, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand				
34								As Field Testing Results				
36	S-8	60/21	35-40	NA	NA			Gray, saturated, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand				
38												
40												
42	S-9	60/22	40-45	NA	NA			Gray, saturated, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand				
44								As Field Testing Results				
46	S-10	60/24	45-50	NA	NA			Gray, saturated, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand	SAND	1	Ground 2'-48"  Borehole 48'-50'	
48												
50												
<b>Notes:</b> 1) Direct Push groundwater profile sampling conducted on 6-7-10 & 6-8-10 2) Groundwater profile sampler refusal @ 102' As - 5 ug/l; @ 102' 3) 4) 5) 6)											<b>Key:</b> 	
<b>Remarks:</b> 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l, collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA Not Applicable. NR No Recovery. lbs: below ground surface. ags: above ground surface.												




 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-02</b>		Sheet 3 of 4			
Client: USACE Project: SHM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spoon Type: Steel Size: 3.25" Hammer: Fall NA lbs: N/A			
<b>Sample Information</b>							Start Date: 6/30/2010 Completion Date: 7/1/2010		Casing Elevation: 222.86 - NGVD 29' Surface Elevation: 220.0 +/- NGVD 29' Wellhead Type: Standpipe			
Depth	Sample ID	Pen/Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction	
52	S-11	60-12	50-55	NA	NA			Gray, saturated, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand			#2 Marie Sand 50'-63'	
54								As Field Testing Results				
56	S-12	60-23	55-60	NA	NA			Gray, saturated, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand	SAND		1.5" Schedule 40 PVC Well screen - 0.01" slot 53'-63'	
58								Bottom - Light brown to gray, saturated, FINE SAND				
60												
62	S-13	60-26	60-65	NA	NA			Light brown to gray, Wet, MEDIUM TO COARSE SAND, some (angular) gravel, trace fine sand				
64								As Field Testing Results				
66	S-14	60-27	65-70	NA	NA			Light brown to gray, saturated, FINE SAND, some medium sand, trace coarse sand	SAND		CASING REFUSAL @ 65'	
68												
70												
72	S-15	60-42	60-73	NA	NA			Light brown, saturated, FINE SAND, trace medium sand and silt	SAND			
74								As Field Testing Results				
Notes: 1) Direct Push groundwater profile sampling conducted on 6/7/10 & 6/8/10 2) Groundwater profile sampler refusal @ 102' AS - 50 ft @ 102' 3) 4) 5) 6)											Key: 	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA=Not Applicable NR=No Recovery. bgs=below ground surface ags=above ground surface												

 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-02</b>		Sheet 4 of 4		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spoon Size: 1.25" Hammer: Fall NA lbs: NA"		
<b>Sample Information</b>							Start Date: 6/30/2010 Completion Date: 7/1/2010		Casing Elevation: 222.86 - NGVD 29' Surface Elevation: 220.0+/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
76	S-16	36/13	75-78	NA	NA			Light brown, saturated, FINE SAND, trace medium sand and silt	SAND		
78								Grey, moist, FINE SAND, (angular) rock fragments, rock in tip of spoon			
								SAMPLER REFUSAL @ 78'			
80											
82											
84								As Field Testing Results			
86											
88											
90											
92											
94								As Field Testing Results			
96											
98											
100											
Notes: 1) Direct Push groundwater profile sampling conducted on 6/7/10 & 6/8/10 2) Groundwater profile sampler refusal @ 102' As 5 ug/L @ 102' 3) 4) 5) 6)										Key: 	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▽ = Approximate water table. NA=Not Applicable. NR=No Recovery. bgs=below ground surface. ags=above ground surface.											



Sovereign Consulting Inc. 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: SHM-10-03		Sheet 1 of 3			
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman			Casing: Steel Type: Steel Size: 3.25" Hammer NA lbs Sampler: Geoprobe Spudr 60" Fall NA"		
Sample Information							Start Date: 6/23/2010 Completion Date: 6/23/2010			Casing Elevation: 231.88 - NGVD 29' Surface Elevation: 229.6 +/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction	
0	S-1	60-32	0-5	NA	NA			Topsoil	TOPSOIL		Standpipe is 3' ags	
2								Brown, dry, MEDIUM TO COARSE SAND, some gravel.			Cement 0-2'	
4												
6	S-2	60-25	5-10	NA	NA			Light brown, dry, MEDIUM TO COARSE SAND, some Gravel (large angular rock fragments in spoon)	SAND			
8												
10												
12	S-3	60-60	10-15	NA	NA			Light brown, dry, MEDIUM TO COARSE SAND, some (sub-angular) gravel, trace fine sand, (gradational) layering, large angular rock fragments)	SAND			
14												
16	S-4	60-60	15-20	NA	NA			9"-24" Brown, moist, MEDIUM SAND, trace coarse sand, with (sub-rounded) gravel.				
18								22"-60" Brown, moist, COARSE SAND, and (sub-angular) gravel.	SAND			
20												
22	S-5	60-28	20-25	NA	NA			Brown, wet, COARSE SAND, some (sub-angular) gravel.			Grout 2'-5.5'	
24												
Notes: 1) Direct Push groundwater profile sampling conducted on 6-10-10. 2) Groundwater profile sampler refusal at 70' 3) 4) 5) 6)										Key	Cement Drill Cuttings Native Soils Bentonite Grout Sand Screen Riser	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in mg/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table: NA: Not Applicable NR: No Recovery - logs below ground surface, ags: above ground surface												

<div> Sovereign Consulting Inc.</div> <div>905B South Main Street Mansfield, Massachusetts</div>							Boring/Well ID: SHM-10-03			Sheet 2 of 3			
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DJT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman			Casing: Steel Sampler: Geoprobe Spoon Type: 3.25" Size: 60" Hammer: Fall NA lbs: NA"			
Sample Information							Start Date: 6/23/2010 Completion Date: 6/23/2010			Casing Elevation: 231.88 - NGVD 29' Surface Elevation: 229.6 +/- NGVD 29' Wellhead Type: Standpipe			
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction		
26	S-6	60-75	25-30	NA	NA			Brown, wet, COARSE SAND, some (sub-angular) gravel	SAND				
28								As Field Testing Results					
30	S-7	60-70	30-35	NA	NA			Brown, wet, COARSE SAND, some (sub-angular) gravel					
32													
34													
36	S-8	100 lbs	35-40	NA	NA			Brown, saturated, FINE TO MEDIUM SAND, trace coarse sand					
38													
40								As Field Testing Results					
42	S-9	60-74	40-45	NA	NA			Brown, saturated, MEDIUM TO COARSE SAND, trace fine sand					
44													
46	S-10	60-77	45-50	NA	NA			8"-8' Brown, saturated, COARSE SAND AND GRAVEL with angular rock fragments	SAND				
48								9"-27" Brown, saturated, FINE TO MEDIUM SAND, trace coarse sand					
50								As Field Testing Results					
Notes												Key	<div><div></div>Centent</div> <div><div></div>Drill Cuttings Native Soils</div> <div><div></div>Bentonite Grout</div> <div><div></div>Sand</div> <div><div></div>Screen</div> <div><div></div>Riser</div>
1) Direct Push groundwater profile sampling conducted on 6/10/10													
2) Groundwater profile sampler refusal at 70'													
3)													
4)													
5)													
Remarks													
1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made													
2) Field As testing values represent arsenic concentrations (in ug/l) collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data													
3) Sample is designated as either "C" for composite or "G" for a discrete grab sample													
4) Approximate water table. NA - Not Applicable. NR - No Recovery. bgs - below ground surface. ags - above ground surface													




Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems' Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample.  
▼ Approximate water table. N/A Not Applicable. NR No Recovery, but below ground surface. ags above ground surface.











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 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-04</b>		Sheet 3 of 4		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DJ Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Type: Steel Size: 3.25" Hammer: Fall NA lbs		
<b>Sample Information</b> Start Date: 6/24/2010 Completion Date: 6/24/2010							Casing Elevation: 212.37 - NGVD 29 Surface Elevation: 209.8 +/- NGVD 29 Wellhead Type: Standpipe				
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
52	S-11	60-5	50-55	NA	NA			Brown, saturated, FINE TO MEDIUM SAND, trace silt			Bentonite 49'-52'
54							5	As Field Testing Results			#2 More Sand 52'-65'
56	S-12	60-23	55-60	NA	NA			Brown, saturated, COARSE TO MEDIUM SAND, little fine sand (increasing percentage with depth)	SAND		1 5" Schedule 40 PVC Well screen - 0.01" slot 55'-65'
58											
60											
62	S-13	60-24	60-65	NA	NA			Brown, saturated, FINE TO MEDIUM SAND (some orange coloring)	SAND		
64							5	As Field Testing Results			
66	S-14	60-35	65-70	NA	NA			Brown, saturated, FINE TO MEDIUM SAND (some orange coloring)			CASING REFUSAL @ 65'
68											
70									SAND		
72	S-15	60-28	70-78	NA	NA			Brown, saturated, FINE TO MEDIUM SAND (some orange coloring)			
74							5	As Field Testing Results			

**Notes:**

- 1) Direct Push groundwater profile sampling conducted on 6/8/10
- 2) Groundwater profile sampler refusal @ 65'
- 3)
- 4)
- 5)
- 6)

**Key:**







-  Cement
-  Drill Cuttings Native Soils
-  Bentonite Grout
-  Sand
-  Screen
-  Refusal

**Remarks:**

- 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.
- 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data.
- 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample.


▼ Approximate water table. NA: Not Applicable. NR: No Recovery. bgs: below ground surface. ags: above ground surface.



 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SIIM-10-04</b>		Sheet 4 of 4		
Client: USACE Project: SIIL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DI Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spoon Type: 3.25" Size: 60" Hammer: Fall S.A. lbs: N/A		
<b>Sample Information</b>							Start Date: 6/24/2010 Completion Date: 6/24/2010		Casing Elevation: 212.37 - NGVD 29' Surface Elevation: 209.8+/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
76	S-16	60-19	75-80	NA	NA			Brown and orange, wet, COARSE TO MEDIUM SAND, trace gravel, dense.			
78								Bottom 2" - Gray, saturated, Fine Sand	GLACIAL TILL		
80											
82	S-17	60/38	80-85	NA	NA			Dark brown to brown, saturated, MEDIUM TO COARSE SAND, trace gravel and fine sand, dense (some orange coloring)			
84								As Field Testing Results			
86	S-18	60/18	85-90	NA	NA			Brown, saturated, MEDIUM TO COARSE SAND, trace fine gravel and fine sand, dense.			
88											
90											
92	S-19	60/20	90-95	NA	NA			9"-10" - Brown, saturated, MEDIUM TO COARSE SAND, little fine sand			
								10"-14" - Brown, saturated, FINE SAND AND SILT			
94								14" - 16" Gray, saturated, MEDIUM TO COARSE SAND, little fine gravel and fine sand, trace silt, dense.			
					10-20			As Field Testing Results			
96								SAMPLER REFUSAL 97-95'			
98											
100											
Notes: 1) Direct Push groundwater profile sampling conducted on 6/8/10 2) Groundwater profile sampler refusal at 95' 3) 4) 5) 6)							Key:		Centimeter  Drill Cuttings Native Soils  Bentonite Grout  Sand  Gravel  Rock		
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l, collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) - Approximate water table. NA= Not Applicable. NR= No Recovery. lbs=below ground surface. ags= above ground surface.											











 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-05A</b>		Sheet 2 of 4		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DJT Drill Method: Direct Push Foreman: Rodney Kaddy SCT Inspector: Carolyn Hardt		Casing: Steel Type: Steel Size: 3.25" Hammer: Fall NA lbs Sampler: Geoprobe Spoon 60" NA"		
<b>Sample Information</b>							Start Date: 7/2/2010 Completion Date: 7/2/2010		Casing Elevation: 234.92 - NGVD 29' Surface Elevation: NA Wellhead Type: Flush Mount		
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
26	S-5	60/56	25-30	NA	NA			Light brown to dark brown, moist to wet, FINE TO MEDIUM SAND, trace coarse sand and gravel			
28											
30					5			As Field Testing Results			
32	S-6	60/60	30-35	NA	NA			Dark brown to light brown, wet, FINE TO MEDIUM SAND, trace coarse sand and gravel			
34											
36		60/0	35-40	NA	NA			NO RECOVERY			
38											
40					5			As Field Testing Results			
42	S-7	60/23	40-45	NA	NA			Light brown, saturated, FINE SAND			
44											
46	S-8	60/24	45-50	NA	NA			Light brown, saturated, FINE SAND			
48											
50					3			Light brown, saturated, FINE SAND			

**Notes**

- 1) Direct Push groundwater profile sampling conducted on 6/9/10
- 2) Groundwater profile sampler refusal at 110' AS - 5' below 100'
- 3)
- 4)
- 5)
- 6)

**Key**

-  Cement
-  Drill Cuttings/ Native Soils
-  Bentonite Grout
-  Sand
-  Screen
-  Riser



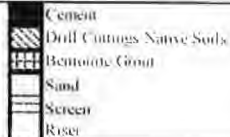
**Remarks:**

1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.


2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data.


3) Sample is designated as either "C" for composite or "G" for a discrete grab sample.

▼ = Approximate water table. NA = Not Applicable. NR = No Recovery. bgs = below ground surface. ags = above ground surface.


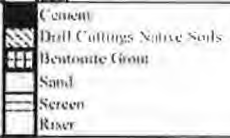
 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-05A</b>		Sheet 3 of 4		
Client: USACE Project: SHM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DI Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Carolyn Hardt		Casing: Steel Sampler: Geoprobe Spoon Size: 3.25" / 60" Hammer: Fall N/A lbs / N/A"		
<b>Sample Information</b>							Start Date: 7/2/2010 Completion Date: 7/2/2010		Casing Elevation: 234.92 - NGVD 29' Surface Elevation: NA Wellhead Type: Flush Mount		
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
52	S-9	60-30	50-55	NA	NA			Light brown, saturated, FINE SAND			
54											
56	S-10	60-13	55-60	NA	NA			Light brown, saturated, FINE SAND	SAND		
58											
60					<5			As Field Testing Results			
62	S-11	60-50	60-65	NA	NA			Light brown, saturated, FINE SAND			
64											
66											
68	S-13	60-30	65-70	NA	NA			Light brown, saturated, FINE SAND	SAND		
70					<5			As Field Testing Results			
72								SAMPLER REFUSAL at 70'			
74											
Notes: 1) Direct Push groundwater profile sampling conducted on 6/9/10. 2) Groundwater profile sampler refusal at 110' As - 5 mg/L, at 109'. 3) 4) 5) 6)										Key: 	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L, collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table: NA - Not Applicable; NR - No Recovery; bgs - below ground surface; ags - above ground surface.											



 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-05A</b>		Sheet 4 of 4		
Client: DSACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCT Inspector: Carolyn Hardt		Casing: Steel Sampler: Geoprobe Spoon Type: 3.25" Size: 6d" Hammer: Fall NA lbs: NA"		
<b>Sample Information</b>							Start Date: 7/2/2010 Completion Date: 7/2/2010		Casing Elevation: 234.92 - NGVD 29' Surface Elevation: NA Wellhead Type: Flush Mount		
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/ft.	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
76											
78											
80											
82											
84											
86											
88											
90											
92											
94											
96											
98											
100											
Notes: 1) Direct Push groundwater profile sampling conducted on 6.9.10 2) Groundwater profile sampler refusal at 110' AS - 5 ug/L at 100' 3) 4) 5) 6)									Key: <div style="display: flex; flex-direction: column; align-items: flex-start;"> <div style="width: 10px; height: 10px; background-color: black; margin-bottom: 2px;"></div> <div style="width: 10px; height: 10px; background-color: gray; margin-bottom: 2px;"></div> <div style="width: 10px; height: 10px; background-color: white; border: 1px solid black; margin-bottom: 2px;"></div> <div style="width: 10px; height: 10px; background-color: white; border: 1px solid black; margin-bottom: 2px;"></div> <div style="width: 10px; height: 10px; background-color: white; border: 1px solid black; margin-bottom: 2px;"></div> <div style="width: 10px; height: 10px; background-color: white; border: 1px solid black; margin-bottom: 2px;"></div> </div> <div style="display: flex; flex-direction: column; align-items: flex-start;"> <div>Cement</div> <div>Drill Cuttings Native Soils</div> <div>Bentonite Grout</div> <div>Sand</div> <div>Screen</div> <div>Riser</div> </div>		
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▼ = Approximate water table. NA = Not Applicable. NR = No Recovery. lbs = below ground surface. ags = above ground surface.											



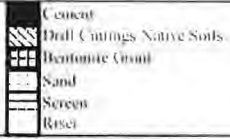
 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SIIM-10-06</b>		Sheet 1 of 4		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sample: Geoprobe Splicer Size: 3.25" 60" Hammer: Fall NA lbs NA"		
<b>Sample Information</b>							Start Date: 6/21/2010 Completion Date: 6/21/2010		Casing Elevation: 232.77 - NGVD 29' Surface Elevation: 229.84/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
0	S-1	60-42	0-5	NA	NA			Topsoil	TOPSOIL		Standpipe is 3' ags
2								Light brown to gray, dry, COARSE SAND, some medium sand			Cement 0-2'
4											
6	S-2	60-41	5-10	NA	NA			Light brown to gray, dry, COARSE SAND, (well sorted)	SAND		
8											
10											
12	S-3	60-53	10-15	NA	NA			Light brown to gray, dry, COARSE SAND, (well sorted)			
14											
16	S-4	60-40	15-20	NA	NA			Brown, moist to wet, COARSE SAND, (well sorted)	SAND		
18											1.5" Schedule 40 PVC Riser 0-69.5'
20											
22	S-5	60-48	20-25	NA	NA			Brown, Sampled, COARSE SAND, (well sorted)			Grout 2-64.5'
24								As Field Testing Results			
Notes: 1) Direct Push groundwater profile sampling conducted on 5/24/10 & 5/26/10. 2) Groundwater profile sampler refusal at 80'. 3) 4) 5) 6)										Key: <ul style="list-style-type: none"> <li>Cement</li> <li>Drill Cuttings/ Native Soils</li> <li>Bentonite Grout</li> <li>Sand</li> <li>Screen</li> <li>Riser</li> </ul>	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l, collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA=Not Applicable NR=No Recovery ags=below ground surface ags=above ground surface											



 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-06</b>		Sheet 2 of 4		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spoon Size: 3.25" Hammer: Fall NA lbs NA"		
<b>Sample Information</b>							Start Date: 6/21/2010 Completion Date: 6/21/2010		Casing Elevation: 232.77 - NGVD 29' Surface Elevation: 229.8 +/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/ft.	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
26	S-6	60/43	25-30	NA	NA			Brown, saturated, COARSE SAND AND GRAVEL, some medium sand			
28											
30											
32	S-7	60/0	30-35	NA	NA			NO RECOVERY			
34								As Field Testing Results			
36	S-8	60/0	35-40	NA	NA			NO RECOVERY			
38											
40	S-9	60/26	40-45	NA	NA			0"-12" Light Brown to gray, saturated, COARSE SAND			
42								12"-26" Light Brown to Gray, Saturated, FINE - MEDIUM SAND			
44								As Field Testing Results			
46	S-10	60/60	45-50	NA	NA			Light brown to gray, wet, FINE TO MEDIUM SAND, (fine silt, well sorted)			
48											
50											
Notes: 1) Direct Push groundwater profile sampling conducted on 5/24/10 & 5/26/10 2) Groundwater profile sampler refusal at 80" 3)							Key:				
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA=Not Applicable NR=No Recovery lbs=below ground surface, abs=above ground surface											






 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring Well ID: <b>SHM-10-06</b>		Sheet 4 of 4		
Client: USACE Project: SHM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney SCT Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spoon Type: 2.25" Size: 60" Hammer: Fall N/A lbs: N/A"		
<b>Sample Information</b>							Start Date: 6/21/2010 Completion Date: 6/21/2010		Casing Elevation: 232.77 - NGVD 29' Surface Elevation: 229.8 +/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
76	S-16	60-40	75-80	NA	NA			Light brown to gray, moist, FINE TO MEDIUM SAND, rock fragments, dense			
78								As Field Testing Results	SAND	1	
80								SAMPLER REFUSAL @ 80'		2	CASING REFUSAL @ 79.5'
82											
84											
86											
88											
90											
92											
94											
96											
98											
Notes: 1) Direct Push groundwater profile sampling conducted on 5-24-10 & 5-26-10 2) Groundwater profile sampler refusal at 80' 3) 4) 5) 6)										Key: 	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l, collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. * - Approximate water table NA - Not Applicable NR - No Recovery hgs - below ground surface ags - above ground surface											








 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts		Boring/Well ID: <b>SIIM-10-06A</b>		Sheet 2 of 4							
Client: USACE Project: SIIL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Geosearch Drill Rig: Geoprobe 6610D1 Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spoon Type: 3.25" Hamber: Fall NA lbs: NA"							
<b>Sample Information</b> Start Date: 6/16/2010 Completion Date: 6/18/2010		Casing Elevation: 248.39 - NGVD 29' Surface Elevation: 245.7 +/- NGVD 29' Wellhead Type: Standpipe									
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
26	S-6	60-60	25-30	NA	NA			Light brown to gray, dry, FINE TO MEDIUM SAND			
28											
30											
32	S-7	60/56	30-35	NA	NA			Light brown, moist, MEDIUM SAND, some fine and coarse sand, trace gravel	SAND		
34											
36											
38								As Field Testing Results			
40	S-8	60/56	35-40	NA	NA			Light brown, wet, MEDIUM SAND, some fine and coarse sand, trace gravel			1.5" Schedule 40 PVC Riser 0.77'
42											
44											
46	S-9	60/22	40-45	NA	NA			Light brown, wet, MEDIUM SAND, some fine and coarse sand, trace gravel	SAND		Gravel 2'0.2"
48											
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52											
54											
56											
58											
60											
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 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts		Boring/Well ID: <b>SHM-10-06.A</b>		Sheet 4 of 4							
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DI Drill Method: Direct Push Foreman: Rodney Kaddy SCT Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spoon Type: Steel Size: 1.25" Hammer: Fall NA lbs: NA"							
<b>Sample Information</b>		Start Date: 6/16/2010 Completion Date: 6/18/2010		Casing Elevation: 248.39 - NGVD 29' Surface Elevation: 245.7 +/- NGVD 29' Wellhead Type: Standpipe							
Depth	Sample ID	Pen/Rec. (in.)	Interval (ft.)	Blow/ft.	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
76	S-16	60-14	75-80	NA	NA			Light gray to brown, saturated, FINE TO MEDIUM SAND, dense	SAND		 #2 Marie Sand 74'-87'  1.5" Schedule 40 PVC Well screen - 0.01" slot 77'-87'
78											
80	S-17	60/34	80-85	NA	NA			Light gray to brown, saturated, FINE TO MEDIUM SAND, dense			
82											
84					60			As Field Testing Results			
86	S-18	60/14	85-90	NA	NA			Light gray to brown, saturated, FINE TO MEDIUM SAND, dense	SAMPLER REFUSAL at 90'		CASING REFUSAL at 90'
88											
90											
92											
94					5			Arsenic Field Testing Results			
96											
98											
Notes: 1) Direct Push groundwater profile sampling conducted on 5/24/10 & 5/25/10 2) Groundwater profile sampler refusal at 110.5' As = 0 mg/L at 104' and As = 20 mg/L at 110' 3) 4) 5) 6)											
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in mg/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA = Not Applicable. NR = No Recovery. bgs = below ground surface. ags = above ground surface.											


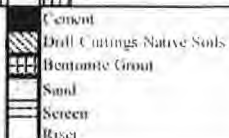
 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts						Boring Well ID: <b>SHM-10-07</b>		Sheet 1 of 3			
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA						Drilling Co: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Rob Danckert SCT Inspector: PJV		Casing: Steel Sampler: Fine Bore Size: 6" 60" Hammer: Fall NA lbs NA"			
<b>Sample Information</b>						Start Date: 5/19/2010 Completion Date: 5/20/2010		Casing Elevation: 246.59 - NGVD 29' Surface Elevation: 244.6 +/- NGVD 29' Wellhead Type: Standpipe			
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
0	S-1	60.36	0-5	NA	NA			0"-16" Brown, dry, MEDIUM TO COARSE SAND, little fine gravel, trace coarse gravel			Standpipe is 3'ags
4								16"-19" Dark brown, FINE SAND, organic materials (leaves & wood)			Cement 0-2'
6	S-2	60.53	5-10	NA	NA			19"-36" Gray, dry, FINE TO MEDIUM SAND, some coarse sand to fine gravel, trash (metal fragments)			
8								4"-12" Brown, moist, MEDIUM TO COARSE SAND, little fine gravel			
10								12"-53" Light brown, moist, FINE TO MEDIUM SAND, little coarse sand, trace fine gravel			
12	S-3	60.51	10-15	NA	NA			Brown, moist to wet, FINE TO MEDIUM SAND			
14											
16	S-4	60.46	15-20	NA	NA			Brown, moist to wet, FINE TO MEDIUM SAND			Cement 2-3 ft
18											
20	S-5	60.40	20-22	NA	NA			Brown, wet, FINE TO MEDIUM SAND			
22											
24											
Notes: 1) Groundwater profile sampling conducted with a bladder pump 2) Soil sample collected for laboratory analysis 3) 4) 5) 6)								Key: <ul style="list-style-type: none"> <li>Cement</li> <li>Drill Cuttings Native Soils</li> <li>Bentonite Grout</li> <li>Sand</li> <li>Screen</li> <li>Riser</li> </ul>			
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▼ = Approximate water table. NA=Not Applicable. NR=No Recovery. bgs=below ground surface. ags=above ground surface.											



Sovereign Consulting Inc. 905B South Main Street Mansfield, Massachusetts							Boring Well ID: SHM-10-07		Sheet 2 of 3			
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: SCI Inspector: PJV		Casing: Steel Type: Steel Size: 6" Type: Hammer Size: NA lbs		Sampler: Core Barrel Size: 60" Type: Fall Size: NA"	
Start Date: 5/19/2010 Completion Date: 5/20/2010							Casing Elevation: 246.59 - NGVD 29' Surface Elevation: 244.6 +/- NGVD 29' Wellhead Type: Standpipe					
Sample Information							Stratum Change (ft.)		Notes		Test Boring/ Monitoring Well Construction	
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction	
26	S-6	60-46	25-30	NA	NA			0"-22" Brown, wet, FINE TO MEDIUM SAND				
28								22"-46" Gray, saturated, FINE TO MEDIUM SAND		2	2" Schedule 40 PVC Riser 0-40'	
30	S-7	60-54	30-35	NA	NA			Gray, saturated, FINE TO MEDIUM SAND	SAND		Grout 2'-36"	
32												
34												
36	S-8	60-50	35-40	NA	NA			Brown, saturated, FINE TO MEDIUM SAND			Remnant 11'-15"	
38												
40								As Field Testing Results		1	#2 More Sand 38'-50'	
42	S-9	60-51	40-45	NA	NA			0"-10" Brown, saturated, FINE TO MEDIUM SAND				
44								10"-25" Brown, moist, FINE TO COARSE SAND AND FINE TO COARSE GRAVEL, little silt, dense		2	2" Schedule 40 PVC Well screen - 0.01" slot 40'-50'	
46	S-10	60-48	45-50	NA	NA			25"-30" COBBLES AND ROCK FRAGMENTS	GLACIAL TILL			
48								30"-51" Gray, moist, FINE TO COARSE SAND AND FINE TO COARSE GRAVEL, little silt, dense				
50								0"-36" Gray, moist, FINE TO COARSE SAND AND FINE TO COARSE GRAVEL, little silt, dense				
								36"-48" ROCK FRAGMENTS AND ROCK DUST	GLACIAL TILL	1		
Notes: 1) Groundwater profile sampling conducted with a bladder pump 2) Soil sample collected for laboratory analysis 3) 4) 5) 6)							Key:		Cement Drill Cuttings Native Soils Bentonite Grout Sand Screen Riser			
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected in the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA Not Applicable. NR No Recovery. bgs below ground surface. ags above ground surface.												



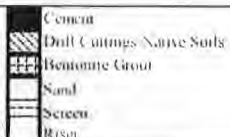
 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SIIM-10-07</b>		Sheet 3 of 3		
Client: USACE Project: SIIL - Fort Devens Project Number: AC001 Location: Fort Devens Aver, MA							Drilling Co: Bort Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: SCI Inspector: PJV		Casing: Steel Sampler: Core Barrel Size: 6" Hammer: Fall S.A lbs: NA*		
<b>Sample Information</b>							Start Date: 5/19/2010 Completion Date: 5/20/2010		Casing Elevation: 246.59 - NGVD 29' Surface Elevation: 244.6+/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/g <sup>2</sup>	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
52	S-11	60-45	50-55	NA	NA			ROCK FRAGMENTS AND ROCK DUST 1" - 5" Thick Rock "Pucks" in Bottom	BEDROCK		
54											
56								END BORING @ 55 FEET			
58											
60											
62											
64											
66											
68											
70											
72											
74											
Notes: 1) Groundwater profile sampling conducted with a bladder pump 2) Soil sample collected for laboratory analysis. 3) 4) 5) 6)										Key: <div style="display: flex; flex-direction: column; align-items: flex-start;"> <div style="width: 15px; height: 15px; background-color: black; margin-bottom: 2px;"></div> <div style="width: 15px; height: 15px; background: repeating-linear-gradient(45deg, transparent, transparent 2px, black 2px, black 4px); margin-bottom: 2px;"></div> <div style="width: 15px; height: 15px; background: repeating-linear-gradient(-45deg, transparent, transparent 2px, black 2px, black 4px); margin-bottom: 2px;"></div> <div style="width: 15px; height: 15px; background: radial-gradient(circle, black 1px, transparent 1px); background-size: 4px 4px; margin-bottom: 2px;"></div> <div style="width: 15px; height: 15px; border: 1px solid black; margin-bottom: 2px;"></div> <div style="width: 15px; height: 15px; border: 1px dashed black;"></div> </div> <div style="margin-top: 5px;">           Cement            Drill Cuttings Native Soils            Bentonite Grout            Sand            Screen            Buser         </div>	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▼ Approximate water table NA=Not Applicable NR=No Recovery bgs=below ground surface ags=above ground surface											




 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-08</b>			Sheet 1 of 3		
Client: USACE Project: SHIL - Fort Devens Project Number: AC 001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman			Casing: Steel Sampler: Geoprobe Sprocket Type: Steel Size: 4.25" Hammer: Fall NA lbs NA"		
<b>Sample Information</b> Start Date: 6/29/2010 Completion Date: 6/29/2010							Casing Elevation: 214.21 - NGVD 29' Surface Elevation: 211.6+/- NGVD 29' Wellhead Type: Standpipe					
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction	
2	S-1	60.34	0-5	NA	NA			Topsoil (4-inches)	TOPSOIL			Standpipe is 3' ups
4								Brown, moist, FINE SAND, trace medium to coarse sand, trace silt, (well sorted)				Cement 0-2'
6	S-2	60.36	5-10	NA	NA			Brown, moist, MEDIUM TO COARSE SAND, trace silt and fine sand, with rock fragments	SAND			
8								Brown, moist, FINE SAND, trace medium sand and silt				
10								Brown, wet, MEDIUM TO COARSE SAND, some gravel (sub-rounded)				1.5" Schedule 40 PVC Riser 0-46'
12	S-3	60.50	10-15	NA	NA			0"-11" Brown, wet, FINE TO MEDIUM SAND, trace silt As Field Testing Results				
14								11"-20" Brown, wet, MEDIUM TO COARSE SAND, trace silt and fine sand, with rock fragments				
16	S-4	60.56	15-20	NA	NA			20"-27" Dark brown, saturated, FINE TO MEDIUM coarse sand 27"-50" Brown, saturated, FINE SAND	SAND			
18								Brown, saturated, FINE SAND, some medium sand, trace silt				
20												Grout 2'-41'
22	S-5	60.60	20-25	NA	NA			Dark brown, saturated, MEDIUM TO COARSE SAND, some gravel (sub-rounded) As Field Testing Results	SAND			
24								Brown, saturated, MEDIUM TO FINE SAND, trace coarse sand Grayish brown, SAND, well sorted, Wet				
<b>Notes:</b> 1) Direct Push groundwater profile sampling conducted on 6/3/10 2) Groundwater profile sampler refusal at 62.5' 3) 4) 5) 6)										<b>Key</b> 		
<b>Remarks:</b> 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▼ Approximate water table. NA=Not Applicable. NR=No Recovery. fgs=below ground surface. ags=above ground surface.												


Sovereign Consulting Inc. 905B South Main Street Mansfield, Massachusetts							Boring Well ID: SHM-10-08		Sheet 2 of 3		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spoon Type: Steel Size: 4.25" Hammer: Fall NA lbs: NA		
Sample Information							Start Date: 6/29/2010 Completion Date: 6/29/2010		Casing Elevation: 214.21 - NGVD 29' Surface Elevation: 211.6 +/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
26	S-6	60-14	25-30	NA	NA			Light brown, saturated, FINE TO MEDIUM SAND, trace silt, (percent of fine sand increasing with depth)			
28											
30											
32	S-7	60-27	30-35	NA	NA			Light brown to gray, saturated, MEDIUM TO FINE SAND, trace silt and coarse sand As Field Testing Results	SAND		
34											
36	S-8	60-35	35-40	NA	NA			Light brown, saturated, FINE SAND, trace silt			
38								Light brown, saturated, MEDIUM SAND, trace fine sand			
40								Brown, saturated, FINE SAND, trace silt	SAND		
42	S-9	60-35	40-45	NA	NA			Brown, saturated, MEDIUM TO COARSE SAND, trace gravel, fine sand, and silt As Field Testing Results			
44								Orange brown, saturated, MEDIUM TO COARSE SAND AND GRAVEL, (sub-angular to sub-rounded)			
46											
48	S-10	60-30	45-50	NA	NA			Brown, saturated, MEDIUM TO COARSE SAND, some gravel (angular)	SAND		
50								Brown, saturated, FINE SAND, some medium sand, trace silt			
Notes									Key		
1) Direct Push groundwater profile sampling conducted on (6/3/10) 2) Groundwater profile sampler refusal at (62.5') 3) 4) 5) 6)									Cement Drill Cuttings/ Native Soils Bentonite Grout Sand Screen Riser		
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l, collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA=Not Applicable NR=No Recovery lbs=below ground surface ags=above ground surface											





 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts		Boring/Well ID: <b>SIIM-10-08</b>		Sheet 3 of 3							
Client: USACE Project: SIIM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCL Inspector: Danielle Eastman		Casing: Steel Sample: Geoprobe Spoon Size: 3.25" Hammer: Fall N/A lbs: N/A"							
<b>Sample Information</b>		Start Date: 6/29/2010 Completion Date: 6/29/2010		Casing Elevation: 214.21 - NGVD 29' Surface Elevation: 211.6 +/- NGVD 29' Wellhead Type: Standpipe							
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/d"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
52	S-11	60-30	50-55	NA	NA			Light brown, saturated, FINE SAND, some gravel and coarse sand, trace silt As Field Testing Results	SAND	1	 #2 Mono Sand 43'-56'  1.5" Schedule 40 PVC Well screen - 0.01" slot 46'-56'
56	S-12	24-12	55-57	NA	NA			Brown, saturated, MEDIUM TO COARSE SAND, some fine sand Gray, dry, FINE SAND, some silt, with rock fragments (angular) (Till)	GLACIAL TILL		CASING REFUSAL @ 56'
58								SAMPLER REFUSAL @ 57'			
60											
62								As Field Testing Results			
64											
66											
68											
70											
72											
74											
Notes: 1) Direct Push groundwater profile sampling conducted on 6/3/10 2) Groundwater profile sampler refusal at 62.5' 3) 4) 5) 6)										Key:  Cement Drill Cuttings/ Native Soils Bentonite Grout Sand Screen Risin	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA= Not Applicable. NR= No Recovery. bgs= below ground surface. ags= above ground surface.											


 Sovereign Consulting Inc. 905B South Main Street Mansfield, Massachusetts		Boring/Well ID: SHM-10-09		Sheet 1 of 3	
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Geosarch Drill Rig: Geoprobe 6610D1 Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe/Spoon Type: Steel Size: 3.25" Hammer: Fall N/A lbs: N/A"	
		Start Date: 6/14/2010 Completion Date: 6/15/2010		Casing Elevation: NA Surface Elevation: NA Wellhead Type: Standpipe	
				Stratum Change (ft.)	
				Notes	
				Test Boring/ Monitoring Well Construction	
				</	


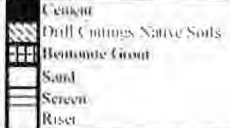


 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts		Boring Well ID: <b>SIIM-10-09</b>		Sheet 2 of 3							
Client: USACE Project: SIIL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Geosearch Drill Rig: Geoprobe 6610D1 Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spool Type: 3.25" Size: 60" Hammer: Fall NA lbs: NA"							
<b>Sample Information</b>		Start Date: 6/14/2010 Completion Date: 6/15/2010		Casing Elevation: NA Surface Elevation: NA Wellhead Type: Standpipe							
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
26	S-6	60-30	25-30	NA	NA			Light brown, saturated, MEDIUM SAND, some coarse sand			
28											
30											
32	S-7	60-16	30-35	NA	NA			Light brown, saturated, MEDIUM TO COARSE SAND, (well sorted) As Field Testing Results			
34											
36	S-8	60-23	35-40	NA	NA			Light brown, saturated, MEDIUM TO COARSE SAND, (well sorted)			
38											
40											
42	S-9	60-26	40-45	NA	NA			Light brown, saturated, MEDIUM SAND, some coarse sand (well sorted) As Field Testing Results			
44											
46	S-10	60-32	45-50	NA	NA			Brown, saturated, FINE TO MEDIUM SAND AND SILT little coarse sand			
48											
50											
Notes: 1) Direct Push groundwater profile sampling conducted on 5/28/10 & 6/1/10 2) Groundwater profile sampler refusal at 82' As - 5' to 1', at 81' 3) 4) 5) 6)									Key: <div style="display: flex; flex-direction: column; align-items: flex-start;"> <div style="width: 15px; height: 15px; background-color: black; margin-bottom: 2px;"></div> <div style="width: 15px; height: 15px; background-color: gray; margin-bottom: 2px;"></div> <div style="width: 15px; height: 15px; border: 1px solid black; margin-bottom: 2px;"></div> <div style="width: 15px; height: 15px; border: 1px dashed black; margin-bottom: 2px;"></div> <div style="width: 15px; height: 15px; border: 1px dotted black; margin-bottom: 2px;"></div> <div style="width: 15px; height: 15px; border: 1px solid black; margin-bottom: 2px;"></div> <div style="width: 15px; height: 15px; border: 1px solid black; margin-bottom: 2px;"></div> </div> <div style="display: flex; flex-direction: column; align-items: flex-start;"> <div>Cement</div> <div>Drill Cuttings/ Native Soils</div> <div>Bentonite Grout</div> <div>Sand</div> <div>Screen</div> <div>Riser</div> </div>		
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) = Approximate water table. NA= Not Applicable. NR= Not Recovery. bgs= below ground surface. ags= above ground surface.											








 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SIIM-10-09</b>		Sheet 3 of 3		
Client: USACE Project: SHH - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCL Inspector: Danielle Eastman		Casing: Steel Sampler: Geoprobe Spoon Size: 1.25" Hammer: Fall NA lbs NA"		
<b>Sample Information</b>							Start Date: 6/14/2010 Completion Date: 6/15/2010		Casing Elevation: NA Surface Elevation: NA Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
52	S-11	60-25	50-55	NA	NA			Brown, saturated, MEDIUM TO COARSE SAND, some gravel (rounded) As Field Testing Results			NO WELL INSTALLED
54											
56	S-12	60-13	55-60	NA	NA			0"-4" Brown, saturated, FINE SAND, trace silt 0"-33" Brown, saturated, COARSE SAND, some gravel (angular)	SAND		
58											
60											
62	S-13	60-26	60-65	NA	NA			Grey, saturated, FINE SAND, some rock fragments (angular) (HLL) As Field Testing Results	GLACIAL (HLL)		
64											
66											
68											
70											
72											
74											
Notes: 1) Direct Push groundwater profile sampling conducted on 5/28/10 & 6/1/10 2) Groundwater profile sampler refusal at 82' As - 5' (ug/L) at 81' 3) 4) 5) 6)							Key: 				
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▽ = Approximate water table. NA = Not Applicable. NR = No Recovery. bgs = below ground surface. ags = above ground surface.											




 Sovereign Consulting Inc. 905B South Main Street Mansfield, Massachusetts		Boring/Well ID: SHM-10-10		Sheet 1 of 3							
Client: USACE Project: SHM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DI Drill Method: Direct Push Foreman: Rodney Kaddy SCT Inspector: Danielle Eastman		Casing: Steel Type: Steel Size: 3.25" Hammer: Fall N/A lbs Sample: Geoprobe Spoon Size: 1.625" N/A"							
Start Date: 6/2/2010 Completion Date: 6/3/2010		Casing Elevation: 217.04 - NGVD 29' Surface Elevation: 215.0+/- NGVD 29' Wellhead Type: Standpipe									
Sample Information		Sample Description		Stratum Change (ft.)	Test Boring/ Monitoring Well Construction						
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/ft.	Field As Testing	Sample Type	Water Detected				
2	S-1	60-23	0-5	NA	NA			Topsoil (6-inches)	TOPSOIL		Standpipe is 3' ags
4								Light brown, dry, FINE TO MEDIUM SAND, some gravel	Sand		Cement 0-2'
6	S-2	60-29	5-10	NA	NA			Light brown, dry, COARSE SAND AND GRAVEL, some medium sand, trace fine sand	SAND & GRAVEL		
8											
10											1.5" Schedule 40 PVC Riser 0-50'
12	S-3	60-22	10-15	NA	NA			0"-14" Light brown, dry, MEDIUM TO COARSE SAND AND GRAVEL, trace fine sand As Field Testing Results			
14								14"-20" Light brown, dry, COARSE SAND AND GRAVEL, trace fine sand As Field Testing Results			
16	S-4	60-43	15-20	NA	NA			0"-20" Light brown, dry, COARSE TO MEDIUM SAND AND GRAVEL			
18								20"-43" Light brown, wet, COARSE SAND AND GRAVEL (sub-angular to sub-rounded), some medium sand			
20											Grout 2'-51'
22	S-5	60-4	20-25	NA	NA			Brown, saturated, COARSE SAND AND GRAVEL (sub-rounded to rounded), rock fragments As Field Testing Results	SAND & GRAVEL		
24											
Notes								Key			
1) Direct Push groundwater profile sampling conducted on 6/2/10 & 6/3/10								Cement			
2) Groundwater profile sampler refusal at 72'								Drill Cuttings/Native Soils			
3)								Bentonite Grout			
4)								Sand			
5)								Screen			
6)								Riser			
Remarks											
1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.											
2) Field As testing values represent arsenic concentrations in mg/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data.											
3) Sample is designated as either "C" for composite or "G" for a discrete grab sample.											
▼ = Approximate water table. NA = Not Applicable. NR = No Recovery. bgs = below ground surface. ags = above ground surface.											

 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring Well ID: <b>SHM-10-10</b>			Sheet 2 of 3		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Geosearch Drill Rig: Geoprobe 6610(2) Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman			Casing Type: Steel Size: 3-25" Hammer: Fall N/A lbs: N/A"		
<b>Sample Information</b>							Start Date: 6/2/2010 Completion Date: 6/3/2010			Casing Elevation: 217.04 - NGVD 29' Surface Elevation: 215.0 +/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen/Rec. (in.)	Interval (ft.)	Blow/ft.	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction	
26	S-6	60-15	25-30	NA	NA			Brown, saturated, COARSE SAND AND GRAVEL (sub-rounded to rounded), rock fragments	SAND & GRAVEL	1	1 1/2" Schedule 40 PVC Riser 0-56'	
28												
30												
32	S-7	60-15	30-35	NA	NA	5		As Field Testing Results Brown, saturated, COARSE SAND AND GRAVEL (sub-rounded to rounded), rock fragments				
34												
36	S-8	60-15	35-40	NA	NA			Brown, saturated, COARSE SAND AND GRAVEL (sub-rounded to rounded), rock fragments				
38												
40									SAND & GRAVEL	1		
42	S-9	60-22	40-45	NA	NA	8		As Field Testing Results Brown, saturated, COARSE SAND AND GRAVEL (sub-rounded to rounded), rock fragments			Grout 25-51'	
44												
46	S-10	60-22	45-50	NA	NA			Brown, saturated, MEDIUM TO COARSE SAND, some fine sand, trace gravel	SAND			
48												
50												
<b>Notes:</b> 1) Direct Push groundwater profile sampling conducted on 6/2/10 & 6/3/10 2) Groundwater profile sampler refusal @ 72" 3) 4) 5) 6)										<b>Key:</b> 		
<b>Remarks:</b> 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l, collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA=Not Applicable, NR=No Recovery, lbs=below ground surface, ngs=above ground surface												



 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts						Boring/Well ID: <b>SIIM-10-10</b>		Sheet 3 of 3	
Client: USACE Project: SIIL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA						Drilling Co.: Geosearch Drill Rig: Geoprobe 6610DT Drill Method: Direct Push Foreman: Rodney Kaddy SCI Inspector: Danielle Eastman		Casing: Steel Type: Steel Size: 3.25" Hammer N/A lbs Sampler: Geoprobe Spinn Size: 1.0" Fall N/A"	
<b>Sample Information</b> <div> <div>Depth</div> <div>Sample ID</div> <div>Pen./Rec. (in.)</div> <div>Interval (ft.)</div> <div>Blow (ft.)</div> <div>Field As Testing</div> <div>Sample Type</div> <div>Water Detected</div> </div>						Start Date: 6/2/2010 Completion Date: 6/3/2010		Casing Elevation: 217.04 - NGVD 29' Surface Elevation: 215.0+/- NGVD 29' Wellhead Type: Standpipe	
						<b>Sample Description</b>		<b>Stratum Change (ft.)</b>	<b>Test Boring/ Monitoring Well Construction</b>
52	S-11	60-29	50-55	NA	5	0"-15" light brown, saturated, FINE SAND, trace silt, (mottled) As Field Testing Results	SAND		Grout 2'-51"
54						15"-29" light brown, saturated, MEDIUM TO COARSE SAND, trace fine sand, (well sorted)			Bentonite 51'-53"
56	S-12	60-18	55-60	NA	NA	Brown, saturated, FINE TO MEDIUM SAND, trace coarse sand			#2 Mottie Sand 53'-66"
58									
60									
62	S-13	60-26	60-65	NA	NA	As Field Testing Results 0"-15" Brown, saturated, FINE TO MEDIUM SAND, trace coarse sand	GRAVELLY SILT		
64						15"-29" light brown, saturated, COARSE TO MEDIUM SAND, trace fragments (angular)			1.5" Schedule 40 PVC Well screen - 0.01" slot size
66	S-14	24-15	65-67	NA	NA	(gray) moist, FINE SAND, with rock fragments (angular) (fill)			
68									
70									
72					5	As Field Testing Results			
74									
Notes: 1) Direct Push groundwater profile sampling conducted on 6/2 (6 & 6/3/10) 2) Groundwater profile sampler refusal at 72' 3) 4) 5) 6)								Key	 Cement  Drill Cuttings Native Soils  Bentonite Grout  Sand  Screen  Riser
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample ▼ = Approximate water table NA=Not Applicable NR=No Recovery lbs below ground surface ags=above ground surface									

 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-11</b>		Sheet 1 of 3		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCT Inspector: JJC/WJM		Casing: Steel Sampler: Core Barrel Size: 6" (6") Hammer: Fall NA lbs NA"		
<b>Sample Information</b> Start Date: 8/3/2010 Completion Date: 8/4/2010							Casing Elevation: 260.99 - NGVD 29' Surface Elevation: 260.35 +/- NGVD 29' Wellhead Type: Standpipe				
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/s*	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
0	S-1	60	0-5	NA	NA			Topsoil	TOPSOIL		Standpipe is 3' ags
4								Light brown, MEDIUM TO COARSE SAND, with pebbles	SAND & GRAVEL		Cement 0-2'
6	S-2	60	5-10 5-7	NA	NA			Light brown, MEDIUM SAND, with waste	SAND & WASTE		
8	S-3		7-12	NA	NA			COMPACTED WASTE (paper), some light brown medium sand			2" Schedule 40 PVC Riser 0-50'
10		60	10-15	NA	NA						
12											
14											
16	S-5	60	15-20	NA	NA			Light brown, COARSE SAND, with wood fragments			
18											
20											Grout 2'-46'
22	S-6		20-23	NA	NA			Dark brown to grey, COARSE SAND			
24											
26											
28											
30											
32											
34											
36											
38											
40											
42											
44											
46											
48											
50											
52											
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72											
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78											
80											
82											
84											
86											
88											
90											
92											
94											
96											
98											
100											







**Notes:**

- 1) Groundwater profile sampling conducted with a bladder pump
- 2)
- 3)
- 4)
- 5)
- 6)








**Remarks:**


- 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.
- 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data.
- 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample.
- ▽ = Approximate water table. NA=Not Applicable. NR=No Recovery. bgs=below ground surface. ags=above ground surface.

**Key:**

-  Cement
-  Drill Cuttings Native Soils
-  Bentonite Grout
-  Sand
-  Screen
-  Riser









<div> Sovereign Consulting Inc.</div> <div>905B South Main Street Mansfield, Massachusetts</div>							Boring Well ID: SIIM-10-11			Sheet 2 of 3		
Client: USACE Project: SIIM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCT Inspector: JJC/WJW			Casing Type: PVC Size: 6" Hammer: Fall N/A lbs: N/A"		
Sample Information							Start Date: 8/3/2010 Completion Date: 8/4/2010			Casing Elevation: 260.99 - NGVD 29' Surface Elevation: 260.35 +/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blows/6"	Field As Testing	Sample Type Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction		
26		60'	25-30	NA	NA		Light brown, COARSE SAND	SAND				
	S-8		25-33									
28												
30		60'	30-35	NA	NA		Light brown, FINE SAND	SAND				
32												
	S-9		33-35									
34							NO RECOVERY	SAND				
36		60'	35-40	NA	NA							
38												
40						80	As Field Testing Results		1			
42		60'	40-45	NA	NA		Light brown, COARSE SAND (speckled)	SAND				
	S-10		50-55									
44												
46		60'	45-50	NA	NA			SAND				
48												
50						70	As Field Testing Results		1			
Notes:										Key:		
1) Groundwater profile sampling conducted with a bladder pump.										 Cement		
2)										 Drill Cuttings Native Soils		
3)										 Bentonite Grout		
4)										 Sand		
5)										 Screen		
6)										 Riser		
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▼ = Approximate water table. NA = Not Applicable. NR = No Recovery. lbs = below ground surface. ags = above ground surface.												

 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-11</b>		Sheet 3 of 3		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCI Inspector: JJC/WJW		Casing: PVC Type: PVC Size: 4" Hammer: Fall N/A lbs.		
<b>Sample Information</b>							Start Date: 8/3/2010 Completion Date: 8/4/2010		Casing Elevation: 260.99 - NGVD 29' Surface Elevation: 260.35 +/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
52		60	50-55	NA							2" Schedule 40 PVC Well screen - 0.01" slot 50'-60'
54											
56	S-11	60	55-60	NA	NA			Light brown, MEDIUM SAND	SAND		
58											
60					150			As Field Testing Results			
62	S-12	60	60-65	NA	NA			GLACIAL Till over lying Bedrock	GLACIAL Till		
64								Bedrock is approximately 60' below			
66								As Field Testing Results	GLACIAL Till		
68								END OF BORING 65 FEET			
70											
72											
74											

**Notes:**


- 1) Groundwater profile sampling conducted with a bladder pump
- 2)
- 3)
- 4)
- 5)
- 6)

**Key:**


-  Cement
-  Drill Cuttings Native Soils
-  Bentonite Grout
-  Sand
-  Screen
-  Riser


**Remarks:**

- 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.
- 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data.
- 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample.

 Approximate water table  
 NA Not Applicable  
 NR No Recovery  
 bgs below ground surface  
 ags above ground surface



 Sovereign Consulting Inc. 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: SHM-10-12			Sheet 1 of 3		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCT Inspector: JIC/WJW			Casing: Steel Sampler: Core Barrel Type: 6" Size: 60" Hammer: Fall N/A lbs		
Sample Information Start Date: 8/5/2010 Completion Date: 8/9/2010							Casing Elevation: 254.39 - NGVD 29' Surface Elevation: 251.41 +/- NGVD 29' Wellhead Type: Standpipe					

 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring Well ID: SHM-10-12		Sheet 2 of 3		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Board Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCI Inspector: JJC/WJW		Casing: PVC Sampler: Core Barrel Type: 6" Size: 60" Hammer: Fall N/A lbs: N/A"		
<b>Sample Information</b> Start Date: 8/5/2010 Completion Date: 8/9/2010							Casing Elevation: 254.39 ± NGVD 29' Surface Elevation: 251.41 ±/- NGVD 29' Wellhead Type: Standpipe				
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
26	S-8	60	25-30	NA	NA			Light brown (5Y 8/2), MEDIUM SAND (well sorted)			
28											
30											
32	S-9	60	30-35	NA	NA			Light brown (5Y 8/2), MEDIUM SAND (well sorted)			
34											
36	S-10	60	35-40	NA	NA			Grey brown to medium grey (5Y 7/1) MEDIUM SAND			
38											
40											
42	S-11	60	40-45	NA	NA			Light Grey (5Y 6/2) MEDIUM SAND			
44	S-12		42-45					Medium grey (5Y 6/2), COARSE SAND (well sorted)			
46		60	45-50	NA	NA			As Field Testing Results			
48	S-13		45-52					Medium grey (5Y 6/2), COARSE SAND (well sorted)			
50											

**Notes:**







- 1) Groundwater profile sampling conducted with a bladder pump
- 2)
- 3)
- 4)
- 5)
- 6)

**Remarks:**


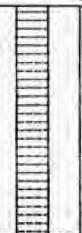
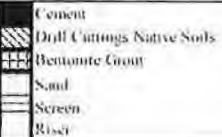
- 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.
- 2) Field As testing values represent arsenic concentrations in mg/l, collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data.
- 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample.
- 4) Sample is designated as either "C" for composite or "G" for a discrete grab sample.

▼ = Approximate water table    NA = Not Applicable    NR = No Recovery    bgs = below ground surface    ags = above ground surface

**Key:**

-  Cement
-  Drill Cuttings Native Soils
-  Bentonite Grout
-  Sand
-  Screen
-  Riser



 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts						Boring/Well ID: <b>SIIM-10-12</b>		Sheet 3 of 3			
Client: USACE Project: SIIL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA						Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCT Inspector: JJC/WJW		Casing: PVC Sampler: Core Barrel Size: 6" Hammer: Fall SCA lbs: NA*			
<b>Sample Information</b>						Start Date: 8/5/2010 Completion Date: 8/9/2010		Casing Elevation: 254.39 - NGVD 29' Surface Elevation: 251.41 +/- NGVD 29' Wellhead Type: Standpipe			
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
52		60	50-55	NA	NA						
54	S-14		52-55					Light brown (5Y 8/3), MEDIUM SAND			
56	S-15	60	55-60	NA	NA			As Field Testing Results: Light brown (5Y 8/3), COARSE SAND	SAND		
58											
60	S-16	60	60-65	NA	NA			GLACIAL FILL	GLACIAL FILL		
62											
64								As Field Testing Results			
66		60	65-70	NA	NA			GLACIAL FILL overlying Bedrock			
68								BEDROCK approximately 70 feet			
70									BEDROCK		
72											
74											
Notes: 1) Groundwater profile sampling conducted with a bladder pump. 2) 3) 4) 5) 6)										Key: 	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▼ = Approximate water table. NA = Not Applicable. NR = No Recovery. bgs = below ground surface. ags = above ground surface.											


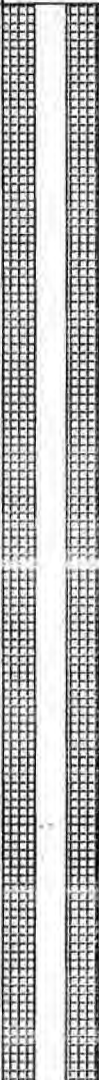
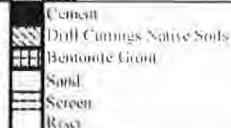
Sovereign Consulting Inc. 905B South Main Street Mansfield, Massachusetts		Boring/Well ID: SHM-10-13		Sheet 1 of 4	
Client: USACE Project: SHM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCT Inspector: JJC/WJW		Casing: Steel Sampler: Core Barrel Type: 6" x 6" Size: 6" x 6" Hammer: N/A lbs Fall: N/A'	
Start Date: 8/9/2010 Completion Date: 8/10/2010		Casing Elevation: 244.52- NGVD 29' Surface Elevation: 241.18 +/- NGVD 29' Wellhead Type: Standpipe			
Sample Information		Sample Description		Stratum Change (ft.)	
Depth	Sample ID	Pen./Rev. (in.)	Interval (ft.)	Blow/6"	Field As Testing
2	S-1	60	0-5	NA	NA
4					
6	S-2	100	5-10	NA	NA
8					
10	S-3		8-10		
12	S-4	140	10-15	NA	NA
14					
16	S-5	140	15-20	NA	NA
18	S-6				
20	S-7		17-20		
22	S-8		20-23		
24	S-9		23-25		








Sample Description		Stratum Change (ft.)		Notes	
Medium gray (5Y 7/2), COARSE SAND, with pebbles, (poorly sorted)		SAND		Standpipe is 3' ags	
Dark gray (5Y 6/2), COARSE SAND		SAND & ASH		Cement 0-2'	
(5Y 7/2), COARSE SAND, with wood and ash		SAND & GRAY CL		2" Schedule 40 PVC Riser 0-60'	
Light gray (5Y 7/2), COARSE SAND, with pebbles		SAND, ASH & DEBRIS		Grout 2'-56'	
Light brown (5Y 8/2), MEDIUM SAND, with pebbles					
Light grey (5Y 8/1), FINE SAND					
Light brown (5Y 6/2), MEDIUM SAND					
Dark grey (5Y 5/1), MEDIUM SAND, with ash and glass					


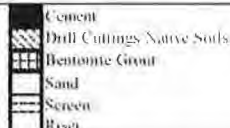
Notes:		Key:	
1) Groundwater profile sampling conducted with a bladder pump		Cement	
2)		Drill Cuttings Native Soils	
3)		Benotone Grout	
4)		Sand	
5)		Screen	
6)		Riser	

Remarks:	
1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made	
2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data	
3) Sample is designated as either "C" for composite or "G" for a discrete grab sample	
4) Approximate water table: N/A=Not Applicable, NR=No Recovery, bgs=below ground surface, ags=above ground surface	





 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts		Boring Well ID: <b>SHM-10-13</b>		Sheet 2 of 4								
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCI Inspector: JJC/WJW		Casing: PVC Type: PVC Size: 6" Hammer: Fall SA lbs: SA"								
Sample Information		Start Date: 8/9/2010 Completion Date: 8/10/2010		Casing Elevation: 244.52- NGVD 29' Surface Elevation: 241.18 +/- NGVD 29' Wellhead Type: Standpipe								
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction	
26	S-10	60	25-30 25-27	NA	NA			Brown (5Y 8/2), MEDIUM SAND	SAND		 2" Schedule 40 PVC Riser 0-60'	
28	S-11		27-30					Dark brown (5Y 4/2), PEAT (thick)	PEAT			
30												
32	S-12	60	30-35 30-32	NA	NA			Dark brown (5Y 4/3), PEAT, with medium SAND	SAND			
34	S-13		32-35					Medium brown (5Y 5/6), PEAT, with medium sand, (less peat 25%)				
36	S-14	60	35-40	NA	NA			Medium brown grey (5Y 6/2), MEDIUM SAND (well sorted)	SAND			
38												
40					As			As Field Testing Results	SAND			
42	S-15	60	40-45	NA	NA			Medium brown grey (5Y 6/2) FINE SAND (well sorted)				
44									SAND			
46		60	45-50	NA	NA			POOR RECOVERY				
48									SAND			
50					As			As Field Testing Results				
Notes: 1) Groundwater profile sampling conducted with a bladder pump 2) 3) 4) 5) 6)												Key: 
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▼ Approximate water table. NA Not Applicable. NR No Recovery. lbs=below ground surface. ags=above ground surface.												

<div> Sovereign Consulting Inc.</div> <div>905B South Main Street Mansfield, Massachusetts</div>						Boring/Well ID: SIIM-10-13				Sheet 3 of 4						
Client: USACE Project: SIH, - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA						Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCT Inspector: JJC/WJW				Casing: PVC Type: PVC Size: 16" Hammer: Fall SNA lbs: SNA						
Start Date: 8/9/2010 Completion Date: 8/10/2010						Casing Elevation: 244.52- NGVD 29' Surface Elevation: 241.18 +/- NGVD 29' Wellhead Type: Standpipe										
Sample Information						Sample Description				Stratum Change (ft.)		Notes		Test Boring/ Monitoring Well Construction		
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/ft.	Field As Testing	Sample Type	Water Detected									
52	S-16	60	50-55	NA	NA			Light brown grey, (SY 8.1), FINE SAND (well sorted)	SAND					Gravel 2'-5ft		
54																
56		60	55-60	NA	NA											
58	S-17		55-67					Light grey (SY 7.2), COARSE SAND							Bentonite 5ft-58"	
60					100			As Field Testing Results	SAND					#2 Motor Sand 58'-60'		
62		60	60-65	NA	NA											
64																
66		60	65-70	NA	NA										2" Schedule 40 PVC Well screen = 0.075" slot 100'-70'	
68	S-18		67-70					Light brown yellow (SY 8.3), FINE SAND	SAND & GRAVEL							
70					>500			As Field Testing Results								
72	S-19		70-72					Medium brown (SY 7.5), MEDIUM SAND, with pebbles								
74								Dark brown water (SY 7.6) MEDIUM SAND with pebbles								
Notes: 1) Groundwater profile sampling conducted with a bladder pump. 2) 3) 4) 5) 6)												Key: <div> Cement</div> <div> Drill Cuttings Native Soils</div> <div> Bentonite Grout</div> <div> Sand</div> <div> Screen</div> <div> Riser</div>				
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l, collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▼ Approximate water table. NA: Not Applicable. NR: No Recovery. bgs: below ground surface. ags: above ground surface.																

 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts		Boring Well ID: <b>SHM-10-13</b>		Sheet 4 of 4							
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCI Inspector: JJC/WJW		Casing: PVC Sampler: Core Barrel Type: 6" Size: 60" Hammer: Fall Nails: NA							
<b>Sample Information</b>		Start Date: 8/9/2010 Completion Date: 8/10/2010		Casing Elevation: 244.52- NGVD 29' Surface Elevation: 241.18 +/- NGVD 29' Wellhead Type: Standpipe							
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
76		60	75-80	NA	NA				SAND & GRAVEL		
	S-21		75-77					Medium brown (5Y 7-4), MEDIUM SAND, with pebbles			
78	S-22		77-80					Medium brown (5Y 7-2), MEDIUM SAND	SAND		
					20			As Field Testing Results			
80		60	80-85	NA	NA			GLACIAL TILL (5Y 8-3)	GLACIAL TILL		
82											
84											
	24		85-87	NA	NA			BEDROCK	BEDROCK		
88											
								END OF BORING 87 FEET			
90											
92											
94											
96											
98											
100											
Notes: 1) Groundwater profile sampling conducted with a bladder pump. 2) 3) 4) 5) 6)										Key:	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA=Not Applicable. NR=No Recovery. bgs=below ground surface. ags=above ground surface.											





 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts		Boring Well ID: <b>SIIM-10-14</b>		Sheet 1 of 4	
Client: USACE Project: SIIL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCT Inspector: JJC/AJW Start Date: 8/16/2010 Completion Date: 8/17/2010		Casing: Steel Sampler: Core Barrel Type: 6" Size: 6" Hammer: Fall N/A lbs: N/A"	
<b>Sample Information</b> Depth Sample ID Pen./Rec. (in.) Interval (Ft.) Blow/6" Field As Testing Sample Type Water Detected		Casing Elevation: 237.43 ± NGVD 29' Surface Elevation: 234.62 ± NGVD 29' Wellhead Type: Standpipe		<b>Test Boring/ Monitoring Well Construction</b> Standpipe is 3" i.d. Cement 0-2' 2" Schedule 40 PVC Riser 0-60' Grout 2'-56'	
		<b>Sample Description</b> Medium brown (5Y 7/2) COARSE SAND, with pebbles. (poorly sorted)		<b>Stratum Change (ft.)</b> SAND & GRAVEL	
		Medium brown (5Y 7/8), SAND, with pebbles			
		Medium brown (5Y 4/1), SAND, with waste, paper and glass			
		Dark grey (5Y 4/3), WASTE (paper and glass) with sand			
		Dark grey (5Y 4/3), SAND, Ash, waste, glass		SAND, ASH & WASTE	
		Medium brown (5Y 7/2) SAND			
Notes: 1) Groundwater profile sampling conducted with a bladder pump. 2) 3) 4) 5) 6)		Key: <ul style="list-style-type: none"> <li>Cement</li> <li>Drill Cuttings Native Soils</li> <li>Benotite Grout</li> <li>Sand</li> <li>Screen</li> <li>Riser</li> </ul>			
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in µg/l, collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▼: Approximate water table. NA: Not Applicable. NR=No Recovery. bgs: below ground surface. ags: above ground surface.					

<div> Sovereign Consulting Inc.</div> <div>905B South Main Street Mansfield, Massachusetts</div>										Boring Well ID: SHM-10-14										Sheet 2 of 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Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA										Drilling Co.: Bort Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCI Inspector: JJC/WJW										Casing: PVC Sampler: Core Barrel Type: 6" Size: 6" Hammer: Fall N/A lbs: 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 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts								Boring Well ID: SHM-10-14		Sheet 4 of 4	
Client: USACE Project: SHM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA								Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCI Inspector: JJC/WJW		Casing: Steel Type: Steel Size: 6" Hammer: Fall NA lbs: NA"	
<b>Sample Information</b> Start Date: 8/16/2010 Completion Date: 8/17/2010								Casing Elevation: 237.43 - NGVD 29' Surface Elevation: 234.62 +/- NGVD 29' Wellhead Type: Standpipe			
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
76	S-18	60'	75-80	NA	NA			Tight (5Y 7.2) FINE SAND	SAND		 #2 Moore Sand 58'-80'  2" Schedule 40 PVC Well screen / 0.01" slot 60'-80'
78								As Field Testing Results			
80		50'	80-85	NA	NA			GLACIAL TILL (5Y 8.3)	GLACIAL TILL		
82											
84											
86		40'	85-90	NA	NA			GLACIAL TILL (5Y 8.3)			
88											
90		40'	90-95	NA	NA			BEDROCK (7.5Y 7.1)	BEDROCK		
92											
94											
96								END OF BORING 96 FEET			
98											
100											

**Notes:**







- 1) Groundwater profile sampling conducted with a bladder pump
- 2)
- 3)
- 4)
- 5)
- 6)


**Remarks:**

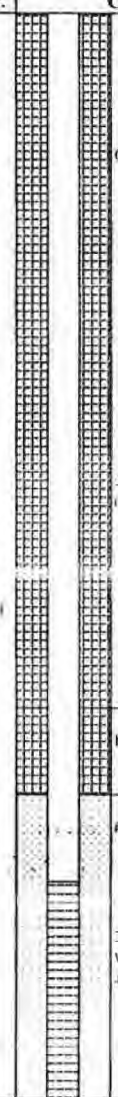






- 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.
- 2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data.
- 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample.

 ≈ Approximate water table  
 NA=Not Applicable  
 NR=No Recovery  
 bgs= below ground surface  
 ags= above ground surface



**Key:**

	Cement
	Drill Cuttings Native Soils
	Bentonite Grout
	Sand
	Screen
	Riser

<div> Sovereign Consulting Inc.</div> <div>905B South Main Street Mansfield, Massachusetts</div>						Boring/Well ID: SHM-10-15			Sheet 1 of 3		
Client: USACE Project: SHM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA						Drilling Co.: Bort Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCI Inspector: JJC/WJW			Casing Type: Steel Sampler: Core Barrel Size: 6" Hammer: Fall SCL lbs: N/A		
<div>Sample Information</div> <div><div>Depth</div><div>Sample ID</div><div>Pen/Rec (in.)</div><div>Interval (Ft.)</div><div>Blow/6"</div><div>Field As Testing</div><div>Sample Type</div><div>Water Detected</div></div>						Start Date: 8/11/2010 Completion Date: 8/11/2010			Casing Elevation: 243.47 - NGVD 29' Surface Elevation: 241.89 +/- NGVD 29' Wellhead Type: Standpipe		
						Sample Description		Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction	
2	S-1	60	0-5 0-4	NA	NA		Light (SY 7 1), MEDIUM SAND (poorly sorted)	SAND		Standpipe is 3' ags Cement 0-2"	
4	S-2		4-5				Light (SY 7 1), WASTE AND SAND	SAND & WASTE			
6	S-3	60	5-10	NA	NA		Light (SY 7 1), WASTE AND SAND				
8											
10	S-4	60	10-15	NA	NA		Light (SY 5 1), WASTE AND ASH	SAND, ASH & WASTE		2" Schedule 40 PVC Riser 0-45'	
12								SAND & WASTE			
14											
16	S-5	60	15-20 15-17	NA	NA		(SY 4 4), MEDIUM SAND, some waste				
18	S-6		17-18				(SY 5/6), MEDIUM SAND, some waste	SAND & WASTE			
20	S-7		18-20'				(SY 4/2), MEDIUM SAND, some waste				
22	S-8	100	20-25	NA	NA		Dark brown (SY 4 4), SAND, with pebbles, some waste			Grout 2'-41"	
24											
Notes						Key					
1) Groundwater profile sampling conducted with a bladder pump						<div><div>Cement</div><div>Drill Cuttings Native Soils</div><div>Bentonite Grout</div><div>Sand</div><div>Screen</div><div>Riser</div></div>					
Remarks						1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample ▼: Approximate water table NA: Not Applicable NR: No Recovery bgs=below ground surface ags: above ground surface					

Sovereign Consulting Inc. 905B South Main Street Mansfield, Massachusetts							Boring Well ID: SHM-10-15		Sheet 2 of 3			
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCI Inspector: JJC/WJW Start Date: 8/11/2010 Completion Date: 8/11/2010		Casing: Sampler Type: PVC Size: 6" Cote Barrel: 60" Hammer: Full S.A. lbs: N/A"			
Sample Information									Casing Elevation: 243.47 - NGVD 29' Surface Elevation: 241.89 +/- NGVD 29' Wellhead Type: Standpipe			
Depth	Sample ID	Pen./Rec. (in.)	Interval (Ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction	
26	S-9	60	25-30 25-28	NA	NA			Black (5Y 3/4), MEDIUM SAND with pebbles, odor (creosote)	SAND & WASTE			Ground 2'-4"
28	S-10		28-30					Brown (5Y 6/2), MEDIUM SAND	SAND			
30	S-11	60	30-35	NA	NA			Brown (5Y 7/6), MEDIUM SAND (orange stains)			2" Schedule 40 PVC Risers 0-45'	
32												
34											2" Schedule 40 PVC Risers 0-45'	
36	S-12	60	35-40	NA	NA			Brown (5Y 7-4), MEDIUM SAND (orange stains)	SAND			
38											2" Schedule 40 PVC Risers 0-45'	
40								As Field Testing Results				
42	S-13	60	40-45	NA	NA			Light Brown (5Y 7/1), MEDIUM SAND			Bentinite 41'-43'	
44												
46		60	45-50	NA	NA			Light Brown (5Y 7-4), MEDIUM SAND	SAND		#2 Movie Sand 43'-55' +/-	
48												
50											2" Schedule 40 PVC Well screen - 0.01" slot 45'-55'	
Notes										Key		
1) Groundwater profile sampling conducted with a bladder pump 2) 3) 4) 5) 6)										 Cement  Drill Cuttings Native Soils  Bentinite Grout  Sand  Screen  Riser		
Remarks												
1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. ▼ = Approximate water table. NA=Not Applicable. NR=No Recovery. bgs=below ground surface. ags=above ground surface.												









 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring/Well ID: <b>SHM-10-15</b>		Sheet 3 of 3		
Client: U.S.A.C.I. Project: SHM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCI Inspector: JJC/WJW		Casing: PVC Sampler: Copy Barrel Size: 6" Hammer: Fall S.A. lbs: N/A		
<b>Sample Information</b> Start Date: 8/11/2010 Completion Date: 8/11/2010							Casing Elevation: 243.47 - NGVD 29' Surface Elevation: 241.89 +/- NGVD 29' Wellhead Type: Standpipe				
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	 Test Boring/ Monitoring Well Construction
52		60	50-55	NA				Light Brown (5Y 7-4), MEDIUM SAND	SAND		#2 More Sand 43'-55'  2" Schedule 40 PVC Well screen - 0.01" slot 45'-55'
54											
56	S-14	60	55-60	NA	NA			Light Tan (7.5Y 8-1), GLACIAL TILL	GLACIAL TILL		
58											
60					80			As Field Testing Results			
62		46	60-65	NA	NA			BEDROCK	BEDROCK		
64								EXTEND BORING TO 111'			
66											
68											
70											
72											
74											

**Notes**

- 1) Groundwater profile sampling conducted with a bladder pump
- 2)
- 3)
- 4)
- 5)
- 6)

**Key**

-  Cement
-  Drill Cuttings Native Soils
-  Bentonite Grout
-  Sand
-  Screen
-  Riser

**Remarks**









1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.

2) Field As testing values represent arsenic concentrations in ug/l collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data.

3) Sample is designated as either "C" for composite or "G" for a discrete grab sample.


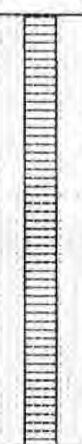
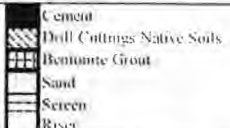
▼ Approximate water table. NA=Not Applicable. NR=No Recovery. bgs=below ground surface. ags=above ground surface.



 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts		Boring Well ID: <b>SHM-10-16</b>		Sheet 2 of 4							
Client: USACE Project: SHM - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA		Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCT Inspector: JC/WJW		Casing: PVC Sampler: Cone Barrel Size: 6" Hammer: Fall NA lbs: NA"							
<b>Sample Information</b>		Start Date: 8/17/2010 Completion Date: 8/19/2010		Casing Elevation: 219.04 - NGVD 29' Surface Elevation: 216.50 +/- NGVD 29' Wellhead Type: Standpipe							
Depth	Sample ID	Pen/Rec. (in.)	Interval (ft.)	Blow/6'	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
26	S-4	60	25-30 25-29	NA	NA			Dark (5Y 5-4), COARSE SAND	SAND	1	 2" Schedule 40 PVC Riser 0-75'
28	S-5		29-30					Orange (5Y 6-8), COARSE SAND			
30		60	30-35	NA	NA			Yellow (5Y 8-3), COARSE SAND			
32	S-6		30-36					As Field Testing Results			
34					5				SAND	1	
36		60	35-40	NA	NA						
38	S-7		30-40					Light grey (5Y 7-1), MEDIUM SAND			
40											
42		60	40-45	NA	NA			ROCK (5Y 7-1)	BOULDER		Grout 2-7 1/2'
44											
46		60	45-50	NA	NA			ROCK (5Y 7-1)			
48											
50											
Notes: 1) Groundwater profile sampling conducted with a bladder pump 2) 3) 4) 5) 6)										Key:  Cement  Drill Cuttings Native Soils  Bentonite Grout  Sand  Screen  Riser	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in mg/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA=Not Applicable. NR=No Recovery. bgs: below ground surface. ags: above ground surface.											





 <b>Sovereign Consulting Inc.</b> 905B South Main Street Mansfield, Massachusetts							Boring Well ID: <b>SHM-10-16</b>		Sheet 4 of 4		
Client: USACE Project: SHL - Fort Devens Project Number: AC001 Location: Fort Devens Ayer, MA							Drilling Co.: Boart Longyear Drill Rig: Mini Sonic Drill Method: Rotary-Vibratory Foreman: Fred Lavoie SCT Inspector: JJC/WJW		Casing: PVC Sampler: Cone Barrel Type: 6" Size: 60" Hammer: Fall NA lbs		
<b>Sample Information</b>							Start Date: 8/17/2010 Completion Date: 8/19/2010		Casing Elevation: 219.04 - NGVD 29' Surface Elevation: 216.50 +/- NGVD 29' Wellhead Type: Standpipe		
Depth	Sample ID	Pen./Rec. (in.)	Interval (ft.)	Blow/6"	Field As Testing	Sample Type	Water Detected	Sample Description	Stratum Change (ft.)	Notes	Test Boring/ Monitoring Well Construction
76		60	75-80	NA	NA						
78											
80	S-13	60	80-85 80-93	NA	NA			Light (SY 7/1), MEDIUM SAND			
82											
84					100			As Field Testing Results			
86		60	85-90	NA	NA						
88											
90											
92											
94					D			As Field Testing Results GLACIAL TILL (SY 7/3)	GLACIAL TILL		
96								BEDROCK (SY 7/1)	BEDROCK		
98								END OF BORING 96 FEET			
Notes: 1) Groundwater profile sampling conducted with a bladder pump 2) 3) 4) 5) 6)										Key: 	
Remarks: 1) Stratification lines represent approximate boundaries between soil types and the transition may be gradual. Water level readings were completed at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. 2) Field As testing values represent arsenic concentrations in ug/L collected using Industrial Test Systems Arsenic Quick Test Kits. Additionally, samples were collected at the same depth interval and submitted to a laboratory for testing. Please see tables for laboratory data. 3) Sample is designated as either "C" for composite or "G" for a discrete grab sample. 4) Approximate water table. NA=Not Applicable. NR=No Recovery. bgs=below ground surface. ags=above ground surface.											





## Attachment B

## **Attachment B**

Seismic Refraction Survey Report  
Devens  
Ayer, Massachusetts

Prepared for  
SOVEREIGN CONSULTING, INC.  
July 2010



# GEOPHYSICAL APPLICATIONS INCORPORATED

July 29, 2010

Mr. Neil Schofield  
SOVEREIGN CONSULTING, INC.  
905B South Main Street  
Unit 202  
Mansfield, MA 02048

Subject: Seismic Refraction Survey Report  
Devens  
Ayer, Massachusetts

Dear Mr. Schofield:

Geophysical Applications, Inc. conducted a seismic refraction survey to help ascertain bedrock depths and elevations at specific locations designated by Sovereign, at the above-noted site.

## **METHODS OF INVESTIGATION**

### Survey Control

Sovereign's surveyor pre-staked three seismic lines prior to data acquisition. Along these three seismic lines, Geophysical Applications' personnel marked the seismic shot points with spray paint (on pavement or other hard surfaces) and labeled pin flags (on soft ground). Horizontal survey control along the seismic traverses (approximately every 100 feet) was provided by Sovereign's surveyors. Vertical control was provided by Geophysical Applications.

The three seismic traverse locations are shown as red lines on Figure 1. Note that the distance stations in red on Figure 1 are those utilized by our field personnel: they represent distances along the ground surface, as determined by our geophone cables.

Distance stations noted on the surveyor's stakes are shown along the ground surface on each seismic cross section. Distance stations used during data acquisition and modeling are shown at the bottom of each seismic cross section. Note that the surveyor's stations along Line B, northeast of approximately geophone station 1125, have a minus sign as a prefix.

### Seismic Refraction Profiling

Refraction profiling was performed along each designated traverse to profile stratigraphic horizons, particularly the bedrock surface.

Refraction data were acquired along 3,900 linear feet of traverse using an EG&G Strataveiw seismograph. Each 24-channel geophone array was 250 feet long with 10-foot geophone spacings. Geophones were coupled to the ground surface with spike bases on soft ground, and tripod bases on pavement or hard ground.

Either a Betsy seisgun or a 450-pound accelerated weight-drop device generated seismic energy at each shot point for this survey. Whenever possible we used the 450-pound weightdrop as the energy source.

A Betsy firing rod was used primarily at shot points that were inaccessible to the trailer-mounted weight-drop device. The firing rod was placed in shot holes driven 1 or 2 feet deep with a steel bar and sledgehammer to enhance recorded energy and minimize airborne noise. The weight-drop device strikes an aluminum impact plate on the ground surface. A geophone on the Betsy firing rod or adjacent to the weight-drop impact plate initiated seismic data recording.

Refraction seismograms were recorded using 0.25-millisecond sampling intervals, with record length of 256 milliseconds. Seismograms were reviewed in the field, and stored on the Strataveiw's internal hard drive and on floppy diskette for backup data storage.

Shot points were usually located at roughly 85-foot intervals along each traverse, with additional shots placed outside the traverse endpoints (where possible) to more accurately profile bedrock near the traverse endpoints. Five to seven shot points were occupied along each geophone array to provide reversed seismic profiles. Each shot point was marked with either spray paint or a labeled pin flag. These labels and flags were left in place at the survey's conclusion.

Refraction data analysis was performed by measuring compressional (P-wave) first-arrival times with WinSism11 software, followed by modeling with Rimrock Geophysics' SIPT2 delay-time interpretation software. This software uses a ray-tracing algorithm, in which calculated layer thickness beneath each geophone is varied to optimize agreement between observed and modeled arrival times. Time-distance plots were reviewed and selected layer depths manually calculated with the crossover-distance technique as a quality assurance check.

### **SURVEY LIMITATIONS**

The southwest section of this site had large changes in ground surface elevation that could have caused some error in layer-depth calculations. We surveyed vertical elevation along each seismic line to within ½ foot to minimize ground surface elevation effect on the model.

Seismic survey depth calculations are typically accurate within  $\pm 10\%$  (or  $\pm 3$  feet, whichever is larger) for cross-sections presented in this report.

Weathered bedrock or overburden layers (especially glacial till) too thin to be detected by seismic profiling may be present along any of the interpreted bedrock surfaces shown on the attached cross sections.

Seismic velocity values shown on the cross sections were calculated over 24-channel geophone arrays, and therefore represent averaged subsurface conditions. Localized low-velocity zones (e.g. discrete bedrock joints or fractures) occur naturally and may be present at this site.

### **RESULTS**

Three seismic traverses covering 3,900 linear feet were performed during this survey, at positions represented by red lines on Sovereign's accompanying plan map (Figure 1). Cross sections depicting interpreted subsurface stratigraphy are presented on Figures 2 through 4. Gaps along each traverse (e.g. Line A between Stations 250 through 412 feet) were due to flooded swampland.

Most seismic cross sections show three interpreted velocity layers. The uppermost layer exhibited compressional seismic velocity values of approximately 1,000 to 1,500 feet per second (ft/sec), probably representing dry, unconsolidated overburden or fill.

Calculated velocity values for the second layer were approximately 5,000 ft/sec. This velocity is judged to represent water-saturated overburden.

The deepest layer is interpreted to represent bedrock, with velocity values averaging mostly between approximately 15,100 to 16,400 feet per second, indicative of competent bedrock with little weathering or fracturing.

Note that the overall range of seismically-inferred bedrock depths and elevations exhibit good agreement with bedrock refusal depths observed at direct-push wells SHM10-2, SHM10-03, SHM10-04, and SHM10-08.

Variances between seismically-modeled bedrock depths and push-rod refusals depths may be due to the following;

- 1) the push rods may have either bent or deflected slightly along the bedrock surface, thus giving slightly deeper "apparent" refusal depths;
- 2) ground elevations at each well were not known at the time this report was prepared, therefore we assumed approximate ground elevations at each well; and
- 3) most wells were offset slightly from the seismic traverses.

\* \* \* \* \*

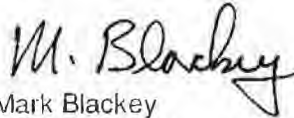
Please call the undersigned at 508/429-2430 if you have questions regarding our report. We appreciate this opportunity to provide geophysical services to Sovereign and we welcome inquiries regarding this survey.

Sincerely,

GEOPHYSICAL APPLICATIONS, INC.



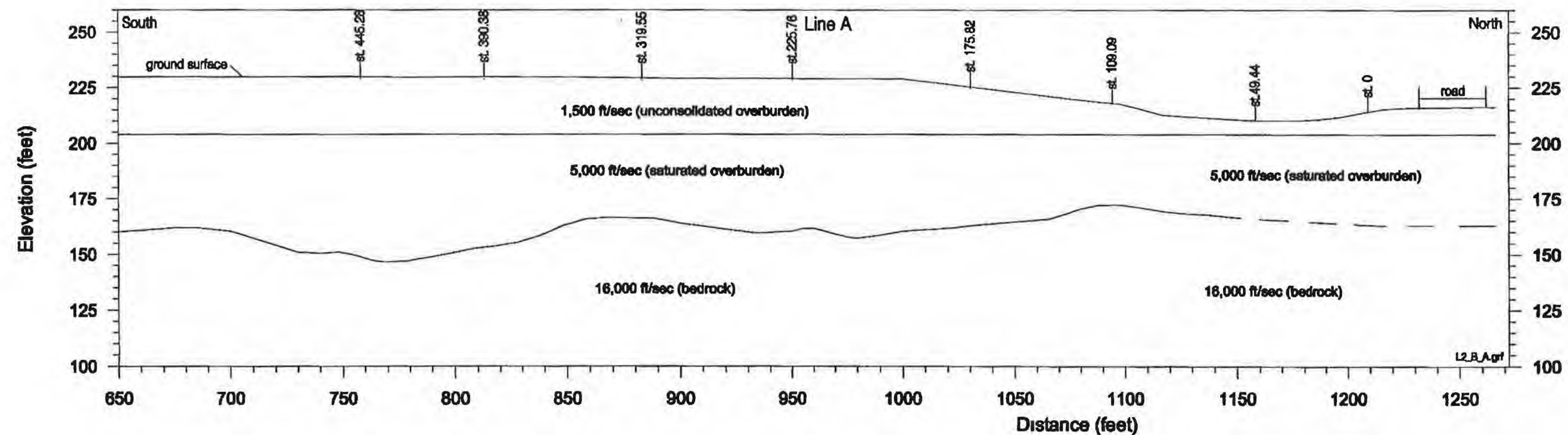
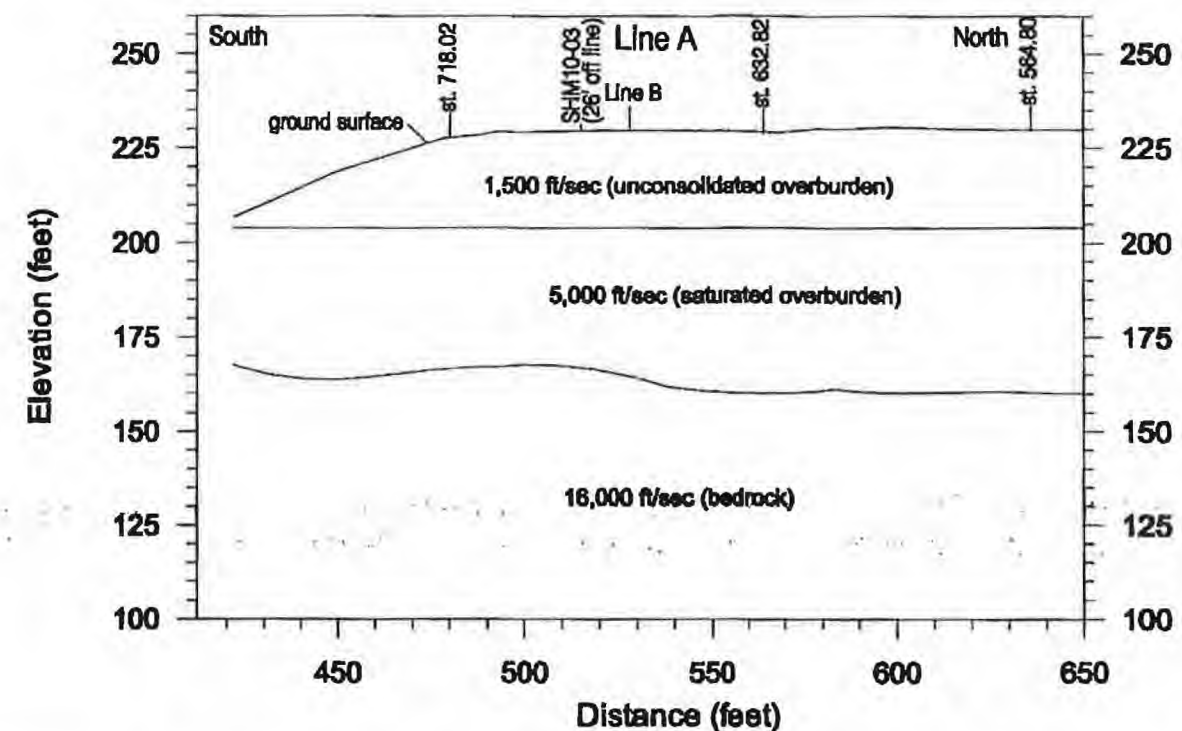
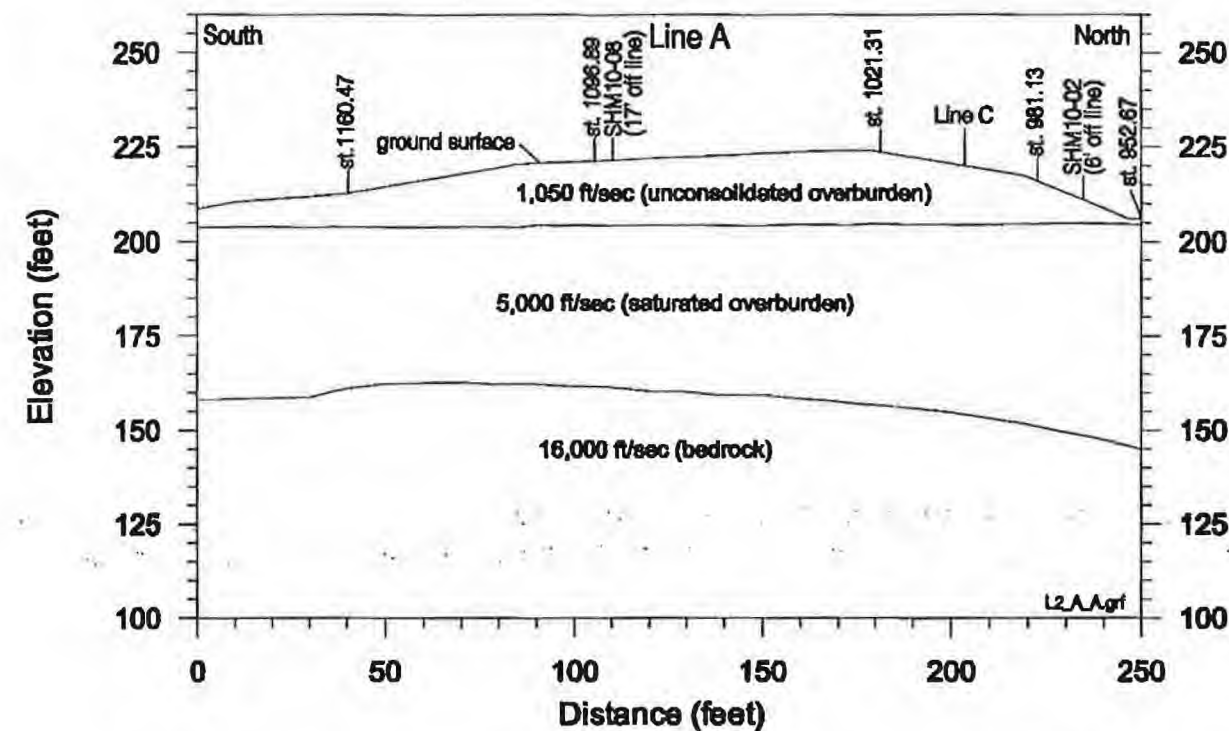
Peter Giger  
Geophysicist



Mark Blackey  
Principal and Geophysicist

1101225





**Notes:**

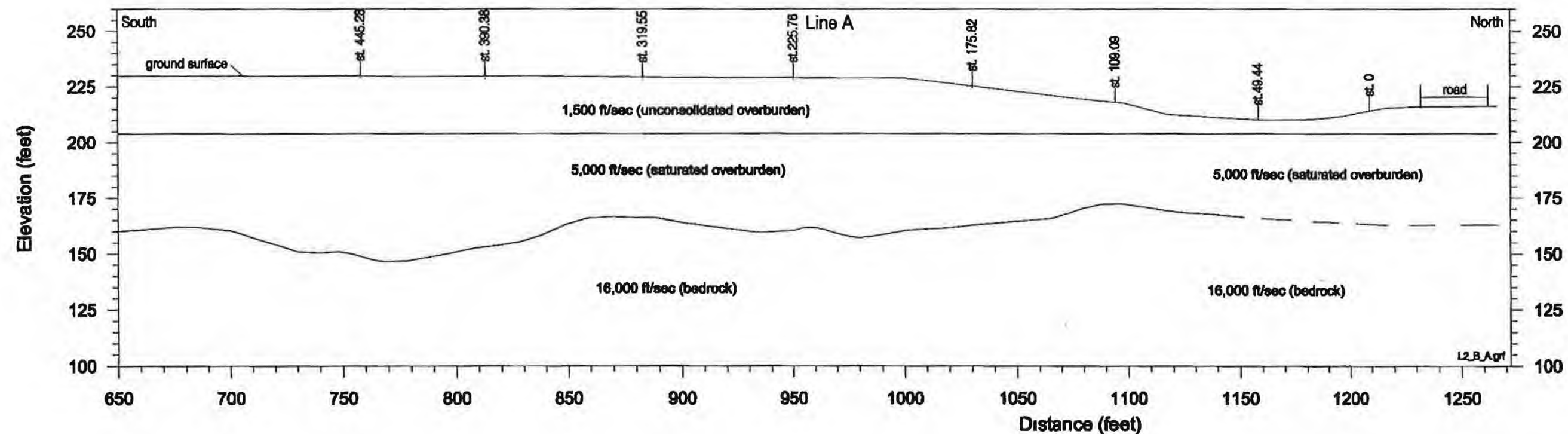
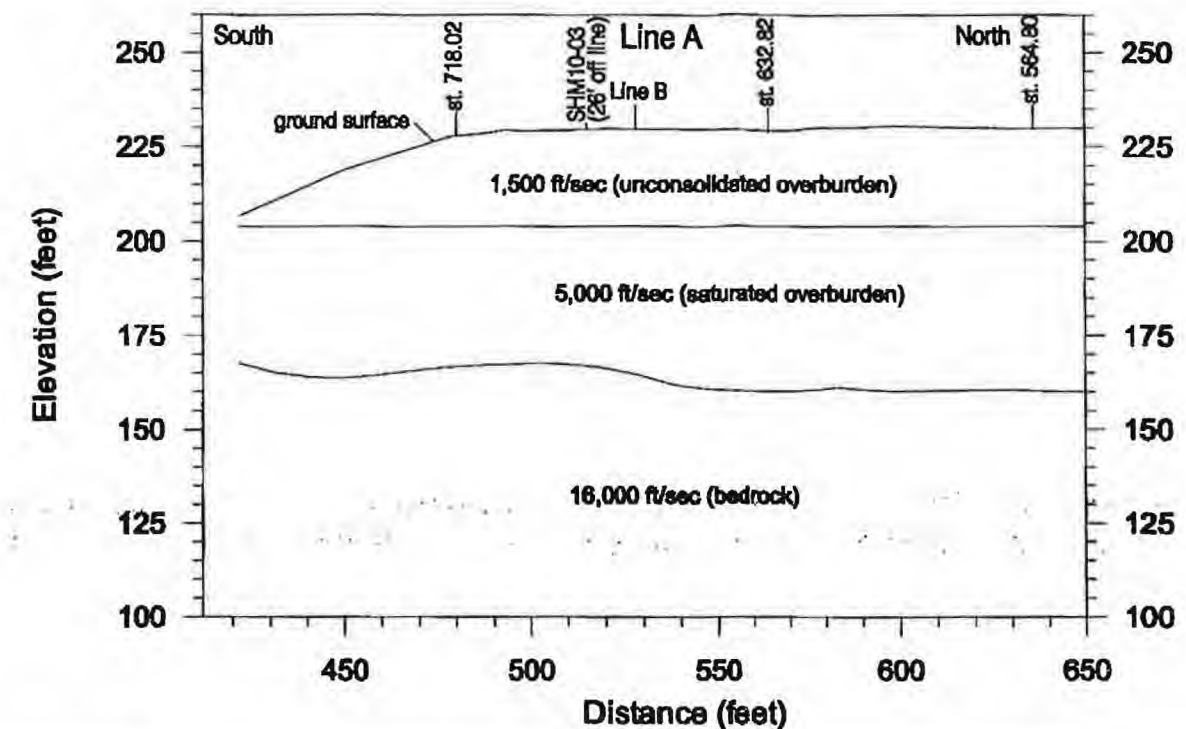
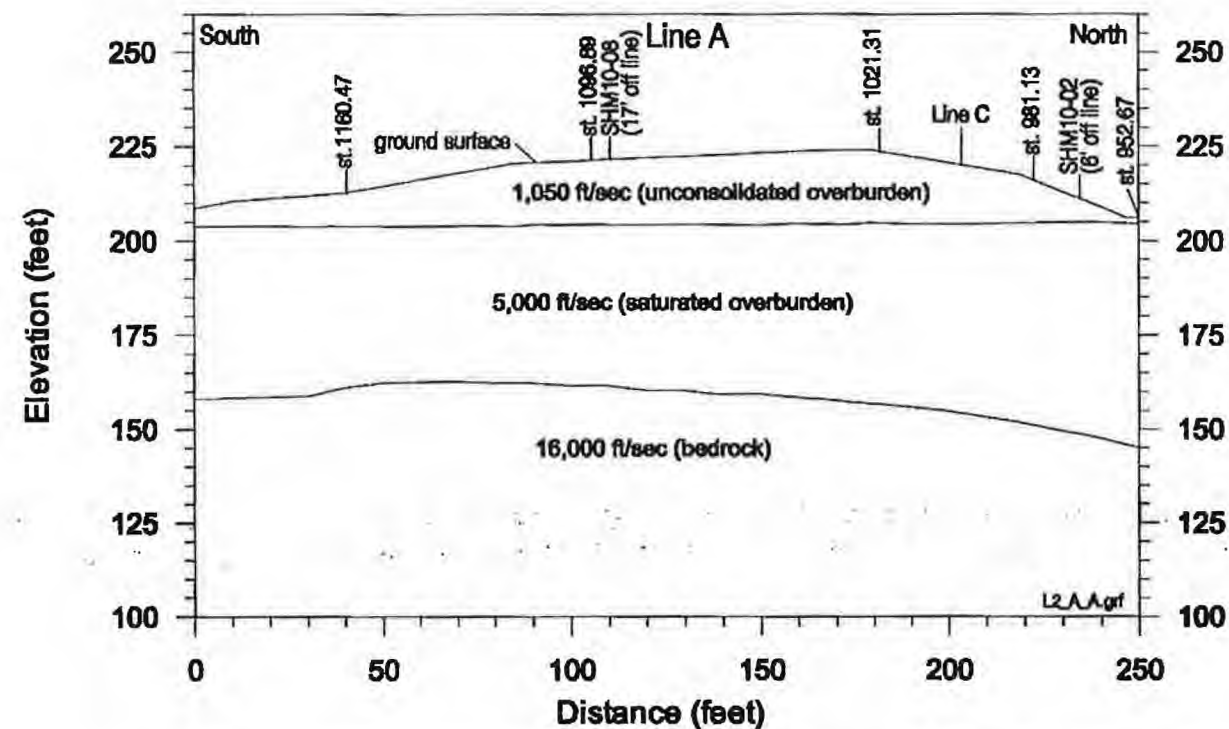
- 1) Seismic velocity values are in units of feet per second (ft/sec)
- 2) Horizontal scale, 1 inch = 50 feet  
Vertical scale, 1 inch = 50 feet  
Vertical exaggeration 1:1

- 3) Elevations were referenced to TBM A2, A3, and C1  
TBM A2 elevation is 230.74 feet  
TBM A3 elevation is 222.70 feet  
TBM C1 elevation is 239.62 feet

1101226 - 1101225cross.dwg  
last modified 07/21/10

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INCORPORATED**

Figure 2, Line A  
Seismic Cross Sections  
Devens  
Ayer, Massachusetts  
prepared for  
**SOVEREIGN CONSULTING, INC.**



**Notes:**

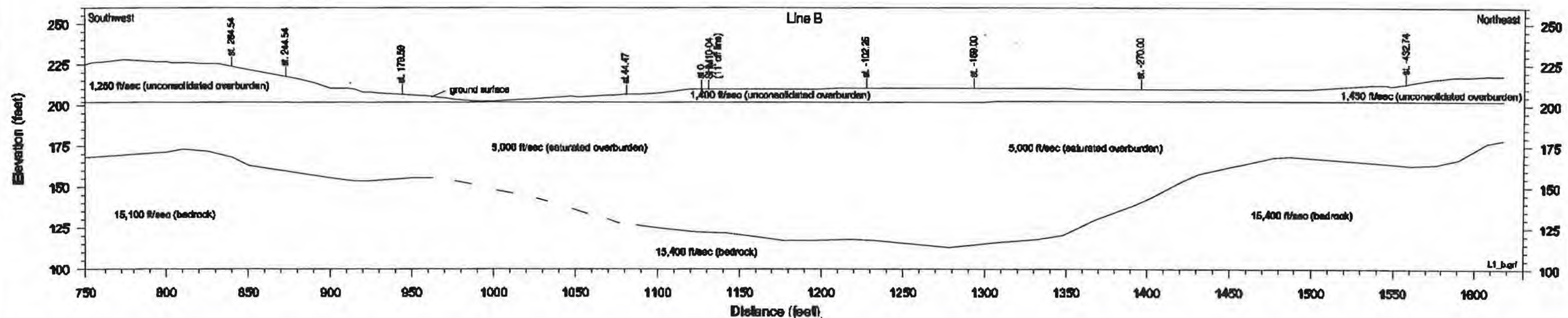
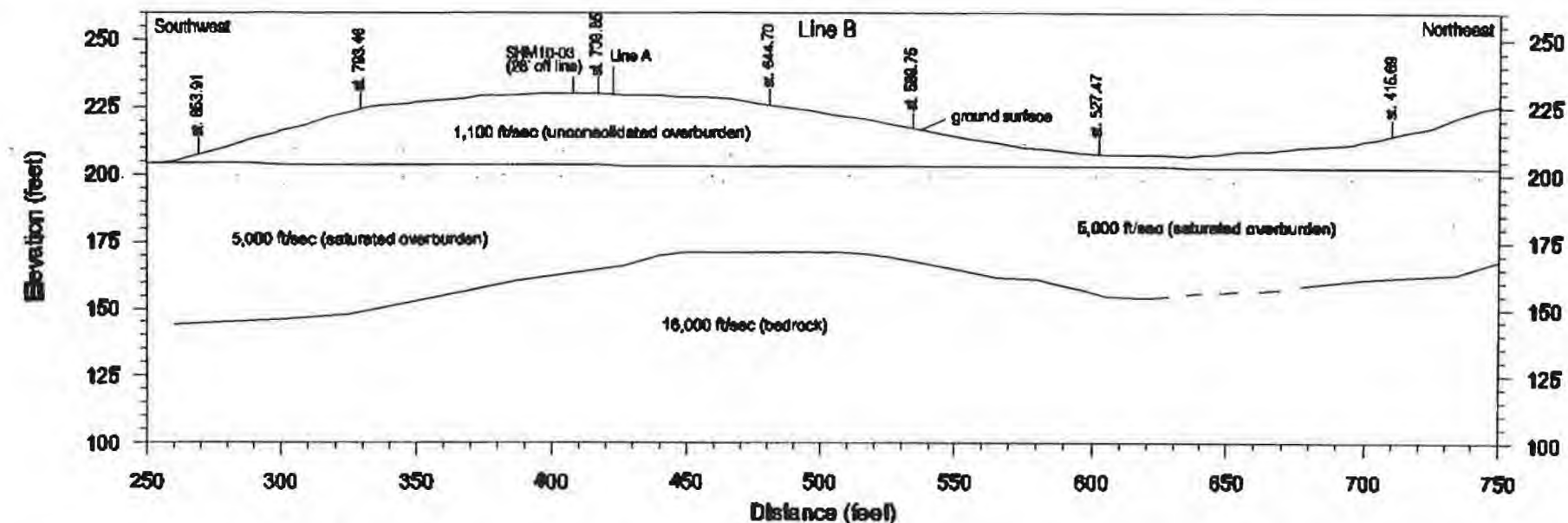
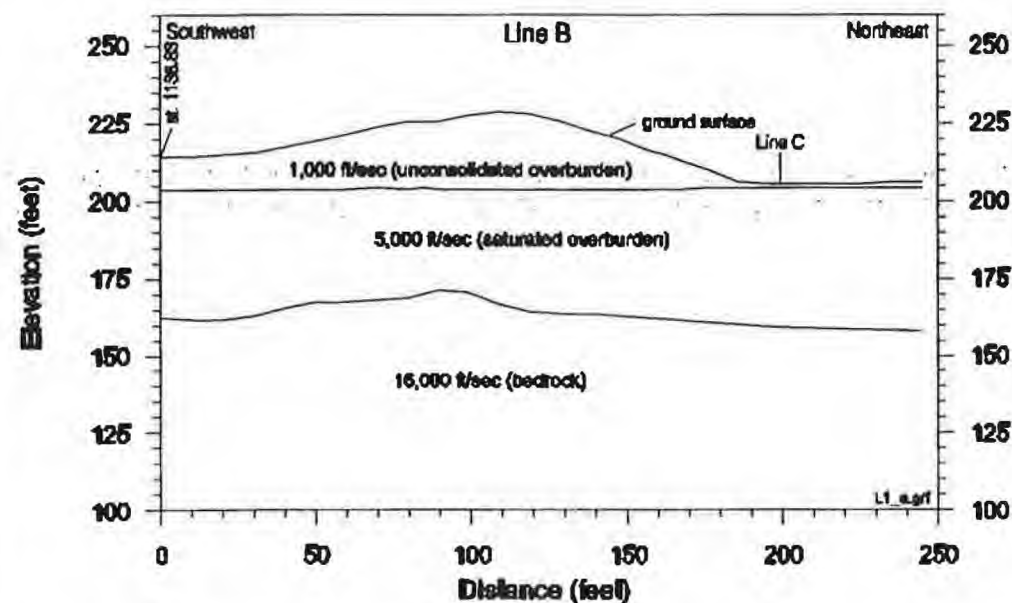
- 1) Seismic velocity values are in units of feet per second (ft/sec)
- 2) Horizontal scale, 1 inch = 50 feet  
Vertical scale, 1 inch = 50 feet  
Vertical exaggeration 1:1

- 3) Elevations were referenced to TBM A2, A3, and C1  
TBM A2 elevation is 230.74 feet  
TBM A3 elevation is 222.70 feet  
TBM C1 elevation is 239.62 feet

1101226 - 1101226cross.dwg  
last modified 07/21/10

**GEOPHYSICAL  
APPLICATIONS  
INCORPORATED**

**Figure 2, Line A  
Seismic Cross Sections  
Devens  
Ayer, Massachusetts  
prepared for  
SOVEREIGN CONSULTING, INC.**



**Notes:**

- 1) Seismic velocity values are in units of feet per second (ft/sec)
- 2) Horizontal scale, 1 inch = 80 feet  
Vertical scale, 1 inch = 60 feet  
Vertical exaggeration 1:1

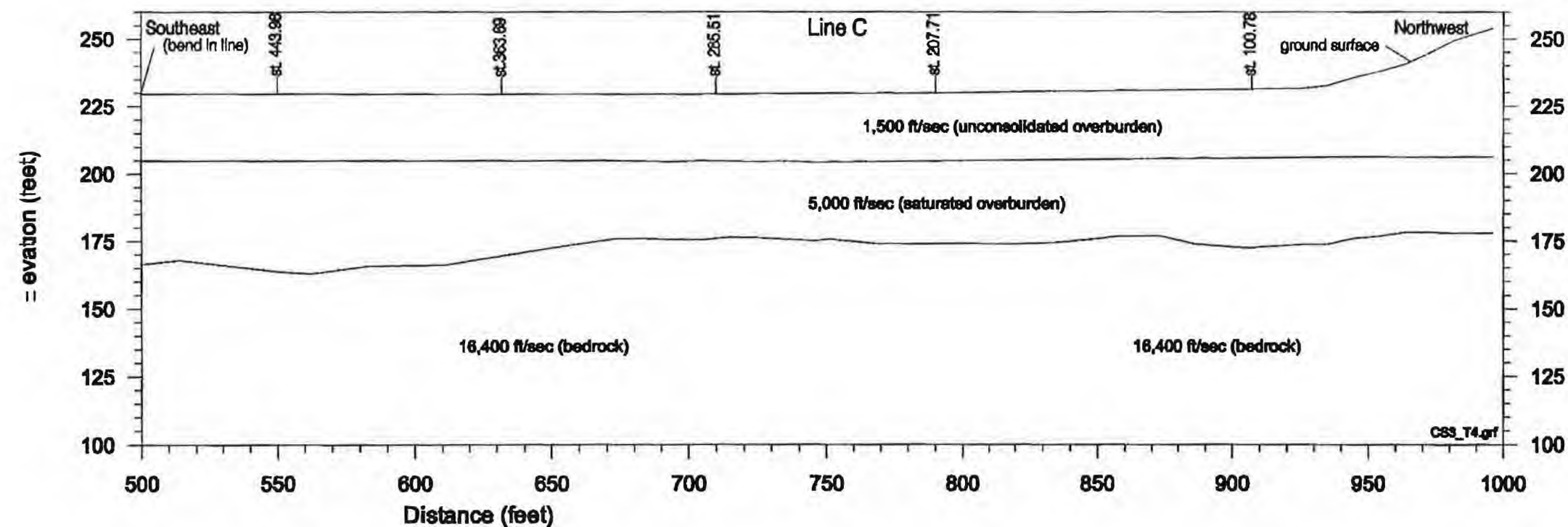
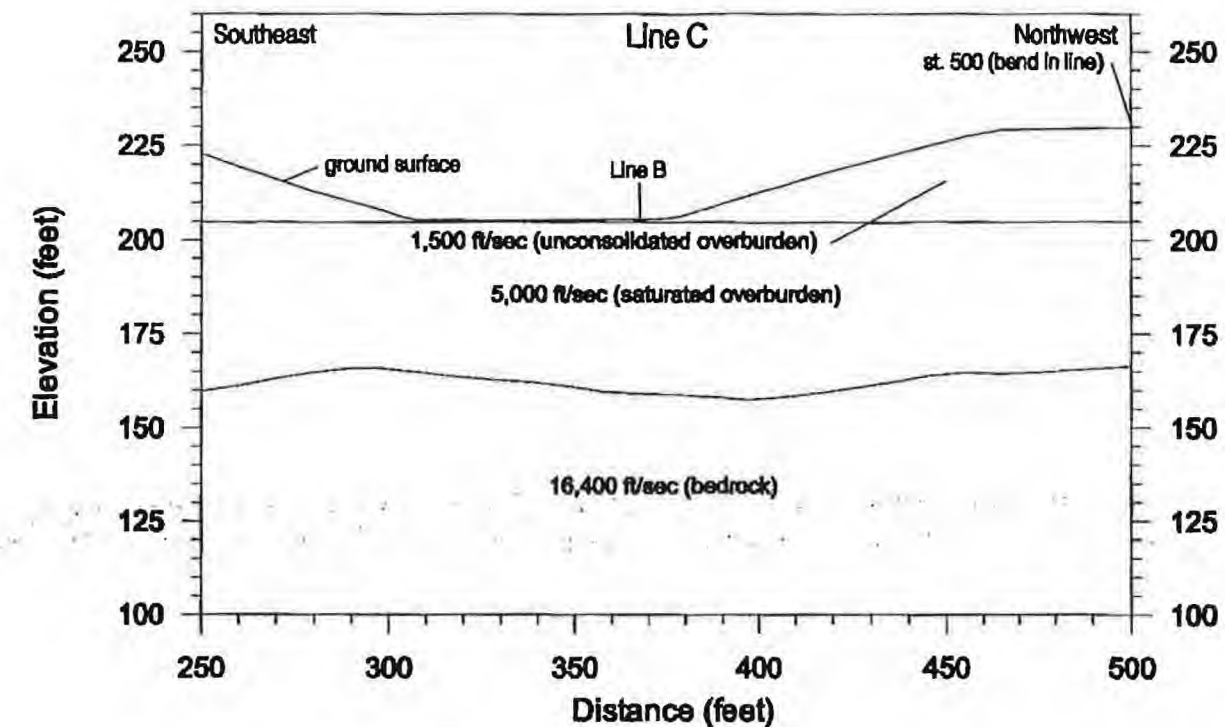
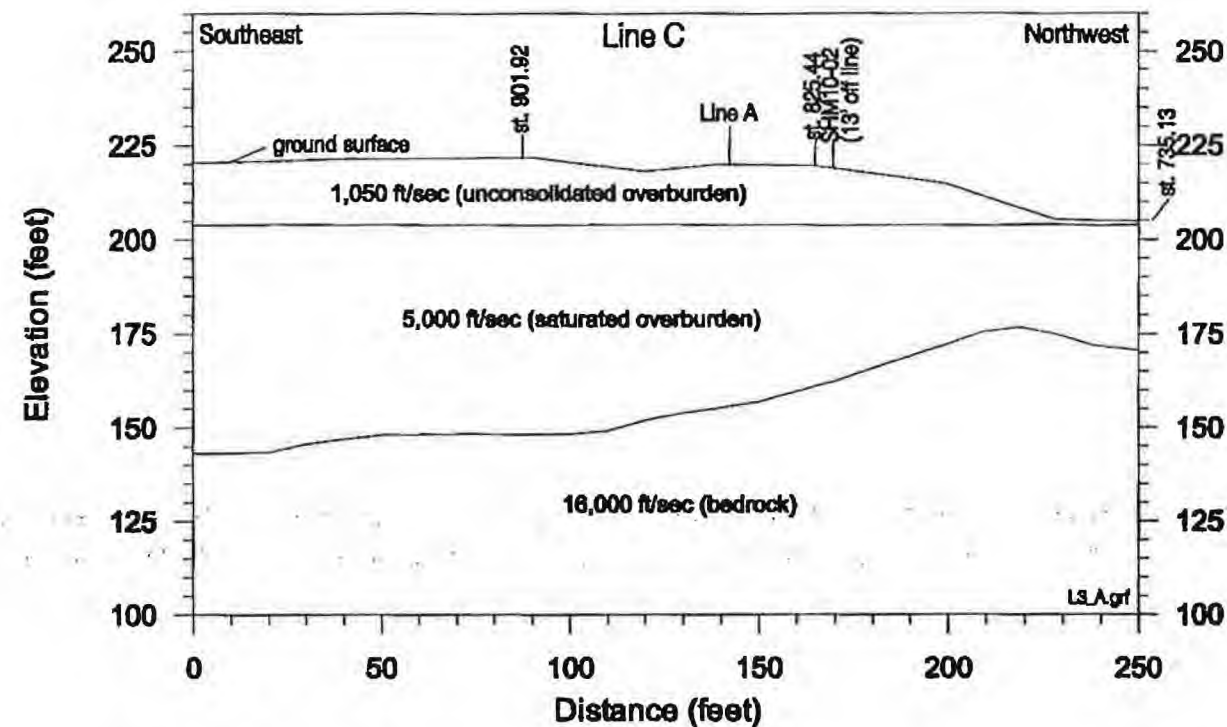
- 3) Elevations were referenced to TBM A2, A3, and C1  
TBM A2 elevation is 230.74 feet  
TBM A3 elevation is 230.74 feet  
TBM C1 elevation is 239.62 feet

**GEOPHYSICAL  
APPLICATIONS  
INCORPORATED**

Figure 3, Line B  
Seismic Cross Sections  
Devens  
Ayer, Massachusetts  
prepared for  
SOVEREIGN CONSULTING, INC.

1101229 - 1101226cross.dwg  
last modified 07/21/10





Notes:

- 1) Seismic velocity values are in units of feet per second (ft/sec)
- 2) Horizontal scale, 1 inch = 50 feet  
Vertical scale, 1 inch = 50 feet  
Vertical exaggeration 1:1

- 3) Elevations were referenced to TBM A3, and C1  
TBM A2 elevation is 230.74 feet  
TBM C1 elevation is 239.62 feet

1101225 - 1101225cross.dwg  
last modified 07/21/10

**GEOPHYSICAL  
APPLICATIONS  
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Figure 4, Line C  
Seismic Cross Sections  
Devens  
Ayer, Massachusetts  
prepared for  
**SOVEREIGN CONSULTING, INC.**

**Attachment C**

## Attachment C







Sovereign Consulting Inc.  
100 North Main Street, Suite 200  
Mansfield, MA 01948  
508-339-1200

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
4 Apple Square Way, Suite #302  
Holyoke, MA 01040  
417-540-0650

PROJECT NAME <b>AU001-002</b>		PROJECT LOCATION		DATE <b>5/27/10</b>		WELL ID <b>SHM-10-07</b>				
PROJECT NUMBER <b>FL Devens</b>		WELL (DRAIN) TEST (inches) <b>2"</b>		DEPTH TO WATER (feet) <b>26.36</b>		DEPTH TO BOTTOM (feet) <b>50.20</b>				
TUBING DIAMETER (inches) <b>1/4"</b>		TUBING MATERIAL CODE (see below) <b>PE</b>		PURGE PUMP TYPE <b>Bladder</b>		PUMP EQUIPMENT MODEL & SERIAL NO. <b>Unknown</b>				
WELL VOLUME PURGE: 1 WELL VOLUME: (TOTAL WELL DEPTH - STATIC DEPTH) TO WATER) * WELL CAPACITY						GALLONS <b>381</b> LITERS				
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02 1' = 0.04 1.25' = 0.06 2' = 0.10 3' = 0.12 4' = 0.16 5' = 0.20 6' = 0.24 12' = 0.48						1 GALLON = 3.785 LITERS				
WELL SCREEN INTERVAL DEPTH (feet) <b>40' - 50'</b>		INITIAL PUMP OR TUBING DEPTH IN WELL (feet) <b>45'</b>		FINAL PUMP OR TUBING DEPTH IN WELL (feet)		PURGING INITIATED AT <b>1210</b>				
				PURGING ENDED AT		GALLONS LITERS				
WATER LEVEL STABILIZATION				DEPTH TO WATER WITH PUMP: (feet) <b>26.84</b>						
TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS				DEPTH TO WATER (feet) START	DEPTH TO WATER (feet) END	Water Level Stable (Yes or No)	VOLUME PURGED DURING INTERVAL (mL)	
<b>0-5</b>	<b>400 mL/min</b>	<b>3 sec refill 4 sec discharge</b>				<b>26.84</b>	<b>26.88</b>	<b>Y</b>		
<b>10-15</b>	<b>400 mL/min</b>	<b>10 sec refill 5 sec discharge</b>				<b>26.88</b>	<b>26.80</b>	<b>Y</b>		
TIME (3-5 minutes)	FLOW RATE (mL/min) (100-500 mL/min)	DEPTH TO WATER (feet) (+/- 0.3')	TURBIDITY (NTU) (+/- 10%)	DISSOLVED OXYGEN (mg/L) (+/- 10%)	pH (+/- 0.1)	TEMP (°C) (+/- 0.1)	SPECIFIC CONDUCTIVITY (µS/cm) (+/- 1%)	ORP (mV) (+/- 10mV)	COLOR (describe)	ODOR (describe)
<b>12:20</b>	<b>400</b>	<b>26.80</b>	<b>314</b>	<b>0.25</b>	<b>6.55</b>	<b>12.21</b>	<b>780</b>	<b>-133.6</b>	<b>cloudy</b>	<b>none</b>
<b>12:35</b>	<b>400</b>	<b>26.81</b>	<b>109.7</b>	<b>0.32</b>	<b>6.56</b>	<b>12.18</b>	<b>784</b>	<b>-139.4</b>	<b>clear</b>	<b>none</b>
<b>12:58</b>	<b>400</b>	<b>26.82</b>	<b>51.2</b>	<b>0.28</b>	<b>6.58</b>	<b>12.20</b>	<b>781</b>	<b>-145.2</b>	<b>clear</b>	<b>none</b>
<b>13:25</b>	<b>400</b>	<b>26.75</b>	<b>25.7</b>	<b>0.29</b>	<b>6.58</b>	<b>12.41</b>	<b>775</b>	<b>-141.3</b>	<b>clear</b>	<b>none</b>
<b>14:00</b>	<b>400</b>	<b>26.75</b>	<b>16.3</b>	<b>0.24</b>	<b>6.58</b>	<b>12.49</b>	<b>771</b>	<b>-143.2</b>	<b>clear</b>	<b>none</b>
<b>14:05</b>	<b>400</b>	<b>26.74</b>	<b>18.8</b>	<b>0.27</b>	<b>6.57</b>	<b>12.36</b>	<b>770</b>	<b>-141.9</b>	<b>clear</b>	<b>none</b>
<b>14:08</b>	<b>400</b>	<b>26.75</b>	<b>18.4</b>	<b>0.28</b>	<b>6.58</b>	<b>12.57</b>	<b>771</b>	<b>-140.9</b>	<b>clear</b>	<b>none</b>
<b>14:12</b>	<b>400</b>	<b>26.74</b>	<b>19.0</b>	<b>0.28</b>	<b>6.57</b>	<b>12.51</b>	<b>771</b>	<b>-139.5</b>	<b>clear</b>	<b>none</b>
Turbidity ↑, DTW ↓, Attempted RE-STABILIZATION:										
<b>16:10</b>	<b>225</b>	<b>26.36</b>	<b>345</b>	<b>0.14</b>	<b>6.99</b>	<b>13.06</b>	<b>751</b>	<b>-196.4</b>	<b>cloudy</b>	<b>none</b>
<b>16:13</b>	<b>225</b>	<b>26.36</b>	<b>286</b>	<b>0.14</b>	<b>6.98</b>	<b>13.21</b>	<b>751</b>	<b>-197.7</b>	<b>cloudy</b>	<b>none</b>
<b>16:16</b>	<b>225</b>	<b>26.31</b>	<b>237</b>	<b>0.15</b>	<b>6.97</b>	<b>13.43</b>	<b>751</b>	<b>-195.6</b>	<b>cloudy</b>	<b>none</b>
No Stabilization after 4 HRS, per SOP began sampling										
EPA stabilization parameters from EPA/540/S-00/004 April 1996										
SAMPLING DATA										
SAMPLED BY (PRINT) & AFFILIATION <b>Laura Simkins - Sov Con</b>			SAMPLE(S) SIGNATURES: <i>Kuril</i>			SAMPLING INITIATED AT <b>1620</b>		SAMPLING ENDED AT <b>1730</b>		
PUMP OR TUBING DEPTH IN WELL (feet) <b>45'</b>		SAMPLE PUMP FLOW RATE (mL per minute) <b>225</b>		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL NO. <b>YSI 600XL</b>						
FIELD DECONTAMINATION <input checked="" type="checkbox"/> N			FIELD FILTERED: Y <input type="checkbox"/> N <input type="checkbox"/> FILTER SIZE: <input type="checkbox"/> µm			DUPLICATE: Y <input type="checkbox"/> N <input type="checkbox"/>				
MATERIAL CODES: AR = Aramid Glass CR = Clear Glass PE = Polyethylene PP = Polypropylene S = Seacock T = Teflon U = Ultrahigh (Super) U										
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)										
Type: Flush Mount / Stand Pipe			General Condition: Good / Needs Repair			Well Caps: Good / Broken / None			Lock: Good / Broken / None	
Evidence of Rain Water Between Steel & PVC? Y / N			Is Well Plumb? Y / N			PVC Riser: Good / Damaged / None				
Evidence of Ponding Around Well? Y / N			Concrete Collar: Good / Cracked / Leaking / None							
REMARKS:										



Sovereign Consulting Inc.  
805B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
4 Orono Square, Suite 1007  
Holyoke, MA 01040  
413-540-0650

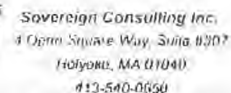
PROJECT NAME: <b>USACE-DEVENS</b>		PROJECT LOCATION: <b>Ayer, MA</b>		DATE: <b>5/24/10</b>		WELL ID: <b>SHM-10-06-024</b>				
JOCT NUMBER: <b>AC001-003-</b>		WELL DIAMETER (inches): <b>1"</b>		DEPTH TO WATER (feet): <b>~25</b>		DEPTH TO BOTTOM (feet): <b>N/A</b>				
PURGING DATA										
TUBING DIAMETER (inches): <b>1/4</b>		TUBING MATERIAL CODE (see below): <b>PE</b>		PLURGE PUMP TYPE: <b>Penstatic</b>		PUMP EQUIPMENT MODEL & SERIAL #s: <b>Geopump 2</b>				
WELL VOLUME PURGE: 1 WELL VOLUME= (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY						GALLONS: _____ LITERS: _____				
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02, 1" = 0.04, 1.25" = 0.06, 2" = 0.10, 3" = 0.13, 4" = 0.16, 5" = 0.20, 6" = 0.24, 8" = 0.32, 10" = 0.40, 12" = 0.48						1 GALLON = 3.785 LITERS				
WELL SCREEN INTERVAL DEPTH (feet): <b>23-25</b>		INITIAL PUMP OR TUBING DEPTH IN WELL (feet): <b>24</b>		FINAL PUMP OR TUBING DEPTH IN WELL (feet): <b>same</b>		PURGING INITIATED AT: _____ PURGING ENDED AT: _____				
WATER LEVEL STABILIZATION		DEPTH TO WATER WITH PUMP (feet): _____								
TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS				DEPTH TO WATER (feet) START	Water Level Stable (Yes or No)	VOLUME PURGED DURING INTERVAL (mL)		
<b>10 min</b>	<b>300 mL/minute</b>					<b>N/A - Purging</b>				
TIME (3-5 minutes)	FLOW RATE (100-500 mL/min)	DEPTH TO WATER (feet) (1/4 - 0.2)	TURBIDITY (NTU) (1/4 - 10%)	DISSOLVED OXYGEN (mg/L) (1/4 - 10%)	pH (1/4 - 0.1)	TEMP (°C) (1/4 - 30)	SPECIFIC CONDUCTIVITY (µS/cm) (1/4 - 200)	ORP (mV) (1/4 - 10mV)	COLOR (describe)	ODOR (describe)
<b>5</b>	<b>450</b>	<b>N/A</b>	<b>240</b>	<b>0.40</b>	<b>7.04</b>	<b>10.17</b>	<b>28</b>	<b>96.7</b>	<b>CLR</b>	<b>None</b>
<b>10</b>	<b>450</b>	<b>N/A</b>	<b>240</b>	<b>0.30</b>	<b>6.67</b>	<b>9.68</b>	<b>28</b>	<b>106.4</b>	<b>CLR/CLD</b>	<b>None</b>
<b>15</b>	<b>450</b>	<b>N/A</b>	<b>170</b>	<b>0.24</b>	<b>6.12</b>	<b>9.44</b>	<b>27</b>	<b>115.7</b>	<b>CLR/CLD</b>	<b>None</b>
<b>20</b>	<b>450</b>	<b>N/A</b>	<b>100</b>	<b>0.20</b>	<b>5.77</b>	<b>9.18</b>	<b>26</b>	<b>122.2</b>	<b>CLR</b>	<b>None</b>
<b>25</b>	<b>450</b>	<b>N/A</b>	<b>50</b>	<b>0.19</b>	<b>5.57</b>	<b>9.16</b>	<b>26</b>	<b>127.4</b>	<b>CLR</b>	<b>None</b>
* EPA stabilization parameters from EPA/540/S-05/004 April 1991										
SAMPLING DATA										
SAMPLED BY (PRINT) / AFFILIATION:			SAMPLER(S) SIGNATURES:				SAMPLING INITIATED AT:		SAMPLING ENDED AT:	
PUMP OR TUBING DEPTH IN WELL (feet):			SAMPLE PUMP FLOW RATE (mL per minute):			FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s:				
FIELD OF CONTAMINATION: Y / N			FIELD FILTERED: Y / N			FILTER SIZE _____ µm			DUPLICATE Y / N	
MATERIAL CODES: AG = Amber Glass, CG = Clear Glass, PE = Polyethylene, PP = Polypropylene, S = Silica, T = Teflon, O = Other (Specify)			WELL CONDITION CHECKLIST (circle appropriate item(s); cross out if not applicable)							
Type: Flush Mount / Stand Pipe			General Condition: Good / Needs Repair			Well Caps: Good / Broken / None			Lock: Good / Broken / None	
source of Rain Water Between Steel & PVC? Y / N			Is Well Plumb? Y / N			PVC Riser: Good / Damaged / None				
evidence of Ponding Around Well? Y / N			Concrete Collar: Good / Cracked / Leaking / None							
REMARKS:										





## MONITORING WELL SAMPLING LOG

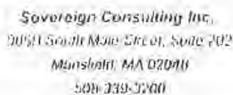
### Low Flow Sampling

[illegible]

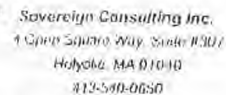


### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

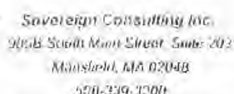
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## MONITORING WELL SAMPLING LOG

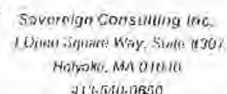
### Low Flow Sampling

[illegible]





### Low Flow Sampling

[illegible]

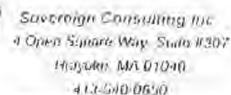
## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



### Low Flow Sampling

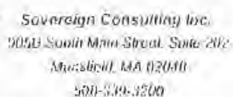
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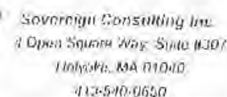
## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

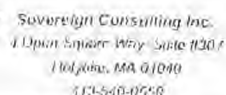
### Low Flow Sampling

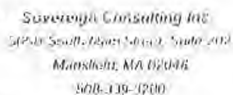
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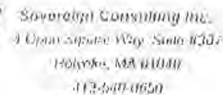


### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Line View Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

#### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]





Sovereign Consulting Inc.  
301 1/2 South Main Street, Suite 202  
Marshall, MA 01946  
508-218-3200

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
301 1/2 South Main Street, Suite 202  
Marshall, MA 01946  
508-218-3200

PROJECT NAME <b>US ACE Decons</b>		PROJECT LOCATION <b>Ayer</b>		DATE <b>5-27-10</b>		WELL ID <b>10-01</b>	
PROJECT NUMBER		WELL DIAMETER (inches) <b>3/4</b>		DEPTH TO WATER (feet) <b>NA</b>		DEPTH TO BOTTOM (feet) <b>NA</b>	
PURGING DATA							
TUBING DIAMETER (inches) <b>1/4</b>		TUBING MATERIAL CODE (see below) <b>Poly</b>		PURGE PUMP TYPE <b>Geopump</b>		PUMP EQUIPMENT MODEL & SERIAL #s	
WELL VOLUME PURGE: 1 WELL VOLUME: (TOTAL WELL DEPTH) STATIC DEPTH TO WATER) x WELL CAPACITY						GALLONS	
WELL CAPACITY (Gallons Per Foot) 0.75 = 0.02, 1' = 0.04, 1.25' = 0.06, 2' = 0.10, 3' = 0.13, 4' = 0.16, 5' = 0.20, 6' = 0.24, 12' = 0.40						1 GALLON = 3.785 LITERS	
WELL SCREEN INTERVAL DEPTH (feet) <b>68-70</b>		INITIAL PUMP OR TUBING DEPTH IN WELL (feet) <b>69</b>		FINAL PUMP OR TUBING DEPTH IN WELL (feet) <b>69</b>		PURGING INITIATED AT <b>1350</b>	
PURGING ENDED AT <b>1400</b>						TOTAL VOLUME PURGED <b>3</b>	
WATER LEVEL STABILIZATION		DEPTH TO WATER WITH PUMP (feet)					
TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS			DEPTH TO WATER (feet) START END		Water Level Stable (Yes or No)
VOLUME PURGED DURING INTERVAL (mL)							
TIME (3.5 minutes)*	FLOW RATE (mL/min) (100-500 mL/min)*	DEPTH TO WATER (feet) (+/- 0.3)*	TURBIDITY (NTU) (+/- 10%)*	DISSOLVED OXYGEN (mg/L) (+/- 10%)*	pH (+/- 0.1)*	TEMP (°C) (+/- 0.5)*	SPECIFIC CONDUCTIVITY (µS/cm) (+/- 3%)*
ORP (mV) (+/- 10mV)*	COLOR (describe)	ODOR (describe)					
1415	300		450	2.04	6.50	13.81	378
1420	300		550	8.8	6.45	13.22	372
1430	300		400	3.9	6.39	12.48	397
1435	300		200	3.5	6.39	12.36	395
* EPA stabilization parameters from EPA/540/S-95/001 April 1996							
SAMPLING DATA							
SAMPLED BY (PRINT) & AFFILIATION <b>Eric Foley, S&amp;L</b>		SAMPLER(S) SIGNATURE <b>Eric</b>		SAMPLING INITIATED AT <b>1440</b>		SAMPLING ENDED AT <b>1455</b>	
PUMP OR TUBING DEPTH IN WELL (feet)		SAMPLE PUMP FLOW RATE (mL per minute)		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s			
FIELD DECONTAMINATION <input checked="" type="checkbox"/> N		FIELD FILTERED <input checked="" type="checkbox"/> Y <input type="checkbox"/> N		FILTER SIZE _____ µm		DUPLICATE <input checked="" type="checkbox"/> N	
MATERIAL CODES AG = Amber Glass CG = Clear Glass PE = Polyethylene PP = Polystyrene S = Silicone T = Teflon D = Other (Specify)							
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)							
Type: Flush Mount / Stand Pipe		General Condition: Good / Needs Repair		Well Caps: Good / Broken / None		Lock: Good / Broken / None	
Evidence of Rain Water Between Steel & PVC? Y / N		Is Well Plumb? Y / N		PVC Riser: Good / Damaged / None			
Evidence of Ponding Around Well? Y / N		Concrete Collar: Good / Cracked / Leaking / None					
REMARKS							

## MONITORING WELL SAMPLING LOG

### Low-Floor Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low to low Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

Low FLOW Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low-Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Signaling

[illegible]

## MONITORING WELL SAMPLING LOG

### Line Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Scrubbing

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

Low / Low Sampling

[illegible]

only diff part last sample location and refusal

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



# MONITORING WELL SAMPLING LOG

### Low-Five Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



Sovereign Consulting Inc.  
300 West Main Street, Suite 100  
Hopedale, MA 01906  
(508) 779-1700

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
300 West Main Street, Suite 100  
Hopedale, MA 01906  
(508) 779-1700

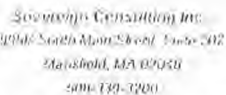
PROJECT NAME <b>USACE - Devens</b>		PROJECT LOCATION <b>Apex, MA</b>		DATE <b>6/3/10</b>		WELL ID <b>10-08</b>																																																																																									
PROJECT NUMBER <b>10001-002 #4</b>		WELL DIAMETER (inches) <b>3/4"</b>		DEPTH TO WATER (feet) <b>N/A</b>		PND READING (gpm) <b>N/A</b>																																																																																									
<b>PURGING DATA</b>																																																																																															
TUBING DIAMETER (inches) <b>1/4"</b>		TUBING MATERIAL CODE (see manual) <b>Poly</b>		PURGE PUMP TYPE <b>geopump</b>		PUMP EQUIPMENT MODEL & SERIAL #s																																																																																									
WELL VOLUME PURGE: 1 WELL VOLUME = (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) x WELL CAPACITY				GALLONS		LITERS																																																																																									
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02, 1" = 0.04, 1.25" = 0.05, 2" = 0.16, 3" = 0.31, 4" = 0.65, 5" = 1.02, 6" = 1.47, 12" = 5.80				1 GALLON = 3.785 LITERS		TOTAL VOLUME PURGED																																																																																									
WELL SCREEN INTERVAL DEPTH (feet)		INITIAL PUMP OR TUBING DEPTH IN WELL (feet) <b>51'</b>		FINAL PUMP OR TUBING DEPTH IN WELL (feet) <b>15'03</b>		PURGING ENDED AT <b>15'30</b>																																																																																									
WATER LEVEL STABILIZATION				DEPTH TO WATER WITH PUMP (feet)																																																																																											
TIME INTERVAL (min)	FLOW RATE (ml/min)	PUMP SETTINGS			DEPTH TO WATER (feet) START	DEPTH TO WATER (feet) END	Water Level Stable (Yes or No)																																																																																								
<table border="1"> <thead> <tr> <th>TIME</th> <th>FLOW RATE (ml/min)</th> <th>DEPTH TO WATER (feet)</th> <th>TURBIDITY (NTU)</th> <th>DISSOLVED OXYGEN (mg/L)</th> <th>pH</th> <th>TEMP (°C)</th> <th>SPECIFIC CONDUCTIVITY (µS/cm)</th> <th>ORP (mV)</th> <th>COLOR (describe)</th> <th>ODOR (describe)</th> </tr> </thead> <tbody> <tr> <td>15:32 00:00</td> <td>600</td> <td></td> <td>84.1</td> <td>0.56</td> <td>6.49</td> <td>13.99</td> <td>946</td> <td>-18</td> <td>tan</td> <td></td> </tr> <tr> <td>15:37 5</td> <td></td> <td></td> <td>201</td> <td>0.31</td> <td>6.53</td> <td>12.15</td> <td>968</td> <td>-28</td> <td>tan/clear</td> <td></td> </tr> <tr> <td>15:42 10</td> <td></td> <td></td> <td>535</td> <td>0.30</td> <td>6.54</td> <td>11.20</td> <td>967</td> <td>-38</td> <td>tan/clear</td> <td></td> </tr> <tr> <td>15:47 15</td> <td></td> <td></td> <td>535</td> <td>0.29</td> <td>6.55</td> <td>11.83</td> <td>966</td> <td>-44</td> <td>tan</td> <td></td> </tr> <tr> <td>15:52 20</td> <td></td> <td></td> <td>380</td> <td>0.24</td> <td>6.55</td> <td>11.75</td> <td>965</td> <td>-46</td> <td>tan</td> <td></td> </tr> <tr> <td>15:57 25</td> <td></td> <td></td> <td>344</td> <td>0.24</td> <td>6.57</td> <td>11.78</td> <td>965</td> <td>-47</td> <td>tan/clear</td> <td></td> </tr> <tr> <td>16:02 30</td> <td></td> <td></td> <td>321</td> <td>0.24</td> <td>6.56</td> <td>11.60</td> <td>964</td> <td>-42</td> <td>tan/clear</td> <td></td> </tr> </tbody> </table>								TIME	FLOW RATE (ml/min)	DEPTH TO WATER (feet)	TURBIDITY (NTU)	DISSOLVED OXYGEN (mg/L)	pH	TEMP (°C)	SPECIFIC CONDUCTIVITY (µS/cm)	ORP (mV)	COLOR (describe)	ODOR (describe)	15:32 00:00	600		84.1	0.56	6.49	13.99	946	-18	tan		15:37 5			201	0.31	6.53	12.15	968	-28	tan/clear		15:42 10			535	0.30	6.54	11.20	967	-38	tan/clear		15:47 15			535	0.29	6.55	11.83	966	-44	tan		15:52 20			380	0.24	6.55	11.75	965	-46	tan		15:57 25			344	0.24	6.57	11.78	965	-47	tan/clear		16:02 30			321	0.24	6.56	11.60	964	-42	tan/clear	
TIME	FLOW RATE (ml/min)	DEPTH TO WATER (feet)	TURBIDITY (NTU)	DISSOLVED OXYGEN (mg/L)	pH	TEMP (°C)	SPECIFIC CONDUCTIVITY (µS/cm)	ORP (mV)	COLOR (describe)	ODOR (describe)																																																																																					
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* EPA stabilization parameters from EPA/540/S-99/004 April 1996																																																																																															
<b>SAMPLING DATA</b>																																																																																															
SAMPLED BY (PRINT) / AFFILIATION				SAMPLE(S) SIGNATURE(S)		SAMPLING INITIATED AT <b>16:04</b>																																																																																									
SAMPLING ENDED AT																																																																																															
PUMP OR TUBING DEPTH (feet)		SAMPLE PUMP FLOW RATE (ml, gals, seconds)		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s																																																																																											
FIELD DECONTAMINATION <input checked="" type="checkbox"/> N		FIELD FILTERED <input checked="" type="checkbox"/> N		FILTER SIZE <input type="text"/>		DUPLICATE <input type="checkbox"/> Y <input type="checkbox"/> N																																																																																									
MATERIAL CODES: AG = Aluminum, CG = Cast Glass, PE = Polyethylene, PP = Polypropylene, S = Silicone, T = Teflon, O = Other (Specify)																																																																																															
<b>WELL CONDITION CHECKLIST</b> (circle appropriate items), cross out if not applicable																																																																																															
Type: Flush Mount / Stand Pipe		General Condition: Good / Needs Repair		Well Caps: Good / Broken / None		Lock: Good / Broken / None																																																																																									
Evidence of Rain Water Between Steel & PVC? Y / N		Is Well Plumb? Y / N		PVC Riser: Good / Damaged / None																																																																																											
Evidence of Ponding Around Well? Y / N		Concrete Collar: Good / Cracked / Leaking / None																																																																																													
REMARKS:																																																																																															



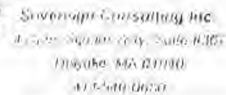
## MONITORING WELL SAMPLING LOG

### Flow Flow Sampling

[illegible]



## Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low-Low Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

Low-Low Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

#### Low Sampling

[illegible]





## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



# MONITORING WELL SAMPLING LOG

Low Flow Sampling



PROJECT LOCATION		DATE <u>6/6/2010</u>		WELL ID <u>54M10-02</u>	
WELLER	WELL DIAMETER (inches)	DEPTH TO WATER (feet)	DEPTH TO BOTTOM (feet)	PID READING (ppm)	

PURGING DATA					
WELL DIAMETER (in)	TUBING MATERIAL CODE (see notes)	PURGE PUMP TYPE	PUMP EQUIPMENT MODEL & SERIAL #s		
WELL VOLUME PURGE: 1 WELL VOLUME: (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY			GALLONS	LITERS	
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.07, 1" = 0.04, 1.25" = 0.06, 2" = 0.16, 3" = 0.31, 4" = 0.65, 5" = 1.02, 6" = 1.47, 12" = 5.88			1 GALLON = 3.785 LITERS		TOTAL VOLUME PURGED
WELL SCREEN INTERVAL DEPTH (feet)	INITIAL PUMP OR TUBING DEPTH IN WELL (feet)	FINAL PUMP OR TUBING DEPTH IN WELL (feet)	PURGING INITIATED AT	PURGING ENDED AT	GALLONS
		<u>94</u>	<u>82550</u>		LITERS

WATER LEVEL STABILIZATION		DEPTH TO WATER WITH PUMP (feet)	
TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS	DEPTH TO WATER (feet) START END
			Water Level Stable (Yes or No)
			VOLUME PURGED DURING INTERVAL (mL)

TIME (3-5 minutes)	FLOW RATE (mL/min) (100-500 mL/min)	DEPTH TO WATER (feet) (1" = 0.3')	TURBIDITY (NTU) (1-10%)	DISSOLVED OXYGEN (mg/L) (1-10%)	pH (1-14)	TEMP (°C) (1-35)	SPECIFIC CONDUCTIVITY (µS/cm) (1-300)	ORP (mV) (1-1000)	COLOR (describe)	ODOR (describe)
0	300		2746	2060	5.42	13.27	2473	-6.9		
5			144	1.59	5.51	12.47	2442	-12.9		
10			484	1.40	5.54	12.74	2477	-22.2		
15			out of range	1.23	5.54	12.65	2432	-61.9		
20			11	1.17	5.63	12.54	2425	-47.9		
25			11	1.16	5.67	12.57	2426	-105.9		
30			11	1.15	5.70	12.54	2431	-97.9		

\* EPA stabilization parameters from EPA/540/S-95/004, April 1996

SAMPLING DATA			
SAMPLED BY (PRINT) / AFFILIATION	SAMPLER(S) SIGNATURES	SAMPLING INITIATED AT	SAMPLING ENDED AT
		<u>925</u>	
PUMP OR TUBING DEPTH IN WELL (feet)	SAMPLE PUMP FLOW RATE (mL per minute)	FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s	
FIELD DECONTAMINATION Y / N	FIELD FILTERED Y / N	FILTER SIZE (µm)	DUPPLICATE Y / N

MATERIAL CODES: AG = Amber Glass, CG = Clear Glass, PE = Polyethylene, PP = Polypropylene, S = Silicone, L = Latex, O = Other (Specify)

WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)	
Type: Flush Mount / Stand Pipe	General Condition: Good / Needs Repair
Evidence of Rain Water Between Steel & PVC? Y / N	Is Well Plumb? Y / N
Evidence of Ponding Around Well? Y / N	PVC Riser: Good / Damaged / None
Concrete Collar: Good / Cracked / Leaking / None	

REMARKS:

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

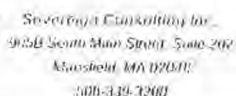
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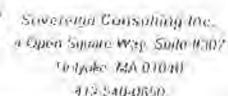
## MONITORING WELL SAMPLING LOG

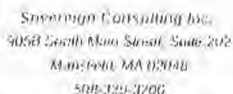
### Low Flow Sampling

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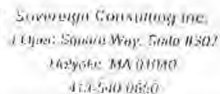


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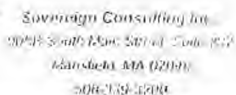
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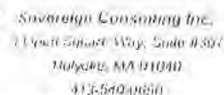
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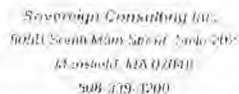
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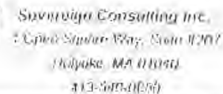


### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

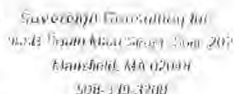
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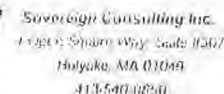
## MONITORING WELL SAMPLING LOG

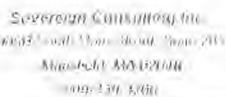
#### Low Flow Sampling

[illegible]

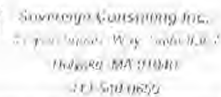


### Low Flow Example

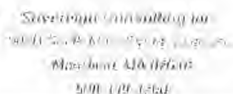
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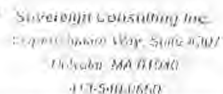
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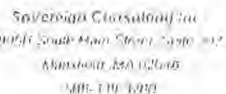
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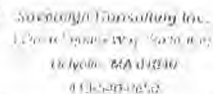


## Low Flow Sampling

[illegible]



### Low Flow Sampling

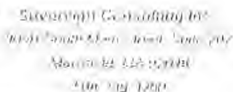
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## MONITORING WELL SAMPLING LOG

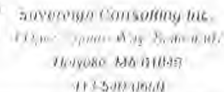
few / fewˈsɪmplicɪti/

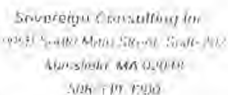
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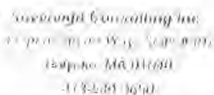


### Low-Low Sampling

[illegible]



### Low-Flow Sampling

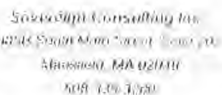
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## MONITORING WELL SAMPLING LOG

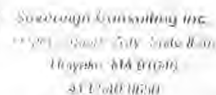
### Low Flow Sampling

[illegible]





## Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Fast Flow Scanning



PROJECT NAME

PROJECT LOCATION

DATE

WELL ID

PROJECT NUMBER

WELL DIAMETER (inches)

DEPTH TO WATER (feet)

DEPTH TO BOTTOM (feet)

WELL HEAD (gpm)

6/4/10

10-05A

PURGING DATA

TUBING DIA/ETER (inches)

TUBING MATERIAL CODE (see below)

PURGE PUMP TYPE

PUMP EQUIPMENT MODEL & SERIAL #

WELL VOLUME PURGED: 1 WELL VOLUME = (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY

GALLONS

LITERS

WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02, 1" = 0.04, 1.25" = 0.06, 2" = 0.10, 3" = 0.17, 4" = 0.25, 5" = 0.32, 6" = 0.42, 8" = 0.56, 10" = 0.71

1 GALLON = 3.785 LITERS

TOTAL VOLUME PURGED

WELL SCREEN INTERVAL DEPTH (feet)

INITIAL PUMP OR TUBING DEPTH IN WELL (feet)

FINAL PUMP OR TUBING DEPTH IN WELL (feet)

PURGING INITIATED AT

PURGING ENDED AT

GALLONS

LITERS

59'

15:14

15:24

WATER LEVEL STABILIZATION

DEPTH TO WATER WITH PUMP (feet)

TIME INTERVAL (min)

FLOW RATE (mL/min)

PUMP SETTINGS

DEPTH TO WATER (feet) START END

Water Level Stable (Yes or No)

VOLUME PURGED DURING INTERVAL (mL)

TIME

FLOW RATE (mL/min)

DEPTH TO WATER (feet)

TURBIDITY (NTU)

DISSOLVED OXYGEN (mg/L)

pH

TEMP (°C)

SPECIFIC CONDUCTIVITY (µS/cm)

ORP (mV)

COLOR (describe)

ODOR (describe)

0

400

Er 1

3.58

6.17

14.77

206

43

tan

5

Er 2

6.61

6.20

14.68

211

32

tan

10

Er 1

6.67

6.13

14.57

210

32

tan

15

replace to best results

Er 1

6.64

6.03

14.10

211

28

tan

20

44.3

1.72

5.94

14.07

209

35

tan / clear

25

33.7

1.75

6.18

13.95

209

35

tan / clear

30

32.9

1.73

6.18

13.89

218

21

tan / clear

EPA stabilization parameters from EPA/600/R-95/004 April 1996

SAMPLING DATA

SAMPLED BY (PRINT) / AFFILIATION

SAMPLER(S) SIGNATURES

SAMPLING INITIATED AT

SAMPLING ENDED AT

PUMP OR TUBING DEPTH IN WELL (feet)

SAMPLE FLOW RATE (mL per minute)

FIELD SAMPLER MODEL / MAKE - EQUIPMENT / MODEL & SERIAL #

FIELD DECONTAMINATION Y N

FIELD FILTERED Y N

FILTER SIZE µm

Duplicate Y N

MATERIAL CODES

AG = Amber Glass CG = Clear Glass PE = Polyethylene PP = Polypropylene SI = Silicon LI = Liquefied O = Other (Specify)

15:57

WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe

General Condition: Good / Needs Repair

Well Caps: Good / Broken / None

Lock: Good / Broken / None

Evidence of Rain Water Between Steel & PVC? Y / N

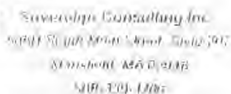
Is Well Plumb? Y / N

PVC Riser: Good / Damaged / None

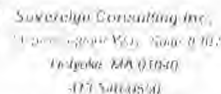
Evidence of Ponding Around Well? Y / N

Concrete Collar: Good / Cracked / Leaking / None

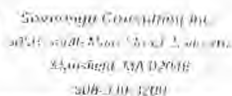
REMARKS:



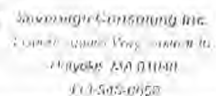
### Low Flow Sampling

[illegible]





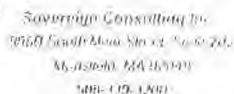
**Figure 1 (continued)**

[illegible]

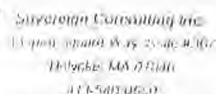
## MONITORING WELL SAMPLING LOG

LOWE J. TEST STATISTICS

[illegible]



### Univariate and bivariate associations

[illegible]



## Low Flow Sampling



### Purge Data

Concrete collar: OK / Cracked / Leaking / None

## MONITORING WELL SAMPLING LOG

### Low-Floor Seating

[illegible]



Saverglass Consulting Inc.  
1000 Corporate Lane, Suite 200  
Methuen, MA 02844  
978-350-1200

# MONITORING WELL SAMPLING LOG

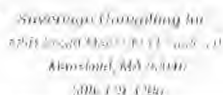
Case 1 (For Sampling)



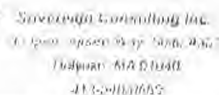
Saverglass Consulting Inc.  
1000 Corporate Lane, Suite 200  
Methuen, MA 02844  
978-350-1200

PROJECT NAME:		PROJECT LOCATION:		DATE: 6/10/2010	WELL ID: 211110-03
OBJECT NUMBER:		WELL DIAMETER (inches):	DEPTH TO WATER (feet):	DEPTH TO BOTTOM (feet):	WELL READING (gpm):
<b>PURGING DATA</b>					
TUBING DIAMETER (inches):		TUBING MATERIAL CODE (see below):	PUMP TYPE:	PUMP EQUIPMENT MODEL & SERIAL #:	
WELL VOLUME PURGE: 1 WELL VOLUME = (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY				GALLONS:	LITERS:
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02, 1" = 0.04, 1.25" = 0.06, 2" = 0.16, 3" = 0.37, 4" = 0.65, 5" = 1.02, 6" = 1.47, 12" = 5.88				1 GALLON = 3.785 LITERS	
WELL SCREEN INTERVAL DEPTH (feet):		INITIAL PUMP OR TUBING DEPTH IN WELL (feet):	FINAL PUMP OR TUBING DEPTH IN WELL (feet): 39	PURGING INITIATED AT: 4845	PURGING ENDED AT:
WELL SCREEN INTERVAL DEPTH (feet):		TOTAL VOLUME PURGED: GALLONS: LITERS:			
<b>WATER LEVEL STABILIZATION</b>					
TIME INTERVAL (min):		FLOW RATE (mL/min):	PUMP SETTINGS:	DEPTH TO WATER (feet) START: END:	Water Level Stable (Yes or No):
VOLUME PURGED DURING INTERVAL (mL):					
TIME (3-5 minutes)	FLOW RATE (mL/min) (100-600 mL/min)	DEPTH TO WATER (feet) (1'-0.2')	TURBIDITY (NTU) (0-100)	DISSOLVED OXYGEN (mg/L) (1-100)	pH (6.5-8.5)
TEMP (°C) (10-35)	SPECIFIC CONDUCTIVITY (µS/cm) (10-200)	ORP (mV) (10-100)	COLOR (describe)	ODOR (describe)	
847	300		450	422	5.90
851			745	271	6.09
856			616	239	6.19
901			442	243	6.24
906			196	250	6.28
911			801	257	6.29
915			585	263	6.30
* EPA stabilization parameters from EPA/540/S-95/004 April 1995					
<b>SAMPLING DATA</b>					
SAMPLED BY (PRINT) / AFFILIATION:		SAMPLER(S) SIGNATURES:		SAMPLING INITIATED AT: 9:20	SAMPLING ENDED AT:
PUMP OR TUBING DEPTH IN WELL (feet):		SAMPLE PUMP FLOW RATE (mL per minute):		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s:	
FIELD DECONTAMINATION: Y / N		FIELD FILTERED: Y / N FILTER SIZE: µm		DUPLICATE: Y / N	
MATERIAL CODES: AG = Amber Glass, CG = Clear Glass, PE = Polyethylene, PP = Polypropylene, S = Stainless Steel, T = Teflon, D = Other (Specify):					
<b>WELL CONDITION CHECKLIST</b> (circle appropriate item(s); cross out if not applicable)					
Type: Flush Mount / Stand Pipe		General Condition: Good / Needs Repair		Well Caps: Good / Broken / None	
Evidence of Rain Water Between Steel & PVC? Y / N		Is Well Plumb? Y / N		PVC Riser: Good / Damaged / None	
Evidence of Ponding Around Well? Y / N		Concrete Collar: Good / Cracked / Leaking / None			
REMARKS:					





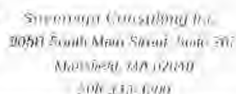
## Low-Low Sampling:

[illegible]

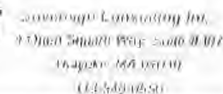
## MONITORING WELL SAMPLING LOG

### Low-Low Sampling

[illegible]



Uwe F. Lipp/Sangam

[illegible]



## WELL DEVELOPMENT DATA FORM

WELL ID: SLM-10-06START TEAM MEMBER: PJV + CMHSITE: Dover's PortDATE: 6/24/13PROJECT NO.: AC001TIME: 0915PUMP TYPE & MODEL: Waterman Hydro L11IWEATHER: 85° Sunny + Wind

## 1. INITIAL READINGS

START TIME: 1430

WELL DIAMETER (INCHES)	PID WELL HEAD (PPM)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)	DEPTH TO PRODUCT (FEET)	PRODUCT THICKNESS (FEET)	DEPTH TO SCREEN (FEET)	PUMP DEPTH (FEET)	WELL VOLUME (Gallons) (Milliliters)
1.5	NA	1989	76.60	NA	NA	70	75 Start	52

Stickup  $\approx 2.80$  ft

## 2. DEVELOPMENT READINGS

TIME (MINUTES)	RATE (gal/min) (ml/min)	DEPTH TO WATER (FEET)	ORP (mV)	D.O. (mg/L)	pH (S.U.)	TEMP (degrees C)	SP COND. (uS/cm)	Turb (NTU)	Volume (gal) (ml)	Appearance (Silty) (Clear)
15										Silty
32	0.35								3.5	
220									7	
240									10.5	
260									14.0	
280									17.5	
300			-929	0.70	5.80	11.20	754	Er 2	19.5	
320			-1349	1.96	6.43	11.29	725	OR	24.5	
340			-1333	1.74	6.56	11.27	711	OR	27.5	
351			-140.4	1.59	6.52	11.37	696	OR	28.0	
359			-145.4	0.84	6.53	11.42	688	OR	29.0	
400			-148.4	0.94	6.55	11.37	680	OR	31.5	

## 3. POST-DEVELOPMENT

END TIME: 1600

TOTAL TIME (MINUTES)	TOTAL VOL (gallons) (milliliters)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)
90	315	1992	812

## ADDITIONAL NOTES:

Er 2/OR = out of Range

## WELL DEVELOPMENT DATA FORM

WELL ID: SHM-10 v6A

START TEAM MEMBER: PJV &amp; CMH

SITE: Fort Devco's SHL

DATE: 6/30/10

PROJECT NO.: ACOOL

TIME: 0930

PUMP TYPE &amp; MODEL: Waterco Hydro Lift I

WEATHER: 75° Sunny

## 1. INITIAL READINGS

START TIME: 0938

WELL DIAMETER (INCHES)	PID WELL HEAD (PPM)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)	DEPTH TO PRODUCT (FEET)	PRODUCT THICKNESS (FEET)	DEPTH TO SCREEN (FEET)	PUMP DEPTH (FEET)	WELL VOLUME (Gallons) (Milliliters)
1.5	NA	35.28	87.30	NA	NA	77	~82 1.5 ft	48

Startup ~ 25'

## 2. DEVELOPMENT READINGS

TIME (MINUTES)	RATE (gal/min) (ml/min)	DEPTH TO WATER (FEET)	ORP (mV)	D.O. (mg/L)	pH (S.U.)	TEMP (degrees C)	Sp COND. (uS/cm)	Turb (NTU)	Volume (gal) (ml)	Appearance (Silty) (Clear)
10	0.35								3.5	Silty
16	0.58								7.0	
22									10.5	
28									14.0	
33									17.5	
38	0.7								21.0	Cloudy
43									24.5	Cloudy
48									28.0	Silty
53									31.5	Silty
58								492	35.0	Cloudy
63								397	38.5	Cloudy
68									42.0	
73			-31.4	2.68	6.34	10.68	342	802		
80			-38.6	0.12	6.37	10.62	305	854	45.5	
88			-43.3	0.49	6.37	10.67	280	795	49.0	
92			-44.1	1.43	6.39	10.67	285	745	50.0	
94			-43.7	2.40	6.37	10.63	280	653	51.0	

## 3. POST-DEVELOPMENT

END TIME: 1115

TOTAL TIME (MINUTES)	TOTAL VOL (gallons) (milliliters)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)
95	510	35.3	84.1

## ADDITIONAL NOTES:

\* Lateral Pump Inlet  
→ Put onto Flow Cell of FYS1

## WELL DEVELOPMENT DATA FORM

WELL ID: 514-10-01START TEAM MEMBER: PSV + CMHSITE: Fort Devens S/HDATE: 6/30/10PROJECT NO.: AC001TIME: 1350PUMP TYPE & MODEL: Western Hydro LFIWEATHER: 75° Sunny

## 1. INITIAL READINGS

START TIME: 1352

WELL DIAMETER (INCHES)	PID WELL HEAD (PPM)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)	DEPTH TO PRODUCT (FEET)	PRODUCT THICKNESS (FEET)	DEPTH TO SCREEN (FEET)	PUMP DEPTH (FEET)	WELL VOLUME (Gallons) (Milliliters)
1.5	NA	4.57	677	NA	NA	60	65 start	3.9

stick up 3.5'

## 2. DEVELOPMENT READINGS

TIME (MINUTES)	RATE (gal/min) (ml/min)	DEPTH TO WATER (FEET)	ORP (mV)	D.O. (mg/L)	pH (S.U.)	TEMP (degrees C)	SP COND. (uS/cm)	Turb (NTU)	Volume (gal) (ml)	Appearance (Silty) (Clear)
5	0.7								3.5	Brown
8	1.2								7.0	Cloudy
12	0.88								10.5	Clear
16									14.0	Silty
20									17.5	Cloudy
24									21.0	Cloudy
27	1.2								24.5	
30									28.0	
40			338	0.70	5.92	11.22	315	OR	30.5	RBT Int
42			128	0.54	6.09	11.22	315	OR	31.5	
47	0.7		-0.9	0.42	6.19	11.24	315	OR	35.0	
52			-6.0	0.65	6.22	11.29	315	10/6	38.5	
58			-8.4	0.72	6.24	11.23	315	732	42.0	
60			-8.2	0.96	6.24	11.24	315	688	43.5	

## 3. POST-DEVELOPMENT

END TIME: 1452

TOTAL TIME (MINUTES)	TOTAL VOL (gallons) (milliliters)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)
60	43.5	4.55	71.8

## ADDITIONAL NOTES:

\* Lowered Pump Inlet

→ Connected YSI

OR = Out of Range



## WELL DEVELOPMENT DATA FORM

WELL ID: 2HM-10 Q3START TEAM MEMBER: JSV, CMHSITE: Fort DevensDATE: 7/1/2010PROJECT NO.: AC001TIME: 1230PUMP TYPE & MODEL: Waterma HydroLift IWEATHER: Sunny, 75°F

## 1. INITIAL READINGS

START TIME: 1305

WELL DIAMETER (INCHES)	PID WELL HEAD (PPM)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)	DEPTH TO PRODUCT (FEET)	PRODUCT THICKNESS (FEET)	DEPTH TO SCREEN (FEET)	PUMP DEPTH (FEET)	WELL VOLUME (Gallons) (Milliliters)
1.5	NA	26.71	26.71	NA	NA	60	65 SMRT	3.8

Sticky 2'

0.225

## 2. DEVELOPMENT READINGS

TIME (MINUTES)	RATE (gal/min) (ml/min)	DEPTH TO WATER (FEET)	ORP (mV)	D.O. (mg/L)	pH (S.U.)	TEMP (degrees C)	COND. (uS/cm)	Turb (NTU)	Volume (gal) (ml)	Appearance (Silty) (Clear)
7									3.5	Silty
13	0.58								7.0	
24									14.0	Cloudy
30									17.5	Silty
34								904	21.0	Cloudy
1400	Restart after refilling Generator w/ Gas									
44								980	28.0	Cloudy
52								216	35.0	Clear
63								976	38.5	Cloudy
74			-28.1	37.82	6.57	10.33	3580	OR	42.0	
80			-32.8	36.78	6.57	10.37	3584	OR	45.0	
83			-34.0	42.87	6.57	10.31	3583	OR	46.0	
86			-34.9	44.09	6.57	10.33	3581	OR	47.5	
90			-34.5	52.76	6.57	10.34	3579	OR	49.0	

## 3. POST-DEVELOPMENT

END TIME: 1455

TOTAL TIME (MINUTES)	TOTAL VOL (gallons) (milliliters)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)
90	49.0	26.77	64.30

## ADDITIONAL NOTES:

\* Lowered Pump Inlet  
 → Connected YSI  
 OR = Over Range

## WELL DEVELOPMENT DATA FORM

WELL ID: SHM 1010START TEAM MEMBER: PJV + CMHSITE: Fort DevensDATE: 7/1/10PROJECT NO.: AC001TIME: 0930PUMP TYPE & MODEL: Winters Hydro Lift IWEATHER: 75° Sunny

## 1. INITIAL READINGS

START TIME: 0938

WELL DIAMETER (INCHES)	PID WELL HEAD (PPM)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)	DEPTH TO PRODUCT (FEET)	PRODUCT THICKNESS (FEET)	DEPTH TO SCREEN (FEET)	PUMP DEPTH (FEET)	WELL VOLUME (Gallons) (Milliliters)
1.5	NA	1107	61.05	NA	NA	56	60 START	4.6

Shut up - 2'

## 2. DEVELOPMENT READINGS

TIME (MINUTES)	RATE (gal/min) (ml/min)	DEPTH TO WATER (FEET)	ORP (mV)	D.O. (mg/L)	pH (S.U.)	TEMP (degrees C)	SP COND. (uS/cm)	Turb (NTU)	Volume (gal) (ml)	Appearance (Silty) (Clear)
8	0.44								3.5	Silty
12	0.88								7.0	Silty
15									10.5	
20									14.0	
24									17.5	Cloudy
28									21.0	Clear
33									24.5	Silty
36									28.0	Cloudy
40									31.5	Cloudy
44									35.0	
48									38.5	
53								OR	42.0	
58									45.5	Cloudy
60			-31.0	2.76	6.55	11.17	740	OR	46.5	
63			-57.9	4.46	6.12	11.21	730	OR	48.0	
66			-66.7	3.13	6.16	11.18	726	OR	49.0	
69			-86.2	5.50	6.35	11.12	722	OR	51.0	
72			-94.4	2.11	6.40	11.12	716	OR	52.5	
75			-96.2	1.57	6.42	11.15	711	OR	54.0	

## 3. POST-DEVELOPMENT

END TIME: 1055

TOTAL TIME (MINUTES)	TOTAL VOL (gallons) (milliliters)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)
75	54.0	1107	66.40

## ADDITIONAL NOTES:

\* Lowered Pump Inlet  
 → Corrected YSI  
 OR = OUT OF RANGE

## WELL DEVELOPMENT DATA FORM

WELL ID: SHM-10-08START TEAM MEMBER: PSVSITE: Fort DevensDATE: 7/2/10PROJECT NO.: AC001TIME: 0815PUMP TYPE & MODEL: Waters Hydro Lift IWEATHER: 75° Sunny

## 1. INITIAL READINGS

START TIME: 0825

WELL DIAMETER (INCHES)	PID WELL HEAD (PPM)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)	DEPTH TO PRODUCT (FEET)	PRODUCT THICKNESS (FEET)	DEPTH TO SCREEN (FEET)	PUMP DEPTH (FEET)	WELL VOLUME (Gallons) (Milliliters)
1.5	NA	9.99	54.35	NA	NA	46	53 START	4

Slightly 2'

## 2. DEVELOPMENT READINGS

TIME (MINUTES)	RATE (gal/min) (ml/min)	DEPTH TO WATER (FEET)	ORP (mV)	D.O. (mg/L)	pH (S.U.)	TEMP (degrees C)	COND. (uS/cm)	Turb (NTU)	Volume (gal) (ml)	Appearance (Silty) (Clear)
5									3.5	Silty
9	0.78								7.0	Silty
21									17.5	Cloudy
25	0.88								21.0	
28								827	24.5	
32									28.0	Silty
42								687	38.5	Cloudy
45								908	42	
48								469	45.5	Clear
51								273	49.0	
56			-19.2	0.86	6.35	10.43	1141	OR	51.0	Silty
60			-36.2	1.45	6.38	10.43	1143	OR	53.0	
63			-48.7	5.90	6.41	10.43	1142	OR	55.0	Cloudy
67			-57.2	1.67	6.41	10.42	1143	OR	57.0	
70			-63.4	1.19	6.40	10.42	1143	OR	59.0	

## 3. POST-DEVELOPMENT

END TIME: 0935

TOTAL TIME (MINUTES)	TOTAL VOL (gallons) (milliliters)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)
70	59.0	9.45	56.2

## ADDITIONAL NOTES:

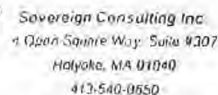
X Lowed Pump Inlet  
 → Connected YSI  
 OR - out of Range

High Pressure on  
 gripper top - Initial  
 DTR may be high



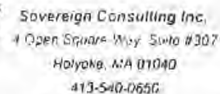


### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]

WELL ID: SHM-10-04

SITE: A1001-002

DATE: 7/6/10

PROJECT NO.: F. Owens

TIME: 1430hr -

PUMP TYPE & MODEL: Waterma

WEATHER: 95°F Sunny

START TIME: 450

WELL DIAMETER (INCHES)	PID WELL HEAD (PPM)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)	DEPTH TO PRODUCT (FEET)	PRODUCT THICKNESS (FEET)	DEPTH TO SCREEN (FEET)	PUMP DEPTH (FEET)	WELL VOLUME (Gallons) (Milliliters)
1 1/2	—	7.86	53.30	—	—			~4

## 2. DEVELOPMENT READINGS

[illegible]

### 3. POST-DEVELOPMENT

END TIME: \_\_\_\_\_

TOTAL TIME (MINUTES)	TOTAL VOL (gallons) (milliliters)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)
75	55	6.72	4.26

ADDITIONAL NOTES:

→ hooked up YSI



AD hooked up ysr

WELL ID: SHM-10-05A

SITE: Ff. Deven's

DATE: 7/7/10

PROJECT NO.: AC001-002

TIME: 0925 - 1040

PUMP TYPE &amp; MODEL: Waterma

WEATHER:

START TIME: 0925

WELL DIAMETER (INCHES)	PID WELL HEAD (PPM)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)	DEPTH TO PRODUCT (FEET)	PRODUCT THICKNESS (FEET)	DEPTH TO SCREEN (FEET)	PUMP DEPTH (FEET)	WELL VOLUME (Gallons) (Milliliters)
1 1/2	—	25.96	58.30	—	—	50	55-60	3

TIME (MINUTES)	RATE (gal/min) (ml/min)	DEPTH TO WATER (FEET)	ORP (mV)	D.O. (mg/L)	pH (S.U.)	TEMP (degrees C)	<del>SPC</del> COND. (uS/cm <sup>2</sup> )	Turb (NTU)	Volume (gal) (ml)	Appearance (Silty) (Clear)
45									3.5	Silty
10				9.71	8.71				7	Cloudy
30			88.6	9.24	8.21				28	Cloudy
35			88.6	9.71	8.29	16.10	229	MAX	29	
40			56.1	10.55	8.71	14.95	228	MAX	30	
45			49.0	10.86	8.78	15.69	223	MAX	31	
50			40.4	10.28	8.92	15.25	222	MAX	32	
55			36.6	10.17	8.98	15.45	220	MAX	33	
60			33.3	11.75	6.03	15.73	218	MAX	34	
65			33.6	10.67	6.02	15.81	218	MAX	35	
70			33.1	10.76	6.03	15.28	220	MAX	36	
75			31.5	10.68	6.03	15.32	220	MAX	37	

END TIME: 1040

TOTAL TIME (MINUTES)	TOTAL VOL (gallons) (milliliters)	DEPTH TO WATER (FEET)	DEPTH TO BOTTOM (FEET)
75	37	25.86	59.90

ADDITIONAL NOTES:

ADDITIONAL NOTES:

- moved tubing to furthest depth
- Set up Y51

### MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]





### Low Flow Sampling



PROJECT NAME: Academy Ft. Devens		PROJECT LOCATION: Ayer, MA		DATE: 7/13/10		WELL ID: SHM-10-01				
PROJECT NUMBER: AC001		WELL DIAMETER: (inches)		DEPTH TO WATER: (feet) 4.57		DEPTH TO BOTTOM: (feet) 71.8		PID READING: (ppmv) NA		
PURGING DATA										
TUBING DIAMETER (inches): 1/2		TUBING MATERIAL CODE (see below) PE		PUMP TYPE: Peristaltic		PUMP EQUIPMENT MODEL & SERIAL #: Gorham 509				
WELL VOLUME PURGE: 1 WELL VOLUME = (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY						GALLONS:	LITERS:			
						6.2	235			
WELL CAPACITY (Gallons Per Foot): 0.75' = 0.02; 1' = 0.04; 1.25' = 0.06; 2' = 0.10; 3' = 0.37; 4' = 0.65; 5' = 1.02; 6' = 1.47; 12' = 5.88						1 GALLON = 3.785 LITERS		TOTAL VOLUME PURGED:		
WELL SCREEN INTERVAL DEPTH (feet): 62-72		INITIAL PUMP OR TUBING DEPTH IN WELL (feet): 65		FINAL PUMP OR TUBING DEPTH IN WELL (feet): 65		PURGING INITIATED AT:  1020	PURGING ENDED AT:  1025	GALLONS:  27.4	LITERS:  28	
WATER LEVEL STABILIZATION					DEPTH TO WATER WITH PUMP: (feet)					
TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS			DEPTH TO WATER (feet) START      END		Water Level Stable (Yes or No)	VOLUME PURGED DURING INTERVAL (mL)		
5	450	0-600 Rpm drive, 68% speed			4.57	4.61		36		
10	400	0-600 Rpm drive 63% speed dial			4.61	4.61	V	56		
5	400	"			4.61	4.61	V	72		
TIME	FLOW RATE (mL/min)	DEPTH TO WATER (feet)	TURBIDITY (NTU)	DISSOLVED OXYGEN (mg/L)	pH	TEMP. (°C)	SPECIFIC CONDUCTIVITY (µS/cm)	ORP (mV)	COLOR (describe)	ODOR (describe)
(3-5 min./day)*	(100-500 mL/min)*	(+/- 0.3')*	(+/- 10%)*	(+/- 10%)*	(+/- 0.1)*	(+/- 324)*	(+/- 300)*	(+/- 10 mV)*		
1025	450									
25	400	4.61	15.1	2.24	6.62	12.86	299	58.8	Clear	None
30	400	4.61	13.6	0.46	6.08	12.59	298	76.1	Clear	None
35	400	4.61	10.45	0.32	5.98	12.66	298	72.3	Clear	None
40	400	4.61	7.10	0.26	6.00	12.48	298	70.7	"	"
45	400	4.61	6.41	0.23	6.09	12.40	297	68.1	"	"
50	400	4.61	5.44	0.20	6.11	12.42	298	66.7	"	"
55	400	4.61	4.83	0.18	6.14	12.37	298	66.4	"	"
60	400	4.61	4.89	0.19	6.18	12.39	297	65.4	"	"
65	400	4.61	3.34	0.18	6.19	12.38	297	63.5	"	"
EPA stabilization parameters from EPA/540/S-95/504 April 1996										
SAMPLING DATA										
SAMPLED BY (PRINT) / AFFILIATION: Philip V. Henneuse SwCon			SAMPLER(S) SIGNATURES: 				SAMPLING INITIATED AT: 1125		SAMPLING ENDED AT: 1205	
PUMP OR TUBING DEPTH IN WELL (feet): 65		SAMPLE PUMP FLOW RATE (mL per minute): 400 ml/min		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #: YSI 30F08H01 Carotto 2/2 c MEM 14843						
FIELD DECONTAMINATION: (Y) N			FIELD FILTERED: (Y) N		FILTER SIZE: 0.45 µm		DUPLICATE: Y (N)			
FILTRATION EQUIPMENT Type: In-line Flow										
MATERIAL CODES:	AG = Amber Glass; CG = Clear Glass; PE = Polyethylene; PP = Polypropylene; S = Silicone; T = Teflon; O = Other (Specify)									
WELL CONDITION CHECKLIST										
Type: Flush Mount (Stand Pipe)	General Condition: Good / Needs Repair		Well Caps: Good / Broken / None		Lock: Good / Broken / None					
Evidence of Rain Water Between Steel & PVC? Y / (N)	Is Well Plumb? (Y) / N		PVC Riser: Good / Damaged / None							
Evidence of Ponding Around Well? (Y) / N	Concrete Collar: Good / Cracked / Leaking / None									
REMARKS: MS/MSD										



### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



PROJECT NAME

ACOWI

PROJECT LOCATION

FT Devens, Ayer, MA

DATE

7/15/10

WELL ID

SHM-10-05A

OBJECT NUMBER

WELL DIAMETER (inches)

1.5"

DEPTH TO WATER (feet)

25.48

DEPTH TO BOTTOM (feet)

52.80

PID READING (ppmv)

PURGING DATA

TUBING DIAMETER (inches)

3/4"

TUBING MATERIAL CODE (see below)

PE

PURGE PUMP TYPE

PERI

PUMP EQUIPMENT MODEL & SERIAL #

WELL VOLUME PURGE: 1 WELL VOLUME: (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY

GALLONS

LITERS

WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1" = 0.04; 1.25 = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

1 GALLON = 3.785 LITERS

TOTAL VOLUME PURGED:

WELL SCREEN INTERVAL DEPTH (feet)

50-60

INITIAL PUMP OR TUBING DEPTH IN WELL (feet)

55'

FINAL PUMP OR TUBING DEPTH IN WELL (feet)

55'

PURGING INITIATED AT:

0935

PURGING ENDED AT:

10:38

GALLONS

LITERS

5

WATER LEVEL STABILIZATION

DEPTH TO WATER WITH PUMP: (feet)

TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS	DEPTH TO WATER (feet) START	DEPTH TO WATER (feet) END	Water Level Stable (Yes or No)	VOLUME PURGED DURING INTERVAL (mL)
10	170	0-1000-ppm, speed dial 100%	25.48	25.91		512
15	100	"	25.91	25.91		12
20	100	"	25.91	25.91		22

TIME (3-5 minutes)*	FLOW RATE (mL/min) (100-500 mL/min)*	DEPTH TO WATER (feet) (1" - 0.3")	TURBIDITY (NTU) (1% - 10%)	DISSOLVED OXYGEN (mg/L) (1% - 10%)	pH (4 - 9.1)*	TEMP (°C) (1 - 35)*	SPECIFIC CONDUCTIVITY (µS/cm) (1 - 300)*	ORP (mV) (1 - 10mV)*	COLOR (describe)	ODOR (describe)
30	100	25.91	11.3	2.75	6.36	17.71	220	20.3	clear	none
35	100	25.91	11.6	2.27	6.32	17.60	205	22.58		
40	100	25.91	7.86	2.03	6.27	17.90	196	25.1		
45	80	25.91	6.61	1.96	6.27	18.21	190	27.2		
50	80	25.91	5.10	1.75	6.27	18.43	184	28.0		
55	80	25.91	5.17	1.46	6.30	18.64	187	29.6		
60	90	25.91	5.37	1.43	6.29	18.87	187	31.3		
65	90	25.91	5.12	1.42	6.29	19.06	186	31.7		

EPA stabilization parameters from EPA/600/S-93/004, April 1996

SAMPLING DATA

SAMPLED BY (PRINT) / AFFILIATION:

Carolyn Hacht / Smacon

SAMPLER'S SIGNATURES

Carolyn Hacht

SAMPLING INITIATED AT:

10:40

SAMPLING ENDED AT:

11:25

PUMP OR TUBING DEPTH IN WELL (feet)

55

SAMPLE PUMP FLOW RATE (mL per minute)

90

FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #:

FIELD DECONTAMINATION ☒ N

FIELD FILTERED ☒ N

FILTER SIZE \_\_\_\_\_ µm

DUPLICATE ☒ N

MATERIAL CODES

AG = Amber Glass, CG = Clear Glass, PE = Polyethylene, PP = Polypropylene, S = Silicone, T = Teflon, O = Other (Specify)

WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)

Type: ☒ Flush Mount / ☒ Stand Pipe

General Condition: ☒ Good / ☒ Needs Repair

Well Caps: ☒ Good / ☒ Broken / ☒ None

Lock: ☒ Good / ☒ Broken / ☒ None

Evidence of Rain Water Between Steel & PVC? ☒ Y / ☒ N

Is Well Plumb? ☒ Y / ☒ N

PVC Riser: ☒ Good / ☒ Damaged / ☒ None

Evidence of Ponding Around Well? ☒ Y / ☒ N

Concrete Collar: ☒ Good / ☒ Cracked / ☒ Leaking / ☒ None

REMARKS:

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
4 Open Square Way, Suite #307  
Holyoke, MA 01040  
413-540-0650

PROJECT NAME: <b>Fort Devens</b>		PROJECT LOCATION: <b>Ayer MA</b>		DATE: <b>7/15/10</b>		WELL ID: <b>SH-10-02</b>				
PROJECT NUMBER: <b>AC001</b>		WELL DIAMETER (inches): <b>1.5</b>		DEPTH TO WATER (feet): <b>18.03</b>		DEPTH TO BOTTOM (feet): <b>64</b>				
TUBING DIAMETER (inches): <b>1 1/2</b>		TUBING MATERIAL CODE: <b>PE</b>		PURGE PUMP TYPE: <b>Peristaltic</b>		PUMP EQUIPMENT MODEL & SERIAL #: <b>Geopump 466</b>				
WELL VOLUME PURGE: 1 WELL VOLUME = (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY				GALLONS: <b>2.710</b>		LITERS: <b>10.28</b>				
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88				1 GALLON = 3.785 LITERS		TOTAL VOLUME PURGED: <b>25</b>				
WELL SCREEN INTERVAL DEPTH (feet): <b>55-65</b>		INITIAL PUMP OR TUBING DEPTH IN WELL (feet): <b>60</b>		FINAL PUMP OR TUBING DEPTH IN WELL (feet): <b>60</b>		PURGING INITIATED AT: <b>1158</b>				
				PURGING ENDED AT: <b>1248</b>		LITERS: <b>25</b>				
WATER LEVEL STABILIZATION				DEPTH TO WATER WITH PUMP (feet): <b>18.07</b>						
TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS		DEPTH TO WATER (feet) START	DEPTH TO WATER (feet) END	Water Level Stable (Yes or No)	VOLUME PURGED DURING INTERVAL (mL)			
0-5	500	600RPM Drive 66% Speed		18.03	18.07		3L			
5-10	500	"		18.07	18.07	Y	25L			
10-15	500	"		18.07	18.07	Y	25L			
TIME	FLOW RATE (mL/min)	DEPTH TO WATER (feet)	TURBIDITY (NTU)	DISSOLVED OXYGEN (mg/L)	pH	TEMP (°C)	SPECIFIC CONDUCTIVITY (µS/cm)	ORP (mV)	COLOR (describe)	ODOR (describe)
(3-6 minutes)*	(100-500 mL/min)*	(± 0.2")	(± 10%)	(± 10%)	(± 0.1)	(± 2%)	(± 2%)	(± 10mV)		
20	500	18.07	3.72	0.33	6.54	12.53	837	69.7	Clear	None
25	500	18.07	3.94	0.45	6.53	12.36	834	77.1	"	"
30	500	18.07	3.32	0.31	6.50	12.33	832	78.3	"	"
35	500	18.07	3.61	0.47	6.45	12.32	835	79.5	"	"
40	500	18.07	3.81	0.43	6.44	12.21	836	79.6	"	"
43	500	18.07	3.70	0.42	6.43	12.19	837	80.6	"	"
46	500	18.07	3.84	0.44	6.43	12.23	838	80.1	"	"
50	500	18.07	3.47	0.45	6.42	12.24	836	80.8	"	"
* EPA stabilization parameters from EPA/540/S-95/504 April 1996										
SAMPLING DATA										
SAMPLED BY (PRINT) / AFFILIATION: <b>Philip V. Hogue / SoGen</b>			SAMPLER SIGNATURE: <i>[Signature]</i>			SAMPLING INITIATED AT: <b>1250</b>		SAMPLING ENDED AT: <b>1335</b>		
PUMP OR TUBING DEPTH IN WELL (feet): <b>60</b>		SAMPLE PUMP FLOW RATE (mL per minute): <b>500</b>		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #: <b>YSI 556 30F081101 Latitude ME 14893</b>						
FIELD DECONTAMINATION: <b>(Y) N</b>			FIELD FILTERED: <b>(Y) N</b>			FILTER SIZE: <b>0.45 µm</b>		DUPLICATE: <b>(Y) N</b>		
MATERIAL CODES: AG = Amber Glass; CG = Clear Glass; PE = Polyethylene; PP = Polypropylene; S = Silicone; T = Teflon; O = Other (Specify)										
WELL CONDITION CHECKLIST										
Type: <b>Flush Mount / Stand Pipe</b>		General Condition: <b>Good</b>		Needs Repair		Well Caps: <b>Good</b>		Broken / None		Lock: <b>Good</b>
Evidence of Rain Water Between Steel & PVC? <b>Y / (N)</b>		Is Well Plumb?: <b>Y / (N)</b>		PVC Riser: <b>Good</b>		Damaged / None				
Evidence of Ponding Around Well? <b>Y / (N)</b>		Concrete Collar: <b>Good</b>		Cracked / Leaking / None						
REMARKS: <b>DUP 071510-U+F</b>										



## MONITORING WELL SAMPLING LOG



Vertical Profiling - DPT

[illegible]



## MONITORING WELL SAMPLING LOG



Vertical Profiling - DPT  
Low Flow Sampling  
LOCATION: Stevens Ave

[illegible]

### MONITORING WELL SAMPLING LOG

### Low Flow Sampling

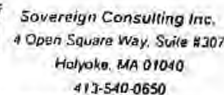
[illegible]





## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

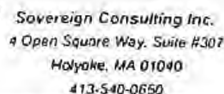
### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]





### Low Flow Sampling



PROJECT NAME

AC00002

PROJECT LOCATION

Davens/Ayer

DATE

8/3/2010

WELL ID

SHW-10-18

OBJECT NUMBER

WELL DIAMETER (inches)

DEPTH TO WATER (feet)

DEPTH TO BOTTOM (feet)

PID READING (spmv)

PURGING DATA

TUBING DIAMETER (inches)

1/4"

TUBING MATERIAL CODE (see below)

Poly

PURGE PUMP TYPE

Geopump

PUMP EQUIPMENT MODEL & SERIAL #s

WELL VOLUME PURGE: 1 WELL VOLUME: (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY

GALLONS

LITERS

WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.89

1 GALLON = 3.785 LITERS

TOTAL VOLUME PURGED:

WELL SCREEN INTERVAL DEPTH (feet)

46-48

INITIAL PUMP OR TUBING DEPTH IN WELL (feet)

47

FINAL PUMP OR TUBING DEPTH IN WELL (feet)

47-48

PURGING INITIATED AT:

10:55

PURGING ENDED AT:

11:43

GALLONS:

LITERS:

WATER LEVEL STABILIZATION

DEPTH TO WATER WITH PUMP (feet)

TIME INTERVAL (min)

FLOW RATE (mL/min)

PUMP SETTINGS

DEPTH TO WATER (feet) START

DEPTH TO WATER (feet) END

Water Level Stable (Yes or No)

VOLUME PURGED DURING INTERVAL (mL)

TIME

FLOW RATE (mL/min)

DEPTH TO WATER (feet)

TURBIDITY (NTU)

DISSOLVED OXYGEN (mg/L)

pH

TEMP (°C)

SPECIFIC CONDUCTIVITY (µS/cm)

ORP (mV)

COLOR (describe)

ODOR (describe)

(3-6 minutes)

(100-500 mL/min)

(± 0.3')

(± 10%)

(± 10%)

(± 0.1)

(± 0.5)

(± 10%)

(± 10mV)

11:08

300

47'

801

0.65

6.52

15.28

808

-66.2

cloudy

none

11:15

300

47'

469

0.42

6.53

14.76

791

-77.1

cloudy

none

11:23

300

47'

288

0.44

6.54

14.73

809

-80.1

cloudy

none

11:27

300

47'

127

0.45

6.54

14.60

809

-80.7

little cloudy

none

EPA stabilization parameters from EPA/540/S-95/504 April 1996

SAMPLING DATA

SAMPLED BY (PRINT) / AFFILIATION

SAVCon

SAMPLER(S) SIGNATURES

OR

SAMPLING INITIATED AT:

11:30

SAMPLING ENDED AT:

11:43

PUMP OR TUBING DEPTH IN WELL (feet)

47

SAMPLE PUMP FLOW RATE (mL per minute)

300

FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s

FIELD DECONTAMINATION: ☒ N

FIELD FILTERED: ☒ N

FILTER SIZE \_\_\_\_\_ µm

DUPPLICATE ☒ N

MATERIAL CODES

AG = Amber Glass; CG = Clear Glass; PE = Polyethylene; PP = Polypropylene; S = Silicone; T = Teflon; O = Other (Specify)

WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe

General Condition: Good / Needs Repair

Well Caps: Good / Broken / None

Lock: Good / Broken / None

Presence of Rain Water Between Steel & PVC? Y / N

Is Well Plumb?: Y / N

PVC Riser: Good / Damaged / None

Presence of Ponding Around Well? Y / N

Concrete Collar: Good / Cracked / Leaking / None

REMARKS:

GP-10-18-047 -U  
-F

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



Vertical Profiling - DPT

[illegible]

### MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]





Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
4 Open Square Way, Suite #307  
Holyoke, MA 01040  
413-540-0650

**PROJECT NAME:** SAL **PROJECT LOCATION:** STM-10-11 **DATE:** 8/3/10 **WELL ID:** STM-10-11

**OBJECT NUMBER:** A000002 **WELL DIAMETER (inches):** 4" **DEPTH TO WATER (feet):** 39.46 **DEPTH TO BOTTOM (feet):** 40 **PID READING (ppmv):** 0

**PURGING DATA:**

**TUBING DIAMETER (inches):** 5/8 **TUBING MATERIAL CODE:** PE **PURGE PUMP TYPE:** bladder/stainless **PUMP EQUIPMENT MODEL & SERIAL #:**

**WELL VOLUME PURGE:** 1 WELL VOLUME = (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY

**WELL CAPACITY (Gallons Per Foot):** 0.75 = 0.02, 1" = 0.04, 1.25" = 0.06, 2" = 0.16, 3" = 0.37, 4" = 0.65, 5" = 1.02, 6" = 1.47, 12" = 5.80 **1 GALLON = 3.785 LITERS**

**WELL SCREEN INTERVAL DEPTH (feet):** 38-40 **INITIAL PUMP OR TUBING DEPTH IN WELL (feet):** 39 **FINAL PUMP OR TUBING DEPTH IN WELL (feet):** 39 **PURGING INITIATED AT:** 11:50 AM **PURGING ENDED AT:** 1220 **GALLONS:** 23.5 **LITERS:**

**WATER LEVEL STABILIZATION** **DEPTH TO WATER WITH PUMP (feet):** 38.1

TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS	DEPTH TO WATER (feet) START	DEPTH TO WATER (feet) END	Water Level Stable (Yes or No)	VOLUME PURGED DURING INTERVAL (mL)
11:50 AM	400	4CPM / 75psi	39.46	—	N/A	N/A
12:00	400	4CPM / 75psi	39.69	—	No	4 Liters
12:10	350	4CPM / 70psi	39.92	—	Yes	—

TIME	FLOW RATE (mL/min)	DEPTH TO WATER (feet)	TURBIDITY (NTU)	DISSOLVED OXYGEN (mg/L)	pH	TEMP (°C)	SPECIFIC CONDUCTIVITY (µS/cm)	ORP (mV)	COLOR (describe)	ODOR (describe)
11:55	400	39.46	259	4.96	6.64	19.68	307	171.0	CLDY	None
12:00	400	39.69	47.4	2.11	6.06	18.42	305	150.3	CLDY	None
12:10	350	39.92	27.6	0.87	5.72	16.70	301	95.1	Clear	None
12:15	250	39.93	18.7	0.60	5.66	16.40	301	68.4	Clear	None
1220	250	39.92	14.5	0.44	5.61	16.26	302	57.2	Clear	None

\* EPA stabilization parameters from EPA/600/S-95/504 April 1996

**SAMPLING DATA**

**SAMPLED BY (PRINT) / AFFILIATION:** EMB/SC **SAMPLER(S) SIGNATURES:** [Signature] **SAMPLING INITIATED AT:** 1225 **SAMPLING ENDED AT:** 1250

**PUMP OR TUBING DEPTH IN WELL (feet):** 39 **SAMPLE PUMP FLOW RATE (mL per minute):** 250 **FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #:**

**FIELD DECONTAMINATION:** (1) N **FIELD-FILTERED:** Y N **FILTER SIZE:** µm **Filtration Equipment Type:** [Signature] N

**MATERIAL CODES:** AG = Amber Glass, CG = Clear Glass, PE = Polyethylene, PP = Polypropylene, S = Silicone, T = Teflon, O = Other (Specify)

**WELL CONDITION CHECKLIST** (circle appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe General Condition: Good / Needs Repair Well Caps: Good / Broken / None Lock: Good / Broken / None

Presence of Rain Water Between Steel & PVC? Y / N Is Well Plumb?: Y / N PVC Riser: Good / Damaged / None

Presence of Ponding Around Well? Y / N Concrete Collar: Good / Cracked / Leaking / None

**REMARKS:**



Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
4 Open Square Way, Suite #307  
Holyoke, MA 01040  
413-540-0650

Vertical Profiling - Photometric

PROJECT NAME: <b>SHL</b>	PROJECT LOCATION: <b>STM-10-11</b>	DATE: <b>8/3/10</b>	WELL ID: <b>STM-10-11</b>
OBJECT NUMBER: <b>ACC0002</b>	WELL DIAMETER (inches): <b>4"</b>	DEPTH TO WATER (feet): <b>39.01</b>	DEPTH TO BOTTOM (feet): <b>50</b>
PURGING DATA		PID READING (ppmv): <b>N/A</b>	

TUBING DIAMETER (inches): <b>5/8</b>	TUBING MATERIAL CODE (see below): <b>PE</b>	PURGE PUMP TYPE: <b>Bladder/Stainless Steel</b>	PUMP EQUIPMENT MODEL & SERIAL #:
WELL VOLUME PURGE: 1 WELL VOLUME (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY		GALLONS:	LITERS:
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1 = 0.04; 1.25 = 0.06; 2 = 0.16; 3 = 0.37; 4 = 0.65; 5 = 1.02; 6 = 1.47; 12 = 5.88		1 GALLON = 3.785 LITERS	
WELL SCREEN INTERVAL DEPTH (feet): <b>48-50</b>	INITIAL PUMP OR TUBING DEPTH IN WELL (feet): <b>49</b>	FINAL PUMP OR TUBING DEPTH IN WELL (feet): <b>49</b>	PURGING INITIATED AT: <b>1340</b>
WATER LEVEL STABILIZATION		PURGING ENDED AT: <b>14:20</b>	TOTAL VOLUME PURGED: <b>3.5G</b>

TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS	DEPTH TO WATER (feet) START	DEPTH TO WATER (feet) END	Water Level Stable (Yes or No)	VOLUME PURGED DURING INTERVAL (mL)
13:50	290mL	4CPM / 130psi	40.01			
13:55	280mL	4CPM / 130psi	40.01	39.41	N/A	NIL
14:10	300mL	4CPM / 140psi	39.41	39.35	Almost	N/A

TIME (3-5 minutes)	FLOW RATE (100-500 mL/min)	DEPTH TO WATER (feet) (+/- 0.3')	TURBIDITY (NTU) (+/- 10%)	DISSOLVED OXYGEN (mg/L) (+/- 10%)	pH (+/- 0.1)	TEMP (°C) (+/- 0.4)	SPECIFIC CONDUCTIVITY (µS/cm) (+/- 5%)	ORP (mV) (+/- 10mV)	COLOR (describe)	ODOR (describe)
14:00	250	39.30	2646	0.20	6.25	18.1	274	-44.5	Cloudy	None
14:05	270	39.15	3319	0.26	6.20	18.40	275	-45.8	Cloudy	None
14:10	280	39.25	5807	0.53	6.25	18.94	274	-45.1	Cloudy	None
14:15	300	39.45	6105	0.20	6.19	18.46	274	-43.4	Cloudy	None
14:20	300	39.31	5373	0.27	6.20	18.09	278	-43.7	Cloudy	None

\* EPA stabilization parameters from EPA/540/S-95/004 April 1996

SAMPLED BY (PRINT) / AFFILIATION: <b>EDS, LLC</b>		SAMPLER(S) SIGNATURES: <i>[Signature]</i>		SAMPLING INITIATED AT: <b>14:25</b>	SAMPLING ENDED AT: <b>14:50</b>
PUMP OR TUBING DEPTH IN WELL (feet): <b>49'</b>	SAMPLE PUMP FLOW RATE (mL per minute): <b>300mL/min</b>	FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #:			
FIELD DECONTAMINATION: <input checked="" type="radio"/> Y <input type="radio"/> N		FIELD FILTERED: <input checked="" type="radio"/> Y <input type="radio"/> N		FILTER SIZE: <b>0.45µm</b>	
MATERIAL CODES: BG = Amber Glass CG = Clear Glass PE = Polyethylene PP = Polypropylene S = Silicone T = Teflon O = Other (Specify)		Filtration Equipment Type: <b>Both</b>		DUPLICATE: <input checked="" type="radio"/> Y <input type="radio"/> N	

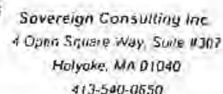
## WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe General Condition: Good / Needs Repair Well Caps: Good / Broken / None Lock: Good / Broken / None  
 Evidence of Rain Water Between Steel & PVC? Y / N Is Well Plumb? Y / N PVC Riser: Good / Damaged / None  
 Evidence of Ponding Around Well? Y / N Concrete Collar: Good / Cracked / Leaking / None

REMARKS:



### Low Flow Sampling

[illegible]





### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



PROJECT NAME: **Acro 002**

PROJECT LOCATION: **Dakota / Aler**

DATE: **8/4/10**

WELL ID: **SHM-10-21**

PROJECT NUMBER:

WELL DIAMETER (inches):

DEPTH TO WATER (feet):

DEPTH TO BOTTOM (feet):

PID READING (ppmv):

PURGING DATA

TUBING DIAMETER (inches): **1/4"**

TUBING MATERIAL CODE (see below): **Poly**

PURGE PUMP TYPE: **Geopump**

PUMP EQUIPMENT MODEL & SERIAL #s:

WELL VOLUME PURGE: 1 WELL VOLUME (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY

GALLONS:

LITERS:

WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

1 GALLON = 3.785 LITERS

TOTAL VOLUME PURGED:

WELL SCREEN INTERVAL DEPTH (feet): **20-22.21**

INITIAL PUMP OR TUBING DEPTH IN WELL (feet): **21**

FINAL PUMP OR TUBING DEPTH IN WELL (feet): **21 20-22.21**

PURGING INITIATED AT: **14:45**

PURGING ENDED AT: **15:25**

GALLONS:

LITERS:

WATER LEVEL STABILIZATION

DEPTH TO WATER WITH PUMP (feet):

TIME INTERVAL (min)

FLOW RATE (mL/min)

PUMP SETTINGS

DEPTH TO WATER (feet) START

DEPTH TO WATER (feet) END

Water Level Stable (Yes or No)

VOLUME PURGED DURING INTERVAL (mL)

TIME	FLOW RATE (mL/min)	DEPTH TO WATER (feet)	TURBIDITY (NTU)	DISSOLVED OXYGEN (mg/L)	pH	TEMP (°C)	SPECIFIC CONDUCTIVITY (µS/cm)	ORP (mV)	COLOR (describe)	ODOR (describe)
(3-5 min/interval)	(100-500 mL/min)	(1" = 0.3')	(1" = 10%)	(1" = 10%)	(1" = 0.1)	(1" = 70)	(1" = 100)	(1" = 10mV)		
14:40	350	21'	1,000	5.13	6.05	15.94	695	93.8	cloudy/silty	none
14:55	350	21'	790	2.77	6.08	15.36	725	88.4	cloudy	none
15:06	360	21'	134	1.43	6.07	14.27	728	97.5	little cloudy	none

EPA stabilization parameters from EPA/540/S-95/504 April 1996

CANENING DATA

SAMPLED BY (PRINT) / AFFILIATION: **SaGen**

SAMPLER(S) SIGNATURES: **qe**

SAMPLING INITIATED AT: **15:15**

SAMPLING ENDED AT: **15:25**

PUMP OR TUBING DEPTH IN WELL (feet): **21**

SAMPLE PUMP FLOW RATE (mL per minute): **350**

FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s:

FIELD DECONTAMINATION: **(C) N**

FIELD FILTERED: **(Y) N**

FILTER SIZE: **µm**

DUPLICATE

**Metals**

MATERIAL CODES: AG = Amber Glass; CG = Clear Glass; PE = Polyethylene; PP = Polypropylene; S = Silicone; T = Teflon; O = Other (Specify)

WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe

General Condition: Good / Needs Repair

Well Caps: Good / Broken / None

Lock: Good / Broken / None

Presence of Rain Water Between Steel & PVC? Y / N

Is Well Plumb? Y / N

PVC Riser: Good / Damaged / None

Presence of Ponding Around Well? Y / N

Concrete Collar: Good / Cracked / Leaking / None

REMARKS:

**GP-10-21-021-F**  
**-u**  
**DUPA-080410-u**  
**-F**



### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



PROJECT NAME

AC006.002

PROJECT LOCATION

Devens / Ayrer

DATE

8/4/10

WELL ID

SHM-10-21

OBJECT NUMBER

WELL DIAMETER (inches)

DEPTH TO WATER (feet)

DEPTH TO BOTTOM (feet)

PID READING (ppmv)

PURGING DATA

TUBING DIAMETER (inches)

1 1/4"

TUBING MATERIAL CODE (see below)

Poly

PURGE PUMP TYPE

Geopump

PUMP EQUIPMENT MODEL & SERIAL #:

WELL VOLUME PURGE: 1 WELL VOLUME (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY

GALLONS:

LITERS:

WELL CAPACITY (Gallons Per Foot): 0.75 \* 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

1 GALLON = 3.785 LITERS

TOTAL VOLUME PURGED:

WELL SCREEN INTERVAL DEPTH (feet):

40-42

INITIAL PUMP OR TUBING DEPTH IN WELL (feet):

41

FINAL PUMP OR TUBING DEPTH IN WELL (feet):

41 40-42

PURGING INITIATED AT:

16:14

PURGING ENDED AT:

16:44

GALLONS:

LITERS:

WATER LEVEL STABILIZATION

DEPTH TO WATER WITH PUMP (feet)

TIME INTERVAL (min)

FLOW RATE (mL/min)

PUMP SETTINGS

DEPTH TO WATER (feet) START

DEPTH TO WATER (feet) END

Water Level Stable (Yes or No)

VOLUME PURGED DURING INTERVAL (mL)

TIME

FLOW RATE (mL/min)

DEPTH TO WATER (feet)

TURBIDITY (NTU)

DISSOLVED OXYGEN (mg/L)

pH

TEMP (°C)

SPECIFIC CONDUCTIVITY (µS/cm)

ORP (mV)

COLOR (describe)

ODOR (describe)

(3-5 minutes)\*

(100-500 mL/min)\*

(± 0.3')\*

(± 10%)\*

(± 10%)\*

(± 0.1)\*

(± 20)\*

(± 20)\*

(± 10mV)\*

16:15

300

41'

591

2.04

6.51

14.97

617

-22.9

cloudy

none

16:25

300

41'

144

0.98

6.64

14.51

687

-73.9

little cloudy

none

16:30

300

41'

89.7

0.42

6.66

14.14

627

-80.2

clear

none

EPA stabilization parameters from EPA/340/S-95/504 April 1996

SAMPLING DATA

SAMPLED BY (PRINT) / AFFILIATION

SavCon

SAMPLER(S) SIGNATURES

QR

SAMPLING INITIATED AT:

16:35

SAMPLING ENDED AT:

16:44

PUMP OR TUBING DEPTH IN WELL (feet):

41

SAMPLE PUMP FLOW RATE (mL per minute):

300

FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #:

FIELD DECONTAMINATION: (Y) N

FIELD FILTERED: (Y) N

FILTER SIZE: µm

DUPLICATE: Y (N)

MATERIAL CODES

AG = Amber Glass CD = Clear Glass PE = Polyethylene PP = Polypropylene S = Silicone T = Teflon O = Other (Specify)

WELL CONDITION CHECKLIST (check appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe

General Condition: Good / Needs Repair

Well Caps: Good / Broken / None

Lock: Good / Broken / None

Incidence of Rain Water Between Steel & PVC? Y / N

Is Well Plumb? Y / N

PVC Riser: Good / Damaged / None

Incidence of Ponding Around Well? Y / N

Concrete Collar: Good / Cracked / Leaking / None

REMARKS:

GP-10-21-041-U-F



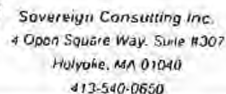


### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]



# MONITORING WELL SAMPLING LOG

### Low Flow Sampling



PROJECT NAME: **Accol-002**

PROJECT LOCATION: **Deverly / Ayer**

DATE: **8/5/10**

WELL ID: **GP-10-23**

OBJECT NUMBER: **14"**

WELL DIAMETER (inches): **14"**

DEPTH TO WATER (feet): **27**

DEPTH TO BOTTOM (feet): **27**

PID READING (pwm): **27**

PURGING DATA

TUBING DIAMETER (inches): **14"**

TUBING MATERIAL CODE (see below): **Poly**

PURGE PUMP TYPE: **Geopump**

PUMP EQUIPMENT MODEL & SERIAL #s:

WELL VOLUME PURGE: 1 WELL VOLUME = (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY

GALLONS:

LITERS:

WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

1 GALLON = 3.785 LITERS

TOTAL VOLUME PURGED:

WELL SCREEN INTERVAL DEPTH (feet): **26-28**

INITIAL PUMP OR TUBING DEPTH IN WELL (feet): **27**

FINAL PUMP OR TUBING DEPTH IN WELL (feet): **27-28**

PURGING INITIATED AT: **10:52**

PURGING ENDED AT: **11:26**

GALLONS:

LITERS:

WATER LEVEL STABILIZATION

TIME INTERVAL (min):

FLOW RATE (mL/min):

PUMP SETTINGS:

DEPTH TO WATER (feet) START:  END:

Water Level Stable (Yes or No):

VOLUME PURGED DURING INTERVAL (mL):

TIME (3-5 minutes)	FLOW RATE (mL/min) (100-500 mL/min)	DEPTH TO WATER (feet) (+/- 0.2')	TURBIDITY (NTU) (+/- 10%)	DISSOLVED OXYGEN (mg/L) (+/- 10%)	pH (+/- 0.1)	TEMP (°C) (+/- 0.5)	SPECIFIC CONDUCTIVITY (µS/cm) (+/- 3%)	ORP (mV) (+/- 10mV)	COLOR (describe)	ODOR (describe)
10:54	350	27'	41,000	3.74	6.11	14.32	1,028	73.1	cloudy	none
10:57	350	27'	797	2.38	6.13	13.99	1,042	66.2	cloudy	none
11:04	350	27'	202	3.23	6.11	14.32	1,063	75.9	cloudy	none
11:15	350	27'	58.5	3.35	6.08	18.10	1,060	94.3	clear	none

EPA stabilization parameters from EPA/540/S-95/004 April 1996

SAMPLING DATA

SAMPLED BY (PRINT) / AFFILIATION: **SovCon**

SAMPLER(S) SIGNATURES: **JK**

SAMPLING INITIATED AT: **11:17**

SAMPLING ENDED AT: **11:26**

PUMP OR TUBING DEPTH IN WELL (feet): **27**

SAMPLE PUMP FLOW RATE (mL per minute): **350**

FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s:

FIELD DECONTAMINATION: **W N**

FIELD FILTERED: **Y N**

FILTER SIZE: **µm**

DUPLICATE: **Y N**

MATERIAL CODES: AG = Amber Glass; CG = Clear Glass; PE = Polyethylene; PP = Polypropylene; S = Silicone; T = Teflon; O = Other (Specify)

WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe

General Condition: Good / Needs Repair

Well Caps: Good / Broken / None

Lock: Good / Broken / None

Incidence of Rain Water Between Steel & PVC? Y / N

Is Well Plumb? Y / N

PVC Riser: Good / Damaged / None

Incidence of Ponding Around Well? Y / N

Concrete Collar: Good / Cracked / Leaking / None

REMARKS: **GP-10-23-027-F**

**MS/MSD**



### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



PROJECT NAME

10001002

PROJECT LOCATION

Duvers/Ayer

DATE

8/5/10

WELL ID

SHM-10-23

OBJECT NUMBER

WELL DIAMETER (inches)

8/4"

DEPTH TO WATER (feet)

DEPTH TO BOTTOM (feet)

PID READING (ppmv)

PURGING DATA

TUBING DIAMETER (inches)

8/4"

TUBING MATERIAL CODE (see below)

PURGE PUMP TYPE

Geopump

PUMP EQUIPMENT MODEL & SERIAL #s

WELL VOLUME PURGE: 1 WELL VOLUME= (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY

GALLONS

LITERS

WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1" = 0.04; 1.25 = 0.06; 2" = 0.16; 3" = 0.32; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

1 GALLON = 3.785 LITERS

TOTAL VOLUME PURGED:

WELL SCREEN INTERVAL DEPTH (feet):

46-48

INITIAL PUMP OR TUBING DEPTH IN WELL (feet):

47

FINAL PUMP OR TUBING DEPTH IN WELL (feet):

47 46-48'

PURGING INITIATED AT:

13:20

PURGING ENDED AT:

14:00

GALLONS:

LITERS:

WATER LEVEL STABILIZATION

DEPTH TO WATER WITH PUMP (feet)

TIME INTERVAL (min)

FLOW RATE (mL/min)

PUMP SETTINGS

DEPTH TO WATER (feet) START

DEPTH TO WATER (feet) END

Water Level Stable (Yes or No)

VOLUME PURGED DURING INTERVAL (mL)

TIME

FLOW RATE (mL/min)

DEPTH TO WATER (feet)

TURBIDITY (NTU)

DISSOLVED OXYGEN (mg/L)

pH

TEMP (°C)

SPECIFIC CONDUCTIVITY (µS/cm)

ORP (mV)

COLOR (describe)

ODOR (describe)

(3-5 minutes)

(100-500 mL/min)

(± 0.3')

(± 10%)

(± 10%)

(± 0.1)

(± 3%)

(µS/cm) (± 1%)

(± 10mV)

13:25

300

47'

60.6

1.47

6.49

16.93

486

-92.7

clear

none

13:31

300

47'

754

1.83

6.56

16.41

494

-95.2

cloudy

none

13:37

300

47'

374

1.34

6.60

15.76

490

-95.1

cloudy

none

EPA stabilization parameters from EPA/540/S-95/504 April 1996

SAMPLING DATA

SAMPLED BY (PRINT) / AFFILIATION:

SAMPLER(S) SIGNATURES:

SAMPLING INITIATED AT:

SAMPLING ENDED AT:

SavCon

9c

13:46

14:00

PUMP OR TUBING DEPTH IN WELL (feet)

SAMPLE PUMP FLOW RATE (mL per minute)

FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s:

47

300

FIELD DECONTAMINATION ☒ N

FIELD FILTERED ☒ N

FILTER SIZE \_\_\_\_\_ µm

DUPLICATE ☐ N

MATERIAL CODES

AG = Amber Glass

CG = Clear Glass

PE = Polyethylene

PP = Polypropylene

S = Silicone

T = Teflon

G = Other (Specify):

WELL CONDITION CHECKLIST (check appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe

General Condition: Good / Needs Repair

Well Caps: Good / Broken / None

Lock: Good / Broken / None

Incidence of Rain Water Between Steel & PVC? Y / N

Is Well Plumb? Y / N

PVC Riser: Good / Damaged / None

Incidence of Ponding Around Wall? Y / N

Concrete Collar: Good / Cracked / Leaking / None

REMARKS:

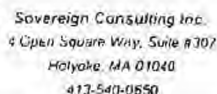
GP-10-23-047-U

-F





### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]





Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

Project Name: A001.002

Date: 5/9/10

Project Location: FT Devens

Project #:

Sampler Name(s): MMH, SSV

WELL IDENTIFICATION: SHP-05-046B

Well Integrity

Protective Casing Secure  
Concrete Pad Intact  
PVC Casing Intact  
Well Gripper Present  
Bolts Present (Pad Wells)  
Locked (Stickup Wells)

YES	NO	N/A
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

Well Information

Diameter: 2"

Depth to Water: 17.00

Material: PVC

Depth to Well Bottom: 27.20

B  
A  
16.49  
75.74

Type of Sampling:

Pump

Disposable Bailor

Field Filtered

Other

Pump Type (if applicable):

Inertial

Submersible

Peristaltic

Other

WELL VOLUME PURGE: 1 WELL VOLUME = (DEPTH TO BOTTOM - DEPTH TO WATER) X WELL CAPACITY (SEE BELOW)  
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

Calculation of One (1) Purge Volume:

1.63

4.59 = 3 well volumes

Purge Start Time: 9:20

Purge End Time: 9:51

Field Water Quality Measurements:

Time	9:38	9:43	9:50		
Temperature (°C)	12.21	12.37	12.43		
Specific Conductivity (uS/cm)	592	656	662		
Dissolved Oxygen (mg/L)	0.45	0.77	0.81		
pH (S.U.)	5.69	5.69	5.71		
ORP (mV)	112.5	12.1	3.0		
Volume Purged (gal)	2	3.5	<del>5.0</del>		

Sample Time: 9:55

NOTES (include well repairs performed and well repairs needed):

Signature of Sampler:

[Signature]

Date:

5/8/10



Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

Project Name: MOOLCOO2

Date: 8/9/10

Project Location: Fort Devens

Project #:

Sampler Name(s): UMH, 55V

WELL IDENTIFICATION: SAM-05-41B(A B C)

Well Integrity

Protective Casing Secure  
Concrete Pad Intact  
PVC Casing Intact  
Well Gripper Present  
Bolts Present (Pad Wells)  
Locked (Stickup Wells)

YES	NO	N/A
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

Well Information

Diameter: 2"

Depth to Water:

Material: PVC

Depth to Well Bottom:

A	B	C
	<u>11.83'</u>	
	<u>64.00</u>	<u>92.6</u>

Type of Sampling:

Pump

Disposable Bailor

Field Filtered

Other

Pump Type (if applicable):

Inertial

Submersible

Peristaltic

Other

WELL VOLUME PURGE: 1 WELL VOLUME = (DEPTH TO BOTTOM - DEPTH TO WATER) X WELL CAPACITY (SEE BELOW)  
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

Calculation of One (1) Purge Volume:

4.34

Purge Start Time: 1235

Purge End Time: 1300

Field Water Quality Measurements

Time	<u>1245</u>	<u>1250</u>			
Temperature (°C)	<u>11.57</u>	<u>11.75</u>	<u>11.75</u>	<u>11.74</u>	<u>11.75</u>
Specific Conductivity (mS/cm)	<u>2310</u>	<u>310</u>	<u>311</u>	<u>311</u>	<u>310</u>
Dissolved Oxygen (mg/L)	<u>0.40</u>	<u>0.37</u>	<u>0.36</u>	<u>0.38</u>	<u>0.32</u>
pH (S.U.)	<u>6.23</u>	<u>6.35</u>	<u>6.38</u>	<u>6.43</u>	<u>6.43</u>
ORP (mV)	<u>-33.4</u>	<u>-34.8</u>	<u>-37.2</u>	<u>42.5</u>	<u>42.6</u>
Volume Purged (gal)	<u>2.5</u>				

Sample Time: 1305

NOTES (Include well repairs performed and well repairs needed):

ms/msd

Signature of Sampler:

[Signature]

Date:

8/9/10



Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

Project Name: Amool 002

Date: 5/9/10

Project Location: Ft Devens

Project #: \_\_\_\_\_

Sampler Name(s): CMH, SSV

WELL IDENTIFICATION: SHP-05-045A

Well Integrity

Protective Casing Secure  
Concrete Pad Intact  
PVC Casing Intact  
Well Gripper Present  
Bole Present (Pad Wells)  
Locked (Stickup Wells)

YES	NO	N/A
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

Well Information

Diameter: 2"

Depth to Water: 18.1

Material: PVC

Depth to Well Bottom: 75.70

AB

BA

17.00

27.19

Type of Sampling:

Pump

Disposable Bailor

Field Filtered

Other \_\_\_\_\_

Pump Type (if applicable):

Inertial

Submersible

Peristaltic

Other \_\_\_\_\_

WELL VOLUME PURGE: 1 WELL VOLUME = (DEPTH TO BOTTOM - DEPTH TO WATER) X WELL CAPACITY (SEE BELOW)  
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

Calculation of One (1) Purge Volume:

1.52

3 well volumes = 4.57

Purge Start Time: 1020

Purge End Time: 1110

Field Water Quality Measurements

Time	<del>1034</del> 1105			
Temperature (°C)	13.22	13.95	13.97	
Specific Conductivity (uS/cm)	296	294	294	
Dissolved Oxygen (mg/L)	0.39	0.30	0.30	
pH (S.U.)	6.18	6.20	6.20	
ORP (mV)	-10.8	-32.0	-32.2	
Volume Purged (gal)	2	6	6.5	

Sample Time: 1115

NOTES (Include well repairs performed and well repairs needed):

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

Signature of Sampler:

Charles Hart

Date:

5/15/10





Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

Project Name: Devers/Ayer

Date: 8/12/2010

Project Location: \_\_\_\_\_

Project #: AC001.002

Sampler Name(s): Matt Crosby, Julie Robshaw

WELL IDENTIFICATION: SHM-07-05

Well Integrity

Protective Casing Secure  
Concrete Pad Intact  
PVC Casing Intact  
Well Gripper Present  
Bolts Present (Pad Wells)  
Locked (Slickup Wells)

YES	NO	N/A
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>

Well Information

Diameter: 2" Depth to Water: 15.41 15.35  
Material: PVC Depth to Well Bottom: 65.5 39.68

Type of Sampling:

Pump

Disposable Bailor

Field Filtered

Other \_\_\_\_\_

Pump Type (if applicable):

Inertial

Submersible

Peristaltic

Other \_\_\_\_\_

WELL VOLUME PURGE: 1 WELL VOLUME = (DEPTH TO BOTTOM - DEPTH TO WATER) X WELL CAPACITY (SEE BELOW)  
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.08; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

Calculation of One (1) Purge Volume:

2.93

Purge Start Time: 9:47

Purge End Time: 10:00

Field Water Quality Measurements

Time	9:53	9:56	10:00		
Temperature (°C)	11.41	11.53	11.43		
Specific Conductivity (uS/cm)	201	240	256		
Dissolved Oxygen (mg/L)	0.38	0.41	0.40		
pH (S.U.)	6.09	6.20	6.45		
ORP (mV)	50.6	26.1	-21.5		
Volume Purged (gal)	1	2	3		

Sample Time: 10:00

NOTES (include well repairs performed and well repairs needed):

SHM-05-40X (next to SHM-07-05) requires new concrete pad.  
(DTW: 15.41) (DTB: 65.5)

Signature of Sampler

QC

Date

8/12/2010



Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

Project Name: Dennis, Ages

Date: 8.12.2010

Project Location: \_\_\_\_\_

Project #: 1001.002

Sampler Name(s): Matt Cooky \* Julie Roberson

WELL IDENTIFICATION: SM-05-42A

Well Integrity

Protective Casing Secure  
Concrete Pad Intact  
PVC Casing Intact  
Well Gripper Present  
Bolts Present (Pad Wells)  
Locked (Silckup Wells)

YES	NO	N/A
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>

Well Information

Diameter: 1" Depth to Water: 6.21  
Material: PVC Depth to Well Bottom: 44.18

Type of Sampling:

Pump

Disposable Bailor

Field Filtered

Other: \_\_\_\_\_

Pump Type (if applicable):

Inertial

Submersible

Peristaltic

Other: \_\_\_\_\_

WELL VOLUME PURGE: 1 WELL VOLUME = (DEPTH TO BOTTOM - DEPTH TO WATER) X WELL CAPACITY (SEE BELOW)  
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

Calculation of One (1) Purge Volume:

1.5

Purge Start Time: 13:20

Purge End Time: 13:35

Field Water Quality Measurements

Time	13:25	13:30	13:35		
Temperature (°C)	10.62	10.46	10.39		
Specific Conductivity (uS/cm)	66	63	61		
Dissolved Oxygen (mg/L)	2.76	1.93	1.20		
pH (S.U.)	6.78	6.64	6.50		
ORP (mV)	88.1	90.4	89.5		
Volume Purged (gal)	0.5	1	1.5		

Sample Time: 13:35

NOTES (include well repairs performed and well repairs needed):

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

Signature of Sampler: \_\_\_\_\_

Date: 8.12.2010



Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

Project Name: Shepley's Hill Landfill Road Date: 8/12/10

Project Location: Exit Devenez, MA Project #: AC001

Sampler Name(s): Jonathan Chaffee, Ryder Murrelman

WELL IDENTIFICATION: SHM-07-03

Well Integrity

Protective Casing Secure  
Concrete Pad Intact  
PVC Casing Intact  
Well Gripper Present  
Bolts Present (Pad Wells)  
Locked (Stickup Wells)

YES	NO	N/A
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>

Well Information

Diameter: 24 Depth to Water: 20.60  
Material: PVC Depth to Well Bottom: 37.47

Type of Sampling:



Disposable Bailor

Field Filtered

Other

Pump Type (if applicable):

Inertial

Submersible

Peristaltic

Other: Bladder

WELL VOLUME PURGE: 1 WELL VOLUME = (DEPTH TO BOTTOM - DEPTH TO WATER) X WELL CAPACITY (SEE BELOW)  
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.68

Calculation of One (1) Purge Volume:

2.08

Purge Start Time: 1200

Purge End Time: 1220

Field Water Quality Measurements

Time	1205	1210	1215	1220
Temperature (°C)	13.00	12.59	12.31	12.25
Specific Conductivity (mS/cm)	76	77	79	81
Dissolved Oxygen (mg/L)	6.84	6.52	6.53	6.61
pH (S.U.)	6.64	6.10	5.91	5.81
ORP (mV)	-103.5	127.2	132.2	133.4
Volume Purged (gal)	~0.25	~0.5	~0.75	~1.0

Sample Time: 1220

NOTES (include well repairs performed and well repairs needed):

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

Signature of Sampler:

RH MHL

Date:

8/12/10





Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

Project Name: Shepley's Hill Landfill Inlet Date: 8/12/10

Project Location: Fort Devens, MA Project #: AC001

Sampler Name(s): Jonathan Chatter, Ryder Musselman

WELL IDENTIFICATION: SHM-99-31B

Well Integrity

Protective Casing Secure  
Concrete Pad Intact  
PVC Casing Intact  
Well Gripper Present  
Bolts Present (Pad Wells)  
Locked (Stickup Wells)

YES	NO	N/A
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>

Well Information

Diameter: 2" Depth to Water: 5.15  
Material: PVC Depth to Well Bottom: 61.5

Type of Sampling:

Pump

Disposable Bailor

Field Filtered

Other

Pump Type (if applicable):

Inertial

Submersible

Peristaltic

Other

WELL VOLUME PURGE: 1 WELL VOLUME = (DEPTH TO BOTTOM - DEPTH TO WATER) X WELL CAPACITY (SEE BELOW)  
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

Calculation of One (1) Purge Volume:

~ 9

Purge Start Time: 1042

Purge End Time: 1110

Field Water Quality Measurements

Time	1050	1055	1100	1105	1110
Temperature (°C)	10.81	10.73	10.69	10.77	10.74
Specific Conductivity (mS/cm)	168	182	184	186	186
Dissolved Oxygen (mg/L)	0.35	0.21	0.21	0.20	0.19
pH (S.U.)	6.05	5.98	5.99	6.00	6.03
ORP (mV)	76.6	47.7	44.2	37.8	33.9
Volume Purged (gal)	~1	~2	~3	~4	~5

Sample Time: 1110

NOTES (Include well repairs performed and well repairs needed):

Signature of Sampler:

J J Cup

Date:

8/12/10



Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

Project Name: Stephens Landfill Investigation Date: 8/12/10

Project Location: Fort Devens, MA Project #: AC001

Sampler Name(s): Jonathan Chaffee, Lyda Misselman

WELL IDENTIFICATION: SHL-23

Well Integrity

Protective Casing Secure  
Concrete Pad Intact  
PVC Casing Intact  
Well Gripper Present  
Bolts Present (Pad Wells)  
Locked (Stickup Wells)

YES	NO	N/A
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>

Well Information

Diameter: 4" Depth to Water: 29.95  
Material: PVC Depth to Well Bottom: 36.0

Type of Sampling:

Pump

Disposable Bailor

Field Filtered

Other: Bladder Pump

Pump Type (if applicable):

Inertial

Submersible

Peristaltic

Other: ↓

WELL VOLUME PURGE: 1 WELL VOLUME = (DEPTH TO BOTTOM - DEPTH TO WATER) X WELL CAPACITY (SEE BELOW)  
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

Calculation of One (1) Purge Volume:

3.9

Purge Start Time: 0835

Purge End Time: 0915

Field Water Quality Measurements

Flow Rate: 250 mL/minute

Time	0845	0855	0905	0915	
Temperature (°C)	10.89	10.93	10.36	10.42	
Specific Conductivity (mS/cm)	31	26	25	25	
Dissolved Oxygen (mg/L)	10.01	10.07	10.02	10.06	
pH (S.U.)	8.52	7.61	6.74	6.45	
ORP (mV)	170.4	188.1	202.1	209.8	
Volume Purged (gal)	~1.0	~1.5	~2.0	~2.5	

Sample Time: 0915

NOTES (include well repairs performed and well repairs needed):

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

Signature of Sampler:

Carlynn Hart

Date:

8/12/10



Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

Project Name Dewens/Ayer

Date 8/12/2010

Project Location \_\_\_\_\_

Project # AC001-002

Sampler Name(s) Matt Crosby, Julie Robshaw

WELL IDENTIFICATION: SHM-05-39A

Well Integrity

Protective Casing Secure  
Concrete Pad Intact  
PVC Casing Intact  
Well Gripper Present  
Bolts Present (Pad Wells)  
Locked (Stickup Wells)

YES	NO	N/A
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>

Well Information

Diameter 2" Depth to Water: 12.68  
Material PVC Depth to Well Bottom: 30.70

Type of Sampling:

Pump

Disposable Bailor

Field Filtered

Other \_\_\_\_\_

Pump Type (if applicable):

Inertial

Submersible

Peristaltic

Other \_\_\_\_\_

WELL VOLUME PURGE: 1 WELL VOLUME = (DEPTH TO BOTTOM - DEPTH TO WATER) X WELL CAPACITY (SEE BELOW)  
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

Calculation of One (1) Purge Volume:

4.16

Purge Start Time: 8:52

Purge End Time: 9:20

Field Water Quality Measurements

Time	9:00	9:15	9:20		
Temperature (°C)	11.59	11.35	11.37		
Specific Conductivity (uS/cm)	252	263	263		
Dissolved Oxygen (mg/L)	0.34	0.35	0.35		
pH (SU)	6.33	6.44	6.45		
ORP (mV)	-19.5	-50.8	-52.9		
Volume Purged (gal)	2	4	5		

Sample Time: 9:20

NOTES (include well repairs performed and well repairs needed):

Well repairs needed.

SHM-05-39B DTW: 13.22'

Signature of Sampler:

Julie Robshaw

Date:

8/12/2010





Sovereign Consulting Inc.  
90513 South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

Project Name: Deverest Ayrer

Date: 8/12/2010

Project Location: \_\_\_\_\_

Project #: AC001.002

Sampler Name(s): Matt Crosby, Julie Robbham

WELL IDENTIFICATION: SHM-10-10

Well Integrity

Protective Casing Secure  
Concrete Pad Intact  
PVC Casing Intact  
Well Gripper Present  
Bolts Present (Pad Wells)  
Locked (Stickup Wells)

YES	NO	N/A
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>

Well Information

Diameter: 1.5" Depth to Water: 11.26  
Material: PVC Depth to Well Bottom: 66.50

Type of Sampling:



Disposable Bailer

Field Filtered

Other \_\_\_\_\_

Pump Type (if applicable):

Vertical

Submersible



Other \_\_\_\_\_

WELL VOLUME PURGE: 1 WELL VOLUME = (DEPTH TO BOTTOM - DEPTH TO WATER) X WELL CAPACITY (SEE BELOW)  
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

Calculation of One (1) Purge Volume: 3.30

Purge Start Time: 11:17

Purge End Time: 11:33

Field Water Quality Measurements

Time	11:23	11:27	11:33		
Temperature (°C)	11.39	11.98	11.27		
Specific Conductivity (uS/cm)	662	691	622		
Dissolved Oxygen (mg/L)	0.60	0.70	0.76		
pH (S.U.)	6.52	6.56	6.57		
ORP (mV)	21.5	-2.3	-9.1		
Volume Purged (gal)	1	2	3		

Sample Time: 11:33

NOTES (include well repairs performed and well repairs needed):

No lock on stick-up well.

Signature of Sampler: [Signature]

Date: 8/12/10



Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

Project Name: Dewens / Aper

Date: 8/12/2010

Project Location: \_\_\_\_\_

Project #: AC001.002

Sampler Name(s): Matt Crosby, Julie Robshaw

WELL IDENTIFICATION: SHM-10-01

**Well Integrity**

Protective Casing Secure  
Concrete Pad Intact  
PVC Casing Intact  
Well Gripper Present  
Bolts Present (Pad Wells)  
Locked (Stickup Wells)

YES	NO	N/A
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>

**Well Information**

Diameter: 1.5"

Depth to Water: 4.66

Material: PVC

Depth to Well Bottom: 71.86

Type of Sampling: Pump

Disposable Bailor

Field Filtered

Other \_\_\_\_\_

Pump Type (if applicable):

Inertial

Submersible

Peristaltic

Other \_\_\_\_\_

WELL VOLUME PURGE: 1 WELL VOLUME = (DEPTH TO BOTTOM - DEPTH TO WATER) X WELL CAPACITY (SEE BELOW)  
WELL CAPACITY (Gallons Per Foot): 0.75" = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

Calculation of One (1) Purge Volume:

4 Gal.

Purge Start Time: 12:25

Purge End Time: 12:40

**Field Water Quality Measurements**

Time	12:30	12:35	12:40		
Temperature (°C)	12.30	11.93	11.86		
Specific Conductivity (uS/cm)	297	292	291		
Dissolved Oxygen (mg/L)	1.38	0.58	0.49		
pH (S.U.)	7.04	6.76	6.61		
ORP (mV)	42.3	41.7	42.2		
Volume Purged (gal)	1.5	2.5	4		

Sample Time: 12:40

NOTES (Include well repairs performed and well repairs needed):

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

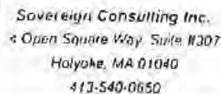
Signature of Sampler

Date:

8.12.2010



### Low Flow Sampling

[illegible]





### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

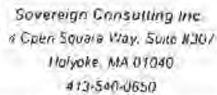
### Low Flow Sampling

[illegible]





### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

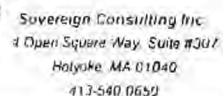
### Low Flow Sampling

[illegible]





### Low Flow Sampling

[illegible]



Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
4 Open Square Way, Suite #301  
Holyoke, MA 01040  
413-540-0650

*Vertical Borehole - Potassium*

*Fast Depress*

PROJECT NAME: AC001002 PROJECT LOCATION: 8/10/2010 WELL ID: SLM-10-13

PROJECT NUMBER: 2593 WELL DIAMETER (inches): 60 DEPTH TO WATER (feet): 60 DEPTH TO BOTTOM (feet): 60 PID READING (ppm): —

**PURGING DATA**

TUBING DIAMETER (inches): 1/4 TUBING MATERIAL CODE (see below): PE PURGE PUMP TYPE: Bladder / Stainless PUMP EQUIPMENT MODEL & SERIAL #:

WELL VOLUME PURGE: 1 WELL VOLUME: (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY GALLONS: — LITERS: —

WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02 1' = 0.04 1.25' = 0.06 2' = 0.10 3' = 0.17 4' = 0.25 5' = 0.37 6' = 0.47 12' = 0.88 1 GALLON = 3.785 LITERS TOTAL VOLUME PURGED: GALLONS: 25 LITERS: —

WELL SCREEN INTERVAL DEPTH (feet): 58-60 INITIAL PUMP OR TUBING DEPTH IN WELL (feet): 59 FINAL PUMP OR TUBING DEPTH IN WELL (feet): 59 PURGING INITIATED AT: 0755 PURGING ENDED AT: 0825

**WATER LEVEL STABILIZATION** DEPTH TO WATER WITH PUMP (feet): 25.93

TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS	DEPTH TO WATER (feet) START	DEPTH TO WATER (feet) END	Water Level Stable (Yes or No)	VOLUME PURGED DURING INTERVAL (mL)
0755	300	LPM: 4 10.0-5.0	25.93	—	N	—

TIME (3.5 min max)	FLOW RATE (mL/min) (100-800 mL/min)	DEPTH TO WATER (feet) (4-10)	TURBIDITY (NTU) (0-100)	DISSOLVED OXYGEN (mg/L) (0-100)	pH (4-12)	TEMP (°C) (4-30)	SPECIFIC CONDUCTIVITY (µS/cm) (1-200)	ORP (mV) (4-100)	COLOR (describe)	ODOR (describe)
0800	300	26.59	506	1.91	7.02	19.92	738	-35.1	Cloudy	None
0805	300	27.15	323	0.53	6.53	19.66	793	-47.9	Cloudy	None
0810	300	27.67	492	0.38	6.47	19.21	805	-46.6	cloudy	NONE
0815	300	27.90	698	0.17	6.42	18.73	802	-36.7	cloudy	NONE
0820	300	28.15	691	0.15	6.40	18.44	800	-33.3	CLOUDY	NONE
0825	300	28.40	565	0.16	6.40	18.34	800	-33.3	CLOUDY	NONE

\* EPA stabilization parameters from EPA/540/S-95/504 April 1996

**SAMPLING DATA**

SAMPLED BY (PRINT) / AFFILIATION: Jonathan Chatter SAMPLER(S) SIGNATURES: [Signature] [Signature] SAMPLING INITIATED AT: 0830 SAMPLING ENDED AT: 0850

PUMP OR TUBING DEPTH IN WELL (feet): 59 SAMPLE PUMP FLOW RATE (mL per minute): 300 FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #:

FIELD DECONTAMINATION: (Y) N FIELD FILTERED: (Y) N FILTER SIZE: 0.45 µm DUPLICATE: (Y) N

MATERIAL CODES: AG = Amber Glass CG = Clear Glass PE = Polyethylene PP = Polypropylene S = Silicone T = Teflon O = Other (Specify)

**WELL CONDITION CHECKLIST** (circle appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe General Condition: Good / Needs Repair Well Caps: Good / Broken / None Lock: Good / Broken / None

Evidence of Rain Water Between Steel & PVC? Y / N Is Well Plumb? Y / N PVC Riser: Good / Damaged / None

Evidence of Ponding Around Well? Y / N Concrete Collar: Good / Cracked / Leaking / None

REMARKS:

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]





Sovereign Consulting Inc.  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3700

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
4 Open Square Way, Suite #307  
Holyoke, MA 01040  
413-540-0650

PROJECT NAME: 10001.002		PROJECT LOCATION: Fort Devens		DATE: 8/10/2010		WELL ID: SM-10-13			
PROJECT NUMBER:		WELL DIAMETER (inches):		DEPTH TO WATER (feet): 37.0		DEPTH TO BOTTOM (feet): 80		PIG READING (ppmv):	
PURGING DATA									
TUBING DIAMETER (inches): 1 1/4		TUBING MATERIAL CODE (see below): PE		PURGE PUMP TYPE: Kshidder / Shindler		PUMP EQUIPMENT MODEL & SERIAL #s:			
WELL VOLUME PURGE: 1 WELL VOLUME (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY						GALLONS: -		LITERS: -	
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02, 1" = 0.04, 1.25" = 0.06, 2" = 0.16, 3" = 0.37, 4" = 0.65, 5" = 1.02, 6" = 1.47, 12" = 5.68						1 GALLON = 3.785 LITERS		TOTAL VOLUME PURGED:	
WELL SCREEN INTERVAL DEPTH (feet): 78 - 80		INITIAL PUMP OR TUBING DEPTH IN WELL (feet): 79		FINAL PUMP OR TUBING DEPTH IN WELL (feet): 79		PURGING INITIATED AT: 1140		PURGING ENDED AT: 1210	
GALLONS: -		LITERS: -		GALLONS: -		LITERS: -		GALLONS: -	
LITERS: -		LITERS: -		LITERS: -		LITERS: -		LITERS: -	
WATER LEVEL STABILIZATION									
TIME INTERVAL (min): 1140		FLOW RATE (mL/min): 250		PUMP SETTINGS: CPM4 / 10.0 - 5.0		DEPTH TO WATER (feet) START: 37.0		Water Level Stable (Yes or No): N	
END:		END:		END:		END:		VOLUME PURGED DURING INTERVAL (mL): -	
TIME									
FLOW RATE									
DEPTH TO WATER									
TURBIDITY (NTU)									
DISSOLVED OXYGEN (mg/L)									
pH									
TEMP (°C)									
SPECIFIC CONDUCTIVITY (µS/cm)									
ORP (mV)									
COLOR (describe)									
ODOR (describe)									
1145									
250									
37.6									
1344									
5.78									
6.76									
25.49									
352									
-4.3									
Cloudy									
None									
1150									
250									
38.3									
530									
6.10									
6.58									
24.44									
342									
-5.6									
Cloudy									
None									
1155									
250									
38.75									
624									
6.50									
6.49									
25.58									
338									
3.1									
Cloudy									
None									
1200									
250									
40.3									
146									
7.55									
6.46									
23.01									
337									
9.1									
Cloudy									
None									
1205									
250									
42.0									
137									
7.67									
6.39									
22.37									
338									
14.9									
Cloudy									
None									
1210									
250									
42.58									
128									
8.68									
6.37									
21.89									
338									
15.9									
Cloudy									
None									
EPA stabilization parameters from EPA/540/5-95/504 April 1996									
SAMPLING DATA									
SAMPLED BY (PRINT) / AFFILIATION: Jonathan Chute		SAMPLER(S) SIGNATURES: J. Chute				SAMPLING INITIATED AT: 12:15		SAMPLING ENDED AT: 12:35	
PUMP OR TUBING DEPTH IN WELL (feet): 79		SAMPLE PUMP FLOW RATE (mL per minute): 250		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s:					
FIELD DECONTAMINATION (Y) (N)		FIELD FILTERED (Y) (N)		FILTER SIZE: 0.45 µm		DUPLICATE (Y) (N)		DUPLICATE (Y) (N)	
MATERIAL CODES: AG = Amber Glass, CG = Clear Glass, PE = Polyethylene, PP = Polypropylene, S = Saccone, T = Teflon, O = Other (Specify):									
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)									
Type: Flush Mount / Stand Pipe General Condition: Good / Needs Repair Well Caps: Good / Broken / None Lock: Good / Broken / None									
Evidence of Rain Water Between Steel & PVC? Y / N Is Well Plumb?: Y / N PVC Riser: Good / Damaged / None									
Evidence of Ponding Around Well? Y / N Concrete Collar: Good / Cracked / Leaking / None									
REMARKS:									

## MONITORING WELL SAMPLING LOG

### Low Elbow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



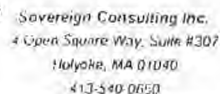
## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



PROJECT NAME

Accolond

PROJECT LOCATION

East Deyens

DATE

8/11/2010

WELL ID

SHM-10-15

OBJECT NUMBER

WELL DIAMETER (inches)

DEPTH TO WATER (feet)

51.2

DEPTH TO BOTTOM (feet)

60

PID READING (ppmv)

PURGING DATA

TUBING DIAMETER (inches)

1/4

TUBING MATERIAL CODE (see below)

PE

PURGE PUMP TYPE

Bladder/Stainless

PUMP EQUIPMENT MODEL & SERIAL #s

WELL VOLUME PURGE: 1 WELL VOLUME= (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY

GALLONS

LITERS

WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

1 GALLON = 3.785 LITERS

TOTAL VOLUME PURGED:

WELL SCREEN INTERVAL DEPTH (feet)

58-60

INITIAL PUMP OR TUBING DEPTH IN WELL (feet)

59

FINAL PUMP OR TUBING DEPTH IN WELL (feet)

59

PURGING INITIATED AT:

1340

PURGING ENDED AT:

1405

GALLONS

~1.5

LITERS

WATER LEVEL STABILIZATION

DEPTH TO WATER WITH PUMP (feet)

TIME INTERVAL (min)

1:40

FLOW RATE (mL/min)

300

PUMP SETTINGS

CPM 4/10.0-5.0

DEPTH TO WATER (feet) START

51.2

DEPTH TO WATER (feet) END

-

Water Level Stable (Yes or No)

N

VOLUME PURGED DURING INTERVAL (mL)

-

TIME

FLOW RATE (mL/min)

DEPTH TO WATER (feet)

TURBIDITY (NTU)

DISSOLVED OXYGEN (mg/L)

pH

TEMP (°C)

SPECIFIC CONDUCTIVITY (µS/cm)

ORP (mV)

COLOR (describe)

ODOR (describe)

1345

300

51.2

782

3.15

7.52

23.10

325

186.2

Cloudy

None

1350

300

51.8

531

4.82

8.02

22.80

307

164.3

cloudy

None

1355

300

52.5

261

5.23

8.26

22.54

310

177.9

Cloudy

None

1400

300

53.15

207

5.11

8.30

21.89

313

181.1

Cloudy

None

EPA stabilization parameters from EPA/540/S-99/504 April 1996

SAMPLING DATA

SAMPLED BY (PRINT) / AFFILIATION

Jonathan Chaffin

SAMPLER(S) SIGNATURES

SAMPLING INITIATED AT:

1410

SAMPLING ENDED AT:

1425

PUMP OR TUBING DEPTH IN WELL (feet)

59

SAMPLE PUMP FLOW RATE (mL per minute)

300

FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s

FIELD DECONTAMINATION

Y N

FIELD FILTERED

Y N

FILTER SIZE

0.5 µm

DUPLICATE

Y N

MATERIAL CODES

AG = Amber Glass CG = Clear Glass PE = Polyethylene PP = Polypropylene S = Silicone T = Teflon O = Other (Specify)

WELL CONDITION CHECKLIST (check appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe

General Condition: Good / Needs Repair

Well Caps: Good / Broken / None

Lock: Good / Broken / None

Sealence of Rain Water Between Steel & PVC? Y / N

Is Well Plumb? Y / N

PVC Riser: Good / Damaged / None

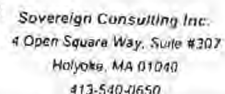
Evidence of Ponding Around Well? Y / N

Concrete Collar: Good / Cracked / Leaking / None

REMARKS:



### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG



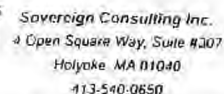
Vertical Pooling - DPT

[illegible]





### Low Flow Sampling

[illegible]

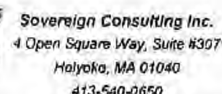


### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]





### Low Flow Sampling



PROJECT NAME:

PROJECT LOCATION:

DATE:

WELL ID:

PROJECT NUMBER:

WELL DIAMETER:

DEPTH TO WATER:

DEPTH TO BOTTOM:

PID READING:

TUBING DIAMETER:

TUBING MATERIAL CODE:

PURGE PUMP TYPE:

PUMP EQUIPMENT MODEL & SERIAL #:

WELL VOLUME PURGE:

GALLONS:

LITERS:

WELL CAPACITY:

WELL SCREEN INTERVAL DEPTH:

INITIAL PUMP OR TUBING DEPTH IN WELL:

FINAL PUMP OR TUBING DEPTH IN WELL:

PURGING INITIATED AT:

PURGING ENDED AT:

GALLONS:

LITERS:

WATER LEVEL STABILIZATION

DEPTH TO WATER WITH PUMP:

TIME INTERVAL:

FLOW RATE:

PUMP SETTINGS:

DEPTH TO WATER:

Water Level Stable:

VOLUME PURGED DURING INTERVAL:

TIME:

FLOW RATE:

DEPTH TO WATER:

TURBIDITY:

DISSOLVED OXYGEN:

pH:

TEMP:

SPECIFIC CONDUCTIVITY:

ORP:

COLOR:

ODOR:

SAMPLED BY:

SAMPLER(S) SIGNATURES:

SAMPLING INITIATED AT:

SAMPLING ENDED AT:

PUMP OR TUBING DEPTH IN WELL:

SAMPLE PUMP FLOW RATE:

FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #:

FIELD DECONTAMINATION:

FIELD FILTERED:

FILTER SIZE:

DUPLICATE:

MATERIAL CODES:

WELL CONDITION CHECKLIST:

Type:

General Condition:

Well Caps:

Lock:

Evidence of Rain Water Between Steel & PVC:

Is Well Plumb:

PVC Riser:

Evidence of Ponding Around Well:

Concrete Collar:

REMARKS:



### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



Vertical Boiling - DPT

[illegible]

### MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### LowFlow Sampling



Vertical Profiling - Photosynthetic

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



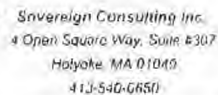
## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]





Sovereign Consulting Inc.  
505B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
4 Open Square Way, Suite 4107  
Holyoke, MA 01040  
413-540-0650

Vertical Profiling - Probsonic

PROJECT NAME <b>Accon 02</b>		PROJECT LOCATION <b>Fort Devens</b>		DATE <b>8/17/2010</b>		WELL ID <b>SHM 10-16</b>																																																																			
PROJECT NUMBER		WELL DIAMETER (inches) <b>8.78</b>	DEPTH TO WATER (feet) <b>8.78</b>	DEPTH TO BOTTOM (feet) <b>25</b>	P/D READING (ppmv)																																																																				
PURGING DATA																																																																									
TUBING DIAMETER (inches) <b>1/4</b>	TUBING MATERIAL CODE (see below) <b>PE</b>	PURGE PUMP TYPE <b>Bladder/Stainless</b>		PUMP EQUIPMENT MODEL & SERIAL #s																																																																					
WELL VOLUME PURGE: 1 WELL VOLUME = (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY				GALLONS <b>—</b>	LITERS <b>—</b>																																																																				
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 6.68				1 GALLON = 3.785 LITERS		TOTAL VOLUME PURGED:																																																																			
WELL SCREEN INTERVAL DEPTH (feet) <b>23-25</b>	INITIAL PUMP OR TUBING DEPTH IN WELL (feet) <b>24</b>	FINAL PUMP OR TUBING DEPTH IN WELL (feet) <b>24</b>	PURGING INITIATED AT <b>1545</b>	PURGING ENDED AT <b>1615</b>	GALLONS <b>—</b>																																																																				
LITERS <b>—</b>																																																																									
WATER LEVEL STABILIZATION																																																																									
TIME INTERVAL (min)		FLOW RATE (mL/min)	PUMP SETTINGS		DEPTH TO WATER (feet) START	DEPTH TO WATER (feet) END	Water Level Stable (Yes or No)																																																																		
<b>1545</b>	<b>400</b>	<b>C#104 = 10.0 / 5.0</b>	<b>8.78</b>	<b>—</b>	<b>N</b>	<b>—</b>	<b>—</b>																																																																		
<table border="1"> <thead> <tr> <th>TIME (3-5 minutes)</th> <th>FLOW RATE (100-500 mL/min)</th> <th>DEPTH TO WATER (16-30")</th> <th>TURBIDITY (&lt; 10%)</th> <th>DISSOLVED OXYGEN (&lt; 10%)</th> <th>pH (&lt; 0.1)</th> <th>TEMP (&lt; 3%)</th> <th>SPECIFIC CONDUCTIVITY (&lt; 2%)</th> <th>ORP (&lt; 10mV)</th> <th>COLOR (describe)</th> <th>ODOR (describe)</th> </tr> </thead> <tbody> <tr> <td>1550</td> <td>400</td> <td>8.70</td> <td>88.0</td> <td>3.37</td> <td>7.43</td> <td>13.84</td> <td>104</td> <td>85.1</td> <td>Cloudy</td> <td>None</td> </tr> <tr> <td>1555</td> <td>400</td> <td>8.71</td> <td>204</td> <td>3.23</td> <td>6.82</td> <td>13.28</td> <td>104</td> <td>82.2</td> <td>Cloudy</td> <td>None</td> </tr> <tr> <td>1600</td> <td>400</td> <td>8.70</td> <td>1199</td> <td>3.18</td> <td>6.34</td> <td>12.94</td> <td>107</td> <td>96.1</td> <td>Silty</td> <td>None</td> </tr> <tr> <td>1605</td> <td>400</td> <td>8.70</td> <td>965</td> <td>3.17</td> <td>6.29</td> <td>12.74</td> <td>107</td> <td>96.8</td> <td>Silty</td> <td>None</td> </tr> <tr> <td>1610</td> <td>400</td> <td>8.75</td> <td>1235</td> <td>3.06</td> <td>6.21</td> <td>12.58</td> <td>107</td> <td>101.1</td> <td>Silty</td> <td>None</td> </tr> </tbody> </table>								TIME (3-5 minutes)	FLOW RATE (100-500 mL/min)	DEPTH TO WATER (16-30")	TURBIDITY (< 10%)	DISSOLVED OXYGEN (< 10%)	pH (< 0.1)	TEMP (< 3%)	SPECIFIC CONDUCTIVITY (< 2%)	ORP (< 10mV)	COLOR (describe)	ODOR (describe)	1550	400	8.70	88.0	3.37	7.43	13.84	104	85.1	Cloudy	None	1555	400	8.71	204	3.23	6.82	13.28	104	82.2	Cloudy	None	1600	400	8.70	1199	3.18	6.34	12.94	107	96.1	Silty	None	1605	400	8.70	965	3.17	6.29	12.74	107	96.8	Silty	None	1610	400	8.75	1235	3.06	6.21	12.58	107	101.1	Silty	None
TIME (3-5 minutes)	FLOW RATE (100-500 mL/min)	DEPTH TO WATER (16-30")	TURBIDITY (< 10%)	DISSOLVED OXYGEN (< 10%)	pH (< 0.1)	TEMP (< 3%)	SPECIFIC CONDUCTIVITY (< 2%)	ORP (< 10mV)	COLOR (describe)	ODOR (describe)																																																															
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1600	400	8.70	1199	3.18	6.34	12.94	107	96.1	Silty	None																																																															
1605	400	8.70	965	3.17	6.29	12.74	107	96.8	Silty	None																																																															
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SAMPLING DATA																																																																									
SAMPLED BY (PRINT) / AFFILIATION <b>Jonathan Chapple</b>		SAMPLE(S) SIGNATURES <b>[Signature]</b>		SAMPLING INITIATED AT <b>1615</b>		SAMPLING ENDED AT <b>1635</b>																																																																			
PUMP OR TUBING DEPTH IN WELL (feet) <b>24</b>	SAMPLE PUMP FLOW RATE (mL per minute) <b>400</b>	FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s																																																																							
FIELD DECONTAMINATION <input checked="" type="checkbox"/> N		FIELD-FILTERED <input checked="" type="checkbox"/> N		FILTER SIZE <b>45</b> $\mu$ m		DUPLICATE <input checked="" type="checkbox"/> N																																																																			
MATERIAL CODES AG = Amber Glass CG = Clear Glass PE = Polyethylene PP = Polypropylene S = Silicone T = Teflon D = Other (Specify)																																																																									
WELL CONDITION CHECKLIST (Check appropriate item(s), cross out if not applicable)																																																																									
Type: Flush Mount / Stand Pipe		General Condition: Good / Needs Repair		Well Caps: Good / Broken / None		Lock: Good / Broken / None																																																																			
Evidence of Rain Water Between Steel & PVC? Y / N		Is Well Plumb?: Y / N		PVC Riser: Good / Damaged / None																																																																					
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REMARKS:																																																																									



Sovereign Consulting Inc.  
905B South Main Street, Suite 2107  
Mansfield, MA 02048  
508-339-3200

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
1 Open Square Way, Suite #307  
Holyoke, MA 01040  
413-540-0550

PROJECT NAME <b>Accol-02</b>		PROJECT LOCATION <b>Fort Devens</b>		DATE <b>8/18/2010</b>	WELL ID <b>S4M-10-16</b>
PROJECT NUMBER		WELL DIAMETER (inches)	DEPTH TO WATER (feet)	DEPTH TO BOTTOM (feet)	PID READING (ppmv)
			<b>31.3</b>	<b>35</b>	
PURGING DATA					
TUBING DIAMETER (inches)	TUBING MATERIAL CODE (see below)	PURGE PUMP TYPE		PUMP EQUIPMENT MODEL & SERIAL #s	
<b>1.25</b>	<b>PE</b>	<b>Sturges / Sturges</b>			
WELL VOLUME PURGE: 1 WELL VOLUME = (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY				GALLONS	LITERS
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02, 1" = 0.04, 1.25" = 0.06, 1.5" = 0.08, 1.75" = 0.10, 2" = 0.12, 2.25" = 0.14, 2.5" = 0.16, 2.75" = 0.18, 3" = 0.20, 3.25" = 0.22, 3.5" = 0.24, 3.75" = 0.26, 4" = 0.28, 4.25" = 0.30, 4.5" = 0.32, 4.75" = 0.34, 5" = 0.36, 5.25" = 0.38, 5.5" = 0.40, 5.75" = 0.42, 6" = 0.44, 6.25" = 0.46, 6.5" = 0.48, 6.75" = 0.50, 7" = 0.52, 7.25" = 0.54, 7.5" = 0.56, 7.75" = 0.58, 8" = 0.60, 8.25" = 0.62, 8.5" = 0.64, 8.75" = 0.66, 9" = 0.68, 9.25" = 0.70, 9.5" = 0.72, 9.75" = 0.74, 10" = 0.76, 10.25" = 0.78, 10.5" = 0.80, 10.75" = 0.82, 11" = 0.84, 11.25" = 0.86, 11.5" = 0.88, 11.75" = 0.90, 12" = 0.92, 12.25" = 0.94, 12.5" = 0.96, 12.75" = 0.98, 13" = 1.00, 13.25" = 1.02, 13.5" = 1.04, 13.75" = 1.06, 14" = 1.08, 14.25" = 1.10, 14.5" = 1.12, 14.75" = 1.14, 15" = 1.16, 15.25" = 1.18, 15.5" = 1.20, 15.75" = 1.22, 16" = 1.24, 16.25" = 1.26, 16.5" = 1.28, 16.75" = 1.30, 17" = 1.32, 17.25" = 1.34, 17.5" = 1.36, 17.75" = 1.38, 18" = 1.40, 18.25" = 1.42, 18.5" = 1.44, 18.75" = 1.46, 19" = 1.48, 19.25" = 1.50, 19.5" = 1.52, 19.75" = 1.54, 20" = 1.56, 20.25" = 1.58, 20.5" = 1.60, 20.75" = 1.62, 21" = 1.64, 21.25" = 1.66, 21.5" = 1.68, 21.75" = 1.70, 22" = 1.72, 22.25" = 1.74, 22.5" = 1.76, 22.75" = 1.78, 23" = 1.80, 23.25" = 1.82, 23.5" = 1.84, 23.75" = 1.86, 24" = 1.88, 24.25" = 1.90, 24.5" = 1.92, 24.75" = 1.94, 25" = 1.96, 25.25" = 1.98, 25.5" = 2.00, 25.75" = 2.02, 26" = 2.04, 26.25" = 2.06, 26.5" = 2.08, 26.75" = 2.10, 27" = 2.12, 27.25" = 2.14, 27.5" = 2.16, 27.75" = 2.18, 28" = 2.20, 28.25" = 2.22, 28.5" = 2.24, 28.75" = 2.26, 29" = 2.28, 29.25" = 2.30, 29.5" = 2.32, 29.75" = 2.34, 30" = 2.36, 30.25" = 2.38, 30.5" = 2.40, 30.75" = 2.42, 31" = 2.44, 31.25" = 2.46, 31.5" = 2.48, 31.75" = 2.50, 32" = 2.52, 32.25" = 2.54, 32.5" = 2.56, 32.75" = 2.58, 33" = 2.60, 33.25" = 2.62, 33.5" = 2.64, 33.75" = 2.66, 34" = 2.68, 34.25" = 2.70, 34.5" = 2.72, 34.75" = 2.74, 35" = 2.76, 35.25" = 2.78, 35.5" = 2.80, 35.75" = 2.82, 36" = 2.84, 36.25" = 2.86, 36.5" = 2.88, 36.75" = 2.90, 37" = 2.92, 37.25" = 2.94, 37.5" = 2.96, 37.75" = 2.98, 38" = 3.00, 38.25" = 3.02, 38.5" = 3.04, 38.75" = 3.06, 39" = 3.08, 39.25" = 3.10, 39.5" = 3.12, 39.75" = 3.14, 40" = 3.16, 40.25" = 3.18, 40.5" = 3.20, 40.75" = 3.22, 41" = 3.24, 41.25" = 3.26, 41.5" = 3.28, 41.75" = 3.30, 42" = 3.32, 42.25" = 3.34, 42.5" = 3.36, 42.75" = 3.38, 43" = 3.40, 43.25" = 3.42, 43.5" = 3.44, 43.75" = 3.46, 44" = 3.48, 44.25" = 3.50, 44.5" = 3.52, 44.75" = 3.54, 45" = 3.56, 45.25" = 3.58, 45.5" = 3.60, 45.75" = 3.62, 46" = 3.64, 46.25" = 3.66, 46.5" = 3.68, 46.75" = 3.70, 47" = 3.72, 47.25" = 3.74, 47.5" = 3.76, 47.75" = 3.78, 48" = 3.80, 48.25" = 3.82, 48.5" = 3.84, 48.75" = 3.86, 49" = 3.88, 49.25" = 3.90, 49.5" = 3.92, 49.75" = 3.94, 50" = 3.96, 50.25" = 3.98, 50.5" = 4.00, 50.75" = 4.02, 51" = 4.04, 51.25" = 4.06, 51.5" = 4.08, 51.75" = 4.10, 52" = 4.12, 52.25" = 4.14, 52.5" = 4.16, 52.75" = 4.18, 53" = 4.20, 53.25" = 4.22, 53.5" = 4.24, 53.75" = 4.26, 54" = 4.28, 54.25" = 4.30, 54.5" = 4.32, 54.75" = 4.34, 55" = 4.36, 55.25" = 4.38, 55.5" = 4.40, 55.75" = 4.42, 56" = 4.44, 56.25" = 4.46, 56.5" = 4.48, 56.75" = 4.50, 57" = 4.52, 57.25" = 4.54, 57.5" = 4.56, 57.75" = 4.58, 58" = 4.60, 58.25" = 4.62, 58.5" = 4.64, 58.75" = 4.66, 59" = 4.68, 59.25" = 4.70, 59.5" = 4.72, 59.75" = 4.74, 60" = 4.76, 60.25" = 4.78, 60.5" = 4.80, 60.75" = 4.82, 61" = 4.84, 61.25" = 4.86, 61.5" = 4.88, 61.75" = 4.90, 62" = 4.92, 62.25" = 4.94, 62.5" = 4.96, 62.75" = 4.98, 63" = 5.00, 63.25" = 5.02, 63.5" = 5.04, 63.75" = 5.06, 64" = 5.08, 64.25" = 5.10, 64.5" = 5.12, 64.75" = 5.14, 65" = 5.16, 65.25" = 5.18, 65.5" = 5.20, 65.75" = 5.22, 66" = 5.24, 66.25" = 5.26, 66.5" = 5.28, 66.75" = 5.30, 67" = 5.32, 67.25" = 5.34, 67.5" = 5.36, 67.75" = 5.38, 68" = 5.40, 68.25" = 5.42, 68.5" = 5.44, 68.75" = 5.46, 69" = 5.48, 69.25" = 5.50, 69.5" = 5.52, 69.75" = 5.54, 70" = 5.56, 70.25" = 5.58, 70.5" = 5.60, 70.75" = 5.62, 71" = 5.64, 71.25" = 5.66, 71.5" = 5.68, 71.75" = 5.70, 72" = 5.72, 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= 7.16, 90.25" = 7.18, 90.5" = 7.20, 90.75" = 7.22, 91" = 7.24, 91.25" = 7.26, 91.5" = 7.28, 91.75" = 7.30, 92" = 7.32, 92.25" = 7.34, 92.5" = 7.36, 92.75" = 7.38, 93" = 7.40, 93.25" = 7.42, 93.5" = 7.44, 93.75" = 7.46, 94" = 7.48, 94.25" = 7.50, 94.5" = 7.52, 94.75" = 7.54, 95" = 7.56, 95.25" = 7.58, 95.5" = 7.60, 95.75" = 7.62, 96" = 7.64, 96.25" = 7.66, 96.5" = 7.68, 96.75" = 7.70, 97" = 7.72, 97.25" = 7.74, 97.5" = 7.76, 97.75" = 7.78, 98" = 7.80, 98.25" = 7.82, 98.5" = 7.84, 98.75" = 7.86, 99" = 7.88, 99.25" = 7.90, 99.5" = 7.92, 99.75" = 7.94, 100" = 7.96, 100.25" = 7.98, 100.5" = 8.00, 100.75" = 8.02, 101" = 8.04, 101.25" = 8.06, 101.5" = 8.08, 101.75" = 8.10, 102" = 8.12, 102.25" = 8.14, 102.5" = 8.16, 102.75" = 8.18, 103" = 8.20, 103.25" = 8.22, 103.5" = 8.24, 103.75" = 8.26, 104" = 8.28, 104.25" = 8.30, 104.5" = 8.32, 104.75" = 8.34, 105" = 8.36, 105.25" = 8.38, 105.5" = 8.40, 105.75" = 8.42, 106" = 8.44, 106.25" = 8.46, 106.5" = 8.48, 106.75" = 8.50, 107" = 8.52, 107.25" = 8.54, 107.5" = 8.56, 107.75" = 8.58, 108" = 8.60, 108.25" = 8.62, 108.5" = 8.64, 108.75" = 8.66, 109" = 8.68, 109.25" = 8.70, 109.5" = 8.72, 109.75" = 8.74, 110" = 8.76, 110.25" = 8.78, 110.5" = 8.80, 110.75" = 8.82, 111" = 8.84, 111.25" = 8.86, 111.5" = 8.88, 111.75" = 8.90, 112" = 8.92, 112.25" = 8.94, 112.5" = 8.96, 112.75" = 8.98, 113" = 9.00, 113.25" = 9.02, 113.5" = 9.04, 113.75" = 9.06, 114" = 9.08, 114.25" = 9.10, 114.5" = 9.12, 114.75" = 9.14, 115" = 9.16, 115.25" = 9.18, 115.5" = 9.20, 115.75" = 9.22, 116" = 9.24, 116.25" = 9.26, 116.5" = 9.28, 116.75" = 9.30, 117" = 9.32, 117.25" = 9.34, 117.5" = 9.36, 117.75" = 9.38, 118" = 9.40, 118.25" = 9.42, 118.5" = 9.44, 118.75" = 9.46, 119" = 9.48, 119.25" = 9.50, 119.5" = 9.52, 119.75" = 9.54, 120" = 9.56, 120.25" = 9.58, 120.5" = 9.60, 120.75" = 9.62, 121" = 9.64, 121.25" = 9.66, 121.5" = 9.68, 121.75" = 9.70, 122" = 9.72, 122.25" = 9.74, 122.5" = 9.76, 122.75" = 9.78, 123" = 9.80, 123.25" = 9.82, 123.5" = 9.84, 123.75" = 9.86, 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# MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



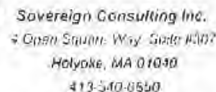
# MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]



### Low Flow Sampling

[illegible]

\* EPA stabilization parameters from EPA/540/S-95/504 April 1996

SAMPLING DATA			
SAMPLED BY (PRINT) / AFFILIATION <i>Truckee Charlie</i>	SAMPLER(S) SIGNATURES <i>[Signature]</i>	SAMPLING INITIATED AT <i>0725</i>	SAMPLING ENDED AT <i>0800</i>
PUMP OR TUBING DEPTH (IN WELL) (feet) <i>74</i>	SAMPLE PUMP FLOW RATE (ml. per minute) <i>250</i>	FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL NO.	
FIELD DECONTAMINATION <input checked="" type="radio"/> Y <input type="radio"/> N	FIELD FILTERED <input checked="" type="radio"/> Y <input type="radio"/> N	FILTER SIZE <i>0.45</i> $\mu$ m	
Filtration Equipment Type: <i>[Signature]</i>			

\* MATERIAL CODES: AG = Amber Glass, CG = Clear Glass, PE = Polyethylene, PP = Polypropylene, S = Silicone, T = Teflon, O = Other (Specify)

**WELL CONDITION CHECKLIST:** (circle appropriate item(s); cross out if not applicable)

Type: Flush Mount / Stand Pipe	General Condition: Good / Needs Repair	Well Caps: Good / Broken / None	Lock: Good / Broken / None
Evidence of Rain Water Between Steel & PVC? Y / N	Is Well Plumb? Y / N	PVC Riser: Good / Damaged / None	
Evidence of Ponding Around Well? Y / N	Concrete Collar: Good / Cracked / Leaking / None		

REMARKS:

## MONITORING WELL SAMPLING LOG

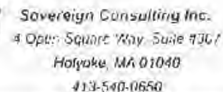
### Low Flow Sampling

[illegible]





### Low Flow Sampling

[illegible]

MONITORING WELL <sup>Development</sup> SAMPLING LOG

### Low Flow Sampling

[illegible]

MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

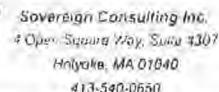


Well Development- No Samples Collected



## Development

### Low Flow Sampling



PROJECT NAME		PROJECT LOCATION		DATE		WELL ID					
AL001-002		Port Stevens NSW		8/24/2010		SHM-10-15					
PROJECT NUMBER		WELL DIAMETER (inches)		DEPTH TO WATER (feet)		DEPTH TO BOTTOM (feet)		PND READING (cc/mv)			
		2		27.82		58.80		-			
PURGING DATA											
TUBING DIAMETER (inches)		TUBING MATERIAL CODE (see below)		PURGE PUMP TYPE		PUMP EQUIPMENT MODEL & SERIAL #S					
1/2				Water							
WELL VOLUME PURGE: 1 WELL VOLUME= (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY						GALLONS		LITERS			
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88						5.1		-			
WELL SCREEN INTERVAL DEPTH (feet)		INITIAL PUMP OR TUBING DEPTH IN WELL (feet)		FINAL PUMP OR TUBING DEPTH IN WELL (feet)		PURGING INITIATED AT		PURGING ENDED AT			
45-55		54		54		1300		1435			
WATER LEVEL STABILIZATION				DEPTH TO WATER WITH PUMP (feet)							
TIME INTERVAL (min)		FLOW RATE (mL/min)		PUMP SETTINGS		DEPTH TO WATER (feet) START END		Water Level Stable (Yes or No)		VOLUME PURGED DURING INTERVAL (mL)	
</											

\* EPA stabilization parameters from EPA/540/S-95/504 April 1996

SAMPLING DATA				
SAMPLED BY (PRINT) / AFFILIATION <i>Jonathan Chiles</i>		SAMPLER(S) SIGNATURES <i>[Signature]</i>		SAMPLING INITIATED AT —
PUMP OR TUBING DEPTH IN WELL (feet) —		SAMPLE PUMP FLOW RATE (ml. per minute) —	FIELD METER MONITORING EQUIPMENT MODEL & SERIAL #s. —	
FIELD DECONTAMINATION: <input checked="" type="radio"/> Y <input type="radio"/> N		FIELD FILTERED: <input type="radio"/> Y <input type="radio"/> N	FILTER SIZE: — µm <i>NA</i>	DUPLICATE: <input type="radio"/> Y <input type="radio"/> N <i>NA</i>
MATERIAL CODES: AG = Amber Glass; CG = Clear Glass; PE = Polystyrene; PP = Polypropylene; S = Silicons; T = Teflon; O = Other (Specify)				

**WELL CONDITION CHECKLIST** (circle appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe      General Condition: Good / Needs Repair      Well Caps: Good / Broken / None      Lock: Good / Broken / None  
Evidence of Rain Water Between Steel & PVC? Y / N      Is Well Plumb?: Y / N      PVC Riser: Good / Damaged / None  
Evidence of Ponding Around Well? Y / N      Concrete Collar: Good / Cracked / Leaking / None

## REMARKS:

MARKS: \_\_\_\_\_

Drilling completed following three successive stable readings of pH, Temperature, and specific conductivity. Turbidity readings of less than 50 NTU unable to be reached. Well Development - No Samples collected

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

Well Development - No Samples Collected



MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

\*A stabilization parameters from EPA/540/S-95/504 April 1996

SAMPLING DATA	
SAMPLED BY (PRINT) / AFFILIATION: E. J. Foley / San. Com.	SAMPLER(S) SIGNATURE(S): E. J. Foley
SAMPLING INITIATED AT: 1120	SAMPLING ENDED AT: 1230
PUMP OR TUBING DEPTH IN WELL (feet): 570' / 57'	SAMPLE PUMP FLOW RATE (mL per minute): 150
FIELD (PANAUL 111) MONITORING EQUIPMENT MODEL & SERIAL #: YSL530 mps # 10F10C02	
FIELD DECONTAMINATION: <input checked="" type="checkbox"/> N	FIELD FILTERED: <input checked="" type="checkbox"/> N Filtration Equipment Type: _____
DUPLICATE: Y <input checked="" type="checkbox"/> N <input checked="" type="checkbox"/> (N)	
MATERIAL CODES: AG = Amber Glass; CG = Clear Glass; PE = Polyethylene; PP = Polypropylene; S = Seals; T = Teflon; O = Other (Specify)	
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)	
Type: Flush Mount / Stand Pipe	General Condition: Good / Needs Repair
Well Caps: Good / Broken / None	Lock: Good / Broken / None
Sealance of Rain Water Between Steel & PVC? Y / N	Is Well Plumb? Y / N
PVC Riser: Good / Damaged / None	
Sealance of Ponding Around Well? Y / N	Concrete Collar: Good / Cracked / Leaking / None
REMARKS: Lamotte 2020 Turb. SN - MF12915	

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



PROJECT NAME		PROJECT LOCATION		DATE		WELL ID				
Fort Owens S/H		Ayer, MA		6/30/10		24M-10-12				
JECT NUMBER		WELL DIAMETER (inches)		DEPTH TO WATER (feet)		DEPTH TO BOTTOM (feet)				
AC001		2		34.05		57.24				
PURGING DATA										
TUBING DIAMETER (inches)		TUBING MATERIAL CODE (see below)		PURGE PUMP TYPE		PUMP EQUIPMENT MODEL & SERIAL No.				
1/4		PE		Bladder		Cont-1209 Pump-11421				
WELL VOLUME PURGE: 1 WELL VOLUME= (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) x WELL CAPACITY						GALLONS				
						36				
WELL CAPACITY (Gallons Per Foot) 0.75 = 0.02, 1" = 0.04, 1.25" = 0.06, 2" = 0.10, 3" = 0.37, 4" = 0.65, 5" = 1.02, 6" = 1.47, 12" = 5.68						1 GALLON = 3.785 LITERS				
WELL SCREEN INTERVAL DEPTH (feet)						TOTAL VOLUME PURGED:				
47-52						136				
INITIAL PUMP OR TUBING DEPTH IN WELL (feet)		FINAL PUMP OR TUBING DEPTH IN WELL (feet)		PURGING INITIATED AT:		PURGING ENDED AT:				
52		52		1342		1453				
WATER LEVEL STABILIZATION				DEPTH TO WATER WITH PUMP (feet)						
TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS				DEPTH TO WATER (feet) START END				
0-10	150	D-105 R-10 PSI/C-40 PSI/T-170				34.05 34.05				
10-20	150					34.05 34.05				
TIME	FLOW RATE (mL/min)	DEPTH TO WATER (feet)	TURBIDITY (NTU)	DISSOLVED OXYGEN (mg/L)	pH	TEMP (°C)	SPECIFIC CONDUCTIVITY (µS/cm)	ORP (mV)	COLOR (describe)	ODOR (describe)
(3-5 minutes)	(100-500 mL/min)	(+/- 0.5')	(+/- 10%)	(+/- 10%)	(+/- 0.1)	(+/- 30)	(+/- 300)	(+/- 10mV)		
1405	150	34.05	62.7	0.39	5.97	14.64	472	-27.3	clear	None
1408	150	34.05	54.5	0.50	5.94	14.80	469	-27.9	clear	None
1411	150	34.05	53.4	1.42	5.95	14.69	469	-28.6	clear	None
1414	150	34.05	52.0	0.57	5.99	14.99	465	-33.2	clear	None
1417	150	34.05	51.4	0.57	5.98	14.97	465	-34.6	clear	None
1423	150	34.05	31.0	0.49	5.98	14.16	461	-32.6	clear	None
1426	150	34.05	26.4	0.38	5.99	14.25	460	-33.8	clear	None
1429	150	34.05	24.2	0.40	5.99	14.44	459	-33.2	clear	None
1435	150	34.05	17.10	4.08	6.01	14.15	460	-34.4	clear	None
1438	150	34.05	14.3	3.81	6.02	14.23	460	-34.1	clear	None
1441	150	34.05	11.3	3.71	5.98	14.52	460	-29.7	clear	None
1444	150	34.05	9.13	3.68	6.04	14.33	460	-35.5	clear	None
1447	150	34.05	8.02	3.51	6.03	14.48	460	-35.3	clear	None
1450	150	34.05	8.77	3.51	6.03	14.55	460	-35.0	clear	None
1453	150	34.05	8.43	3.55	6.04	14.41	460	-34.9	clear	None

<sup>a</sup>A stabilization parameters from EPA/540/S-95/004 April 1996

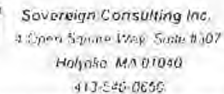
SAMPLING DATA			
SAMPLED BY (PRINT) / AFFILIATION Cassidy Harold	SAMPLER(S) SIGNATURES <i>[Signature]</i>	SAMPLING INITIATED AT 1500	SAMPLING ENDED AT 1555
PUMP OR TAPPING DEPTH IN WELL (feet) 52	SAMPLER PUMP FLOW RATE (in. per minute) 150	PUMP OR TAPPING MONITORING EQUIPMENT MODEL & SERIAL NO. YS1556 mps #10 FloCo2	
FIELD DECONTAMINATION <input checked="" type="radio"/> Y <input type="radio"/> N	FIELD FILTERED <input checked="" type="radio"/> Y <input type="radio"/> N Filtration Equipment Type	FILTER SIZE _____ $\mu$ m	DUPLICATE <input checked="" type="radio"/> Y <input type="radio"/> N
MATERIAL CODES    AG = Amber Glass    CG = Clear Glass    PE = Polyethylene    PP = Polypropylene    S = Silicate    T = Teflon    O = Other (Specify)			
<b>WELL CONDITION CHECKLIST</b> (circle appropriate item(s), cross out if not applicable)			
Type: Flush Mount / Stand Pipe	General Condition: <input checked="" type="radio"/> Good / <input type="radio"/> Needs Repair	Well Caps: <input checked="" type="radio"/> Good / <input type="radio"/> Broken / None	Lock: <input checked="" type="radio"/> Good / <input type="radio"/> Broken / <input type="radio"/> None
Presence of Rain Water Between Steel & PVC? <input checked="" type="radio"/> Y <input type="radio"/> N	Is Well Plumb? <input checked="" type="radio"/> Y <input type="radio"/> N	PVC Riser: <input checked="" type="radio"/> Good / <input type="radio"/> Damaged / None	
Presence of Ponding Around Well? <input checked="" type="radio"/> Y <input type="radio"/> N	Concrete Collar: <input checked="" type="radio"/> Good / <input type="radio"/> Cracked / <input type="radio"/> Leaking / <input type="radio"/> None		
REMARKS: Lamotte 2020 Turb # 3 SN-ME2915			





## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



<sup>a</sup>A stabilization parameters from EPA/540/S-95/504 April 1996

### SAMPLING DATA

SAMPLED BY (PRINT) / AFFILIATION Eric Foley		SAMPLER(S) SIGNATURES Eric Foley		SAMPLING INITIATED AT 11:15		SAMPLING PRICED AT 11:50	
PUMP OR TUBING DEPTH IN WELL (feet) Coloast		SAMPLE PUMP FLOW RATE (mL per min (mL/min)) 200 mL/min		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s 15138 mps 07500085 + 1 OF 10 CO2		micro Purge Controller SN# 1209	
FIELD DECONTAMINATION <input checked="" type="checkbox"/> N		FIELD FILTERED <input checked="" type="checkbox"/> N Filtration Equipment Type:		FILTER SIZE _____ µm		DUPLICATE Y <input checked="" type="checkbox"/> N	

## WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)

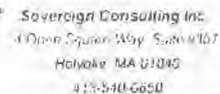
Type: Flush Mount / Stand Pipe General Condition: Good / Needs Repair Well Caps: Good / Broken / None Lock: Good / Broken / None  
 Presence of Rain Water Between Steel & PVC? Y / N Is Well Plumb? Y / N PVC Riser: Good / Damaged / None  
 Presence of Ponding Around Well? Y / N Concrete Collar: Good / Cracked / Leaking / None

REMARKS

ms/mst on well (Turbidity meter - LaMotte 2020e SN-ME12915)



### Low Flow Sampling

1400

\*A stabilization parameters from FPA/540/S-95/504 April 1996

SAMPLING DATA			
SAMPLED BY (PRINT) / AFFILIATION: Carolyn Hasolt		SAMPLER(S) SIGNATURES: Carolyn Hasolt	
SAMPLING INITIATED AT: 1455		SAMPLING ENDED AT: 1545	
PURCH OR TUBING DEPTH IN WELL (feet): 52		SAMPLE PUMP / FLOW RATE (ml per minute): 150	
FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL NO. YS1556 09500085 / 10F1002 Lamotte 2nd E ME12915			
FIELD DECONTAMINATION (Y) N		FIELD FILTERED (Y) N FILTER SIZE 0.1µm	
Filtration Equipment Type:		DUPLICATE (Y) N	
MATERIAL CODES AG = Amber Glass, CG = Clear Glass, PE = Polyethylene, PP = Polypropylene, S = Silica, T = Teflon, O = Other (Specify)			
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)			
Type: Flush Mount / Stand Pipe General Condition: Good / Needs Repair Well Caps: Good / Broken / None Lock: Good / Broken / None			
evidence of Rain Water Between Steel & PVC? Y / N Is Well Plumb? Y / N PVC Riser: Good / Damaged / None			
evidence of Ponding Around Well? Y / N Concrete Collar: Good / Cracked / Leaking / None			
REMARKS: DUP-090110-F/u			

0

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



PROJECT NAME		PROJECT LOCATION		DATE		WELL ID	
Accel-002		Devon, mrt		9/2/10		SHM-10-14	
JECT NUMBER		WELL DIAMETER (inches)		DEPTH TO WATER (feet)		DEPTH TO BOTTOM (feet)	
		2"		20.87		62.35	
PUMP HEADING (gpm)							
62.35							
TUBING DIAMETER (inches)		TUBING MATERIAL CODE (see below)		PURGE PUMP TYPE		PUMP EQUIPMENT MODEL & SERIAL #s	
		PE		Bladder		Cat 1209 Pump 11421 QED	
WELL VOLUME PURGE: 1 WELL VOLUME= (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY						GALLONS	
						LITERS	
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1' = 0.04; 1.25' = 0.06; 2' = 0.16; 3' = 0.32; 4' = 0.65; 5' = 1.02; 6' = 1.47; 12' = 5.88						1 GALLON = 3.785 LITERS	
WELL SCREEN INTERVAL DEPTH (feet)						TOTAL VOLUME PURGED:	
62-62						GALLONS:	
INITIAL PUMP OR TUBING DEPTH IN WELL (feet): 72						LITERS:	
FINAL PUMP OR TUBING DEPTH IN WELL (feet): 72							
PURGING INITIATED AT: 957							
PURGING ENDED AT:							
WATER LEVEL STABILIZATION				DEPTH TO WATER WITH PUMP (feet)			
				20.87			
TIME INTERVAL (min)		FLOW RATE (mL/min)		PUMP SETTINGS		DEPTH TO WATER (feet) START END	
0-20		NA		Adjusting pump & water level			
20-30		22.5		D-10, P-20, TPSI-150, CPSI-50		20.87 20.87	
						Yes	
TIME		FLOW RATE (mL/min)		DEPTH TO WATER (feet)		TURBIDITY (NTU)	
(3-5 minutes)		(100-500 mL/min)		(ft. 0.3')		(ft. 10%)	
1030	22.5	20.87	18.6	0.36	5.14	14.65	1069
1035	22.5	20.87	21.7	0.27	5.56	14.44	1066
1040	22.5	20.87	22.1	0.28	5.86	14.51	1066
1045	22.5	20.87	26.9	0.23	6.04	14.45	1065
1050	22.5	20.87	29.5	0.19	6.18	14.27	1069
1055	22.5	20.87	22.7	0.15	6.25	14.35	1070
1100	22.5	20.87	20.7	0.20	6.29	14.37	1071
1105	22.5	20.87	16.8	0.20	6.28	14.50	1063
1110	22.5	20.87	11.3	0.19	6.30	14.56	1045
1115	22.5	20.87	72.4	0.20	6.31	14.40	1046
1120	22.5	20.87	59.5	0.18	6.33	14.39	1047
1125	22.5	20.87	55.5	0.17	6.35	14.42	1049
1130	22.5	20.87	43.3	0.17	6.35	14.44	1049
1135	22.5	20.87	34.4	0.18	6.35	14.46	1045
1140	22.5	20.87	35.9	0.18	6.34	14.56	1044
1145	22.5	20.87	34.7	0.18	6.35	14.48	1045

<sup>a</sup>A stabilization parameters from EPA/540/S-95/504 April 1995

SAMPLING DATA	
SAMPLED BY (PRINT) / AFFILIATION <b>Caryn Hardy</b>	SAMPLER(S) SIGNATURES  
SAMPLING INITIATED AT <b>1147</b>	SAMPLING ENDED AT <b>1223</b>
PUMP CIL (LUGS) / DEPTH WELL (feet) <b>72'</b>	SAMPLE TYPE / FLOW RATE (gal. per minute) <b>235</b>
FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL NO.  	
FIELD DECONTAMINATION <input checked="" type="radio"/> N	FIELD FILTERED <input checked="" type="radio"/> N FILTER SIZE _____ µm Filtration Equipment Type _____
DUPLICATE <input checked="" type="radio"/> Y <input checked="" type="radio"/> N	
MATERIAL CODES AG = Amber Glass CG = Clear Glass PE = Polyethylene PP = Polypropylene S = Silicone T = Teflon O = Other (Specify) _____	
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)	
Type: Flush Mount / Stand Pipe General Condition: <input checked="" type="radio"/> Good / Needs Repair Well Caps: <input checked="" type="radio"/> Good / Broken / None Lock: Good / Broken / <input checked="" type="radio"/> None	
Evidence of Rain Water Between Steel & PVC? Y / <input checked="" type="radio"/> N Is Well Plumb? Y / <input checked="" type="radio"/> N PVC Riser: <input checked="" type="radio"/> Good / Damaged / None	
Evidence of Ponding Around Well? Y / <input checked="" type="radio"/> N Concrete Collar: <input checked="" type="radio"/> Good / Cracked / Leaking / None	
REMARKS:  <b>msmsd from well</b>	



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

<sup>a</sup>A stabilization parameters from EPA/540/S-95/504 April 1996

SAMPLING DATA			
SAMPLED BY (PRINT) / AFFILIATION: Erin Foley		SAMPLER(S) SIGNATURES: Erin Foley	
PUMP OR TUBING DEPTH IN WELL (feet): 82'		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL NO.:	
SAMPLE PUMP FLOW RATE (liters per minute): 295		SAMPLING INITIATED AT: 1445	
SAMPLING ENDED AT: 1515			
FIELD DECONTAMINATION: <input checked="" type="checkbox"/> Y <input type="checkbox"/> N		Filtration Equipment Type: <input checked="" type="checkbox"/> N	
Filtration Equipment Type: <input type="checkbox"/> Y		FILTER SIZE: _____ $\mu$ m	
MATERIAL CODES: AG = Amber Glass, CG = Clear Glass, PC = Polyethylene, PP = Polypropylene, S = Silicone, T = Teflon, Q = Other (Specify):			
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)			
Type: Flush Mount / Stand Pipe		General Condition: <input checked="" type="checkbox"/> Good / <input type="checkbox"/> Needs Repair	
Incidence of Rain Water Between Steel & PVC? Y / <input checked="" type="checkbox"/> N		Well Caps: Good / Broken / <input checked="" type="checkbox"/> None	
Is Well Plumb? Y / <input checked="" type="checkbox"/> N		Lock: <input checked="" type="checkbox"/> Good / Broken / <input type="checkbox"/> None	
Incidence of Ponding Around Well? Y / <input checked="" type="checkbox"/> N		PVC Riser: <input checked="" type="checkbox"/> Good / Damaged / <input type="checkbox"/> None	
Concrete Collar: <input checked="" type="checkbox"/> Good / Cracked / Leaking / <input type="checkbox"/> None			
REMARKS:			



Sovereign Consulting Inc.  
995B South Main Street, Suite 202  
Marshall, MA 02048  
508-339-3200

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
4 Open Square Way, Suite #302  
Holyoke, MA 01040  
413-540-0650

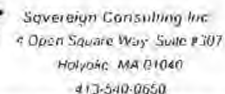
PROJECT NAME <b>Devens ALE</b>		PROJECT LOCATION		DATE <b>9/7/10</b>	WELL ID <b>SM-10-04</b>					
PROJECT NUMBER <b>AL001</b>		WELL DIAMETER (inches) <b>1.25</b>	DEPTH TO WATER (feet) <b>7.10</b>	DEPTH TO BOTTOM (feet) <b>65'</b>	PID READING (ppmv) <b>-</b>					
PURGING DATA										
TUBING DIAMETER (inches) <b>3/4"</b>	TUBING MATERIAL CODE (see below) <b>PE</b>	PURGE PUMP TYPE <b>PERISTALTIC</b>	PUMP EQUIPMENT MODEL & SERIAL #s <b>GEOPUMP</b>							
WELL VOLUME PURGE: 1 WELL VOLUME = (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY			GALLONS <b>3.5</b>	LITERS						
WELL CAPACITY (Gallons Per Foot) 0.75 = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.89			1 GALLON = 3.785 LITERS		TOTAL VOLUME PURGED <b>6.5</b>					
WELL SCREEN INTERVAL DEPTH (feet) <b>55'-65'</b>	INITIAL PUMP OR TUBING DEPTH (feet) <b>60'</b>	FINAL PUMP OR TUBING DEPTH (feet) <b>60'</b>	PURGING INITIATED AT <b>1340</b>	PURGING ENDED AT <b>1426</b>	LITERS					
WATER LEVEL STABILIZATION		DEPTH TO WATER WITH PUMP (feet)								
TIME INTERVAL (min) <b>15 min</b>	FLOW RATE (mL/min) <b>320</b>	PUMP SETTINGS <b>250 Rpm</b>		DEPTH TO WATER (feet) START <b>7.10</b>	DEPTH TO WATER (feet) END <b>7.20</b>					
Water Level Stable (Feet No)		VOLUME PURGED DURING INTERVAL (mL) <b>7 Liters</b>								
TIME	FLOW RATE (mL/min)	DEPTH TO WATER (feet)	TURBIDITY (NTU)	DISSOLVED OXYGEN (mg/L)	pH	TEMP (°C)	SPECIFIC CONDUCTIVITY (µS/cm)	DRP (mv)	COLOR (describe)	ODOR (describe)
(3-5 minutes)	(100-500 mL/min)	(± 0.3')	(± 10%)	(± 10%)	(± 0.1)	(± 0.5)	(± 250)	(± 10mV)		
1400	320	7.20	14.4	0.60	5.96	13.42	704	23.4	Clear	None
1405	320	7.20	11.6	0.42	5.97	12.42	688	27.9	Clear	None
1408	320	7.20	4.96	0.43	5.99	12.00	671	24.3	Clear	None
1411	320	7.20	7.05	0.30	5.98	12.21	666	40.2	Clear	None
1414	320	7.20	4.53	0.24	6.01	12.07	666	42.4	Clear	None
1417	320	7.20	5.48	0.19	6.00	11.93	661	43.9	Clear	None
1420	320	7.20	3.96	0.21	6.00	12.08	658	43.4	Clear	None
1423	320	7.20	4.01	0.23	6.00	12.08	657	43.3	Clear	None
1426	320	7.20	4.28	0.23	5.99	12.10	656	43.7	Clear	None

\*A stabilization parameters from EPA/540/S-95/04 April 1996

SAMPLING DATA			
SAMPLED BY (PRINT) / AFFILIATION <b>Eric Foley</b>	SAMPLER(S) SIGNATURES <b>Eric Foley</b>	SAMPLING INITIATED AT <b>1430</b>	SAMPLING ENDED AT <b>1450</b>
PUMP OR TUBING DEPTH (feet) <b>60'</b>	SAMPLE PUMP FLOW RATE (mL per minute) <b>320</b>	FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s	
FIELD DECONTAMINATION: <input checked="" type="checkbox"/> N	FIELD-FILTERED: <input checked="" type="checkbox"/> N	FILTER SIZE <input type="text"/> µm	DUPLICATE <input checked="" type="checkbox"/> Y
MATERIAL CODES AG = Amber Glass CG = Clear Glass PE = Polyethylene PP = Polypropylene S = Silicone T = Teflon O = Other (Specify)			
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)			
Type: Flush Mount / Stand Pipe	General Condition: <input checked="" type="checkbox"/> Good / Needs Repair	Well Caps: <input checked="" type="checkbox"/> Good / Broken / None	Lock: <input checked="" type="checkbox"/> Good / Broken / None
Incidence of Rain Water Between Steel & PVC? <input checked="" type="checkbox"/> Y / <input checked="" type="checkbox"/> N	Is Well Plumb? <input checked="" type="checkbox"/> Y / <input checked="" type="checkbox"/> N	PVC Riser: <input checked="" type="checkbox"/> Good / Damaged / None	
Evidence of Ponding Around Well? <input checked="" type="checkbox"/> Y / <input checked="" type="checkbox"/> N	Concrete Collar: <input checked="" type="checkbox"/> Good / Cracked / Leaking / None		
REMARKS:			



### Low Flow Sampling



<sup>3</sup>A stabilization parameters from EPA/540/S-95/504 April 1995

SAMPLED BY (PRINT) / AFFILIATION: <b>Erin Foley</b>		SAMPLER(S) SIGNATURES: <b>Erin Foley</b>		SAMPLING INITIATED AT: <b>1045</b>		SAMPLING ENDED AT: <b>1138</b>	
PUMP OR TUBING DEPTH IN WELL (feet) <b>165'</b>		SAMPLE PUMP FLOW RATE (ml per minute) <b>125 mL/min</b>		WELL PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #			
FIELD DECONTAMINATION <input checked="" type="radio"/> Y <input type="radio"/> N		FIELD FILTERED <input checked="" type="radio"/> Y <input type="radio"/> N Filtration Equipment Type:		FILTER SIZE _____ µm		DUPLICATE <input checked="" type="radio"/> Y <input type="radio"/> N	

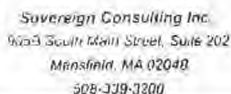
**WELL CONDITION CHECKLIST** (circle appropriate item(s), cross out if not applicable)

Type: Flush Mount / Stand Pipe      General Condition: Good / Needs Repair      Well Caps: Good / Broken / None      Lock: Good / Broken / None  
Incidence of Rain Water Between Steel & PVC? Y / N      Is Well Plumb? Y / N      PVC Riser: Good / Damaged / None  
Incidence of Ponding Around Well? Y / N      Concrete Collar: Good / Cracked / Leaking / None

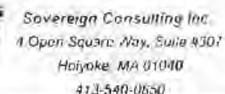
REMARKS:

DUP-090710-FIU





### Low Flow Sampling

[illegible]



Sovereign Consulting Inc.  
9050 South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

# MONITORING WELL SAMPLING LOG

Low Flow Sampling



Sovereign Consulting Inc.  
10901 Squash Pkwy, Suite E307  
Holyoke, MA 01040  
413-540-1850

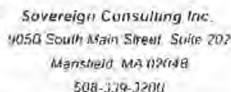
PROJECT NAME <b>AC001.002</b>		PROJECT LOCATION <b>Dexens</b>		DATE <b>9/7/10</b>		WELL ID: <b>SHM-10-09</b>				
PROJECT NUMBER		WELL DIAMETER (inches) <b>1.5</b>	DEPTH TO WATER (feet) <b>9.53</b>	DEPTH TO BOTTOM (feet) <b>57.51</b>	P.D. READING (ppmv)					
PURGING DATA										
TUBING DIAMETER (inches) <b>3/4"</b>	TUBING MATERIAL CODE (see below) <b>Poly PE</b>	PURGE PUMP TYPE <b>Perit</b>		PUMP EQUIPMENT MODEL & SERIAL #s						
WELL VOLUME PURGE: 1 WELL VOLUME (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY				GALLONS	LITERS					
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.37; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88				1 GALLON = 3.785 LITERS		TOTAL VOLUME PURGED				
WELL SCREEN INTERVAL DEPTH (feet): <b>47'-57'</b>	INITIAL PUMP OR TUBING DEPTH IN WELL (feet): <b>52'51"</b>	FINAL PUMP OR TUBING DEPTH IN WELL (feet): <b>52'51"</b>	PURGING INITIATED AT: <b>9:47</b>	PURGING ENDED AT: <b>11:52</b>	GALLONS: <b>41</b>					
WATER LEVEL STABILIZATION		DEPTH TO WATER WITH PUMP: (feet) <b>9.55</b>								
TIME INTERVAL (min)	FLOW RATE (mL/min)	PUMP SETTINGS		DEPTH TO WATER (feet) START	DEPTH TO WATER (feet) END	Water Level Stable (Yes or No)	VOLUME PURGED DURING INTERVAL (mL)			
<b>0-10</b>							<b>6 L</b>			
<b>10-20</b>	<b>375</b>	<b>0-350 RPM, Speed Control 50%</b>		<b>9.55</b>	<b>9.55</b>	<b>Y</b>	<b>5 L</b>			
TIME	FLOW RATE (mL/min)	DEPTH TO WATER (feet)	TURBIDITY (NTU)	DISSOLVED OXYGEN (mg/L)	pH	TEMP (°C)	SPECIFIC CONDUCTIVITY (µS/cm)	ORP (mV)	COLOR (describe)	ODOR (describe)
(3-5 minutes)	(100-500 mL/min)	(± 0.01)	(± 10%)	(± 10%)	(± 0.1)	(± 0.5)	(± 200)	(± 10mV)		
<b>10:14</b>	<b>375</b>	<b>9.55</b>	<b>12.4</b>	<b>4.48</b>	<b>6.19</b>	<b>12.92</b>	<b>1075</b>	<b>-120.1</b>	<b>clear</b>	<b>none</b>
<b>10:19</b>	<b>375</b>	<b>9.55</b>	<b>3989</b>	<b>3.16</b>	<b>6.11</b>	<b>11.52</b>	<b>10107</b>	<b>-144.2</b>	<b>cloudy</b>	<b>none</b>
<b>10:24</b>	<b>375</b>	<b>9.55</b>	<b>171</b>	<b>2.26</b>	<b>6.12</b>	<b>11.64</b>	<b>1065</b>	<b>-174.6</b>	<b>cloudy</b>	<b>none</b>
<b>10:29</b>	<b>375</b>	<b>9.55</b>	<b>31.9</b>	<b>2.81</b>	<b>6.11</b>	<b>11.49</b>	<b>1066</b>	<b>-173.7</b>	<b>clear</b>	<b>none</b>
<b>Pump Turned off to clean slow moving cell</b>										
<b>10:40</b>										
<b>10:55</b>	<b>375</b>	<b>9.55</b>	<b>3.60</b>	<b>2.98</b>	<b>6.15</b>	<b>12.01</b>	<b>1078</b>	<b>-259.6</b>	<b>clear</b>	<b>none</b>
<b>11:05</b>	<b>375</b>	<b>9.55</b>	<b>2.38</b>	<b>4.74</b>	<b>6.14</b>	<b>11.88</b>	<b>1078</b>	<b>-290.8</b>	<b>clear</b>	<b>none</b>
<b>11:05</b>	<b>375</b>	<b>9.55</b>	<b>1.29</b>	<b>4.49</b>	<b>6.16</b>	<b>11.88</b>	<b>1078</b>	<b>-250.4</b>	<b>clear</b>	<b>none</b>
<b>11:10</b>	<b>375</b>	<b>9.55</b>	<b>0.64</b>	<b>4.12</b>	<b>6.16</b>	<b>11.91</b>	<b>1079</b>	<b>-140.9</b>	<b>clear</b>	<b>none</b>
<b>11:15</b>	<b>375</b>	<b>9.55</b>	<b>0.26</b>	<b>5.13</b>	<b>6.18</b>	<b>12.13</b>	<b>1079</b>	<b>-171.7</b>	<b>clear</b>	<b>none</b>
<b>11:20</b>	<b>375</b>	<b>9.55</b>	<b>2.44</b>	<b>6.35</b>	<b>6.17</b>	<b>12.16</b>	<b>1078</b>	<b>-189.5</b>	<b>clear</b>	<b>none</b>
<b>11:25</b>	<b>375</b>	<b>9.55</b>	<b>1.66</b>	<b>2.57</b>	<b>6.14</b>	<b>12.13</b>	<b>1081</b>	<b>-127.6</b>	<b>clear</b>	<b>none</b>
<b>11:30</b>	<b>375</b>	<b>9.55</b>	<b>0.84</b>	<b>1.66</b>	<b>6.14</b>	<b>12.04</b>	<b>1080</b>	<b>-123.9</b>	<b>clear</b>	<b>none</b>
<b>11:35</b>	<b>375</b>	<b>9.55</b>	<b>1.45</b>	<b>0.92</b>	<b>6.19</b>	<b>12.07</b>	<b>1079</b>	<b>-145.6</b>	<b>clear</b>	<b>none</b>
<b>11:40</b>	<b>375</b>	<b>9.55</b>	<b>1.32</b>	<b>8.53</b>	<b>6.22</b>	<b>12.05</b>	<b>1080</b>	<b>-205.8</b>	<b>clear</b>	<b>none</b>
<b>11:45</b>	<b>375</b>	<b>9.55</b>	<b>1.37</b>	<b>3.61</b>	<b>6.19</b>	<b>12.10</b>	<b>1079</b>	<b>-233.0</b>	<b>clear</b>	<b>none</b>
* EPA stabilization parameters from EPA/540/S-95/004 April 1995										
SAMPLING DATA										
SAMPLED BY (PRINT) / AFFILIATION: <b>SouCon Carolyn Hoxell</b>			SAMPLER(S) SIGNATURES: <b>CAH, JAR Carolyn Hoxell</b>			SAMPLING INITIATED AT: <b>11:53</b>		SAMPLING ENDED AT: <b>12:11</b>		
PUMP OR TUBING DEPTH IN WELL (feet) <b>51'</b>		SAMPLE PUMP FLOW RATE (mL per minute) <b>375</b>		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s						
FIELD DECONTAMINATION: <input checked="" type="checkbox"/> N			FIELD FILTERED: <input checked="" type="checkbox"/> N		FILTER SIZE: <u>          </u> µm		DUPLICATE: <input checked="" type="checkbox"/> N			
MATERIAL CODES: AG = Amber Glass; CO = Clear Glass; PE = Polyethylene; PP = Polypropylene; S = Silicone; T = Teflon; O = Other (Specify):										
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)										
Type: Flush Mount / Stand Pipe		General Condition: <input checked="" type="checkbox"/> Good / <input type="checkbox"/> Needs Repair		Well Caps: <input checked="" type="checkbox"/> Good / <input type="checkbox"/> Broken / <input type="checkbox"/> None		Lock: <input checked="" type="checkbox"/> Good / <input type="checkbox"/> Broken / <input type="checkbox"/> None				
Evidence of Rain Water Between Steel & PVC? <input checked="" type="checkbox"/> Y / <input type="checkbox"/> N		Is Well Plumb? <input checked="" type="checkbox"/> Y / <input type="checkbox"/> N		PVC Riser: <input checked="" type="checkbox"/> Good / <input type="checkbox"/> Damaged / <input type="checkbox"/> None						
Evidence of Ponding Around Well? <input checked="" type="checkbox"/> Y / <input type="checkbox"/> N		Concrete Collar: <input checked="" type="checkbox"/> Good / <input type="checkbox"/> Cracked / <input type="checkbox"/> Leaking / <input type="checkbox"/> None								
REMARKS:										



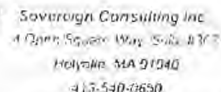
### Low Flow Sampling

[illegible]





### Low Flow Sampling



PROJECT NAME: **Ac001-002**

PROJECT LOCATION: **Ayer mrt**

DATE: **09-08-10**

WELL ID: **SHM-10-01**

WELL NUMBER: **Ac001-002**

WELL DIAMETER (inches): **4.5**

DEPTH TO WATER (feet): **4.78**

DEPTH TO BOTTOM (feet): **71.72**

PURGING DATA

TUBING DIAMETER (inches): **3/4**

TUBING MATERIAL CODE (see below): **PE**

PURGE PUMP TYPE: **Geopump**

PLUMP EQUIPMENT MODEL & SERIAL #:

WELL VOLUME PURGE: 1 WELL VOLUME= (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) \* WELL CAPACITY

GALLONS: **4.01**

LITERS:

WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02; 1" = 0.04; 1.25" = 0.06; 2" = 0.16; 3" = 0.32; 4" = 0.65; 5" = 1.02; 6" = 1.47; 12" = 5.88

1 GALLON = 3.785 LITERS

TOTAL VOLUME PURGED:

WELL SCREEN INTERVAL DEPTH (feet): **62-72'**

INITIAL PUMP OR TUBING DEPTH IN WELL (feet): **67'**

FINAL PUMP OR TUBING DEPTH IN WELL (feet): **67'**

PURGING INITIATED AT: **9:30**

PURGING ENDED AT: **1024**

GALLONS: **5**

LITERS:

WATER LEVEL STABILIZATION

DEPTH TO WATER WITH PUMP (feet):

TIME INTERVAL (min): **15min**

FLOW RATE (mL/min): **320**

PUMP SETTINGS: **~155 Rpm**

DEPTH TO WATER (feet) START: **4.81**

DEPTH TO WATER (feet) END: **4.81**

Water Level Stable (Yes or No): **Yes**

VOLUME PURGED DURING INTERVAL (mL):

TIME (3-5 minutes)	FLOW RATE (mL/min) (100-500 mL/min)	DEPTH TO WATER (feet) (-1.0 - 3.0)	TURBIDITY (NTU) (-1.0 - 10%)	DISSOLVED OXYGEN (mg/L) (-1.0 - 10%)	pH (-1.0 - 14.0)	TEMP (°C) (-1.0 - 35.0)	SPECIFIC CONDUCTIVITY (µS/cm) (10 - 1000)	ORP (mV) (-10 - 1000)	COLOR (resoluble)	ODOR (description)
955	320	4.81	0.50	0.50	6.41	13.17	298	28.4	clear	None
958	320	4.81	0.85	0.41	5.76	12.97	298	53.3	clear	None
1001	320	4.81	0.55	0.24	5.33	12.85	297	53.0	clear	None
1004	320	4.81	0.47	0.22	6.17	12.78	298	23.0	clear	None
1007	320	4.81	0.47	0.19	6.23	12.69	299	15.5	clear	None
1010	320	4.81	0.20	0.17	6.27	12.69	299	15.1	clear	None
1013	320	4.81	0.29	0.14	6.29	12.70	299	13.3	clear	None
1016	320	4.81	0.22	0.13	6.29	12.71	299	11.8	clear	None
1019	320	4.81	0.16	0.13	6.30	12.69	299	11.4	clear	None
1021	320	4.81	0.15	0.12	6.31	12.68	299	11.3	clear	None

SAMPLED BY (PRINT) / AFFILIATION: **Eric Foley**

SAMPLER(S) SIGNATURES: **Eric Foley**

SAMPLING INITIATED AT: **1030**

SAMPLING ENDED AT: **1105**

INITIAL OR TUBING DEPTH IN WELL (feet): **67'**

SAMPLE PUMP FLOW RATE (mL per minute): **320**

FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #:

FIELD DECONTAMINATION: **(N)**

FIELD FILTERED: **(Y)**

FILTER SIZE: **µm**

Filteration Equipment Type:

DUPLICATE: **(N)**

my/ms

MATERIAL CODES: AG = Amber Glass, CG = Clear Glass, PE = Polyethylene, PP = Polypropylene, S = Silicone, T = Teflon, O = Other (Specify)

WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)

Type: Flush Mount / **Stand Pipe**

General Condition: **Good** / Needs Repair

Well Caps: **Good** / Broken / None

Lock: Good / Broken / **None**

Incidence of Rain Water Between Steel & PVC? **Y** / **(N)**

Is Well Plumb?: **Y** / **(N)**

PVC Riser: **Good** / Damaged / None

Evidence of Ponding Around Well? **Y** / **(N)**

Concrete Collar: **Good** / Cracked / Leaking / None

REMARKS: **MS/MSD**

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

<sup>a</sup>A stabilization parameters from EPA/540/S-95/504, April 1996.

SAMPLED BY (PRINT) / AFFILIATION Erin Foley		SAMPLER(S) SIGNATURES Erin Foley		SAMPLING INITIATED AT 1230		SAMPLING ENDED AT 1330	
PUMP OR TAPPING DEPTH IN WELL (feet) 63'		SAMPLE PUMP FLOW RATE (gallons per minute) 300		PUMP PARAMETERS MONITORING EQUIPMENT MODEL & SERIAL NO. YS110F10C02 + 09J100085 Turb 26858			
FIELD DECONTAMINATION <input checked="" type="radio"/> Y <input type="radio"/> N		FIELD FILTERED <input checked="" type="radio"/> Y <input type="radio"/> N Filtration Equipment Type:		FILTER SIZE _____ µm		DUPLICATE <input type="radio"/> Y <input checked="" type="radio"/> N	
MATERIAL CODES: AG = Amber Glass CG = Clear Glass PE = Polyethylene PP = Polypropylene S = Silicone T = Teflon O = Other (Specify)							
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)							
Type: Flush Mount / Stand Pipe		General Condition: <input checked="" type="radio"/> Good / <input type="radio"/> Needs Repair		Well Caps: <input checked="" type="radio"/> Good / <input type="radio"/> Broken / <input type="radio"/> None		Lock: Good / Broken / <input checked="" type="radio"/> None	
Influence of Rain Water Between Steel & PVC? Y / <input checked="" type="radio"/> N		Is Well Plumb? Y / <input checked="" type="radio"/> N		PVC Riser: <input checked="" type="radio"/> Good / <input type="radio"/> Damaged / <input type="radio"/> None			
Influence of Ponding Around Well? <input checked="" type="radio"/> Y / <input type="radio"/> N		Concrete Collar: <input checked="" type="radio"/> Good / <input type="radio"/> Cracked / <input type="radio"/> Leaking / <input checked="" type="radio"/> None					
REMARKS:							





**Sovereign Consulting Inc.**  
105B South Main Street Suite 707  
Mansfield, MA 02048  
508-339-1200

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



Sovereign Consulting Inc.  
4 Cape Cod Square West, Suite 420  
Holyoke, MA 01040  
413-540-0650

[illegible]



**Sovereign Consulting Inc.**  
905B South Main Street, Suite 202  
Mansfield, MA 02048  
508-339-3200

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

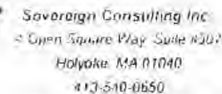


**Sovereign Consulting Inc.**  
4 Open Square Way, Suite 11307  
Holyoke, MA 01040  
417-540-0650

[illegible]



### Low Flow Sampling



<sup>a</sup>A stabilization parameters from EPA/600/S-95/504 April 1996

SAMPLED BY (PRINT) / AFFILIATION <b>Erin Foley</b>		SAMPLER(S) SIGNATURE(S) <b>Eeri J. [Signature]</b>		SAMPLING INITIATED AT <b>1100</b>		SAMPLING ENDED AT <b>1135</b>	
*PUMP (IF TITRIMETER) DEPTH IS WELL (feet) <b>45</b>		SAMPLE FLOW RATE (mL per minute) <b>210</b>		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL #s <b>YSI 015100085 + 10F10C02 Turb ME12915</b>			
FIELD DECONTAMINATION <input checked="" type="radio"/> Y <input type="radio"/> N		FIELD FILTERED <input checked="" type="radio"/> Y <input type="radio"/> N Filteration Equipment Type:			FILTER SIZE _____ $\mu$ m		
MATERIAL CODES AG = Analytical Glass; CG = Clear Glass; PE = Polyethylene; PP = Polypropylene; S = Silicone; T = Teflon; O = Other (Specify)		DUPLICATE <input type="radio"/> Y <input checked="" type="radio"/> N <b>ms/msD</b>					
<b>WELL CONDITION CHECKLIST</b> (circle appropriate item(s), cross out if not applicable)							
Type: Flush Mount / <input checked="" type="radio"/> Sand Pipe      General Condition: <input checked="" type="radio"/> Good / <input type="radio"/> Needs Repair      Well Caps: <input checked="" type="radio"/> Good / <input type="radio"/> Broken / None      Lock: Good / Broken / <input checked="" type="radio"/> None							
Incidence of Rain Water Between Steel & PVC? <input type="radio"/> Y / <input checked="" type="radio"/> N      Is Well Plumb?: <input type="radio"/> Y / <input checked="" type="radio"/> N      PVC Riser: <input checked="" type="radio"/> Good / <input type="radio"/> Damaged / None							
Prevalence of Ponding Around Well? <input type="radio"/> Y / <input checked="" type="radio"/> N      Concrete Collar: <input checked="" type="radio"/> Good / <input type="radio"/> Cracked / <input type="radio"/> Leaking / None							
REMARKS:  <b>ms/msD</b>							



## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

\*PA stabilization parameters from EPA/540/S-95/50A April 1996

SAMPLING DATA			
SAMPLED BY (PRINT) / AFFILIATION <i>Carmen Harris</i>	SAMPLER(S) SIGNATURES <i>Carmen Harris</i>	SAMPLING INITIATED AT <i>11.13</i>	SAMPLING ENDED AT <i>12.02</i>
PUMP OR TURNING DEPTH IN WELL (feet) <i>66</i>	SAMPLE PUMP / PUMP RATE (ml per minute)	FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL # <i>YSI 6003C-4M L-north 241-4110</i>	
FIELD DECONTAMINATION <input checked="" type="radio"/> Y <input type="radio"/> N	FIELD FILTERED <input checked="" type="radio"/> Y <input type="radio"/> N FILTER SIZE <i>0.45</i>	Filtration Equipment Type <i>inline</i>	
MATERIAL CODES: AG = Amber Glass, CG = Clear Glass, PE = Polyethylene, PP = Polypropylene, S = Sarum, T = Teflon, O = Other (Specify)			
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)			
Type: Flush Mount / <u>Stand Pipe</u>	General Condition <u>Good</u> / Needs Repair	Well Caps: <u>Good</u> / Broken / None	Lock: <u>Good</u> / Broken / None
Evidence of Rain Water Between Steel & PVC? <u>Y</u> / <u>N</u>		Is Well Plumb? <u>Y</u> / N	PVC Riser: <u>Good</u> / Damaged / None
Evidence of Ponding Around Well? <u>Y</u> / <u>N</u>		Concrete Collar: <u>Good</u> / Cracked / Leaking / None	
REMARKS: <i>DUP-10/910-FIU</i>			

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



PROJECT NAME		PROJECT LOCATION		DATE		WELL ID	
JECT NUMBER		WELL DIAMETER (inches)		DEPTH TO WATER (feet)		DEPTH TO BOTTOM (feet)	
TUBING DIAMETER (inches)		TUBING MATERIAL CODE (see below)		PURGE PUMP TYPE		PUMP EQUIPMENT MODEL & SERIAL #	
WELL VOLUME PURGE: 1 WELL VOLUME= (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY		INITIAL PUMP OR TUBING DEPTH IN WELL (feet)		FINAL PUMP OR TUBING DEPTH IN WELL (feet)		PURGING INITIATED AT:	
WELL CAPACITY (Gallons Per Foot): 0.75 = 0.02, 1' = 0.04, 1.25' = 0.06, 2' = 0.16, 3' = 0.37, 4' = 0.65, 5' = 1.02, 6' = 1.47, 12' = 5.68		PURGING ENDED AT:		I GALLON = 3.785 LITERS		TOTAL VOLUME PURGED: GALLONS ~ 46 gal LITERS	
WATER LEVEL STABILIZATION		DEPTH TO WATER WITH PUMP (feet)		TIME INTERVAL (min)		FLOW RATE (mL/min)	
PUMP SETTINGS		DEPTH TO WATER (feet) START		DEPTH TO WATER (feet) END		Water Level Stable (Yes or No)	
VOLUME PURGED DURING INTERVAL (mL)		TIME		FLOW RATE (mL/min)		DEPTH TO WATER (feet)	
TURBIDITY (NTU)		DISSOLVED OXYGEN (mg/L)		PH		TEMP (°C)	
SPECIFIC CONDUCTIVITY (uS/cm)		ORP (mV)		COLOR (describe)		ODOR (describe)	
0-20 min		NA		R: 20, D: 10, PSI: 95, CPSI: 50		21.03 21.03 Yes 4500	
1035		225		21.03		615 1.40 6.33 11.86 692 -31.9 cloudy none	
1040		225		21.03		608 1.08 6.26 11.82 688 -31.9 cloudy none	
1045		225		21.03		651 0.44 6.28 11.78 689 -38.4 cloudy none	
1050		225		21.03		81 0.40 6.33 11.87 689 -37.5 cloudy none	
1055		225		21.03		68.8 0.41 6.34 12.00 691 -35.5 cloudy None	
1100		225		21.03		60.0 0.39 6.34 11.97 692 -39.4 cloudy None	
1105		225		21.03		43.7 0.35 6.35 12.00 692 -39.3 cloudy None	
1110		225		21.03		37.9 0.36 6.34 12.00 692 -38.5 little cloudy None	
1115		225		21.03		38.2 0.35 6.35 12.01 691 -38.7 little cloudy None	
1120		225		21.03		34.5 0.36 6.35 11.99 693 -38.6 little cloudy None	

### SAMPLING DATA

SAMPLED BY (PRINT) / AFFILIATION: Erin Foley / San Con		SAMPLER(S) SIGNATURE(S) Erin Foley		SAMPLING INITIATED AT 1125		SAMPLING ENDED AT 1202	
PUMP OR TUBING DEPTH IN WELL (feet) 72'		SAMPLE PUMP FLOW RATE (ml/min) 225 ml/min		WELL CHARACTER MONITORING EQUIPMENT MODEL & SERIAL NO. YSI (10 F07 m01) Turb (7N2364110)			
FIELD DECONTAMINATION <input checked="" type="radio"/> Y <input type="radio"/> N		FIELD FILTERED <input checked="" type="radio"/> Y <input type="radio"/> N Filtration Equipment Type		FILTER SIZE _____ µm		DUPLICATE <input checked="" type="radio"/> MS/MSD	
MATERIAL CODES AG = Amber Glass DG = Dark Glass PE = Polyethylene PP = Polypropylene S = Silicone T = Teflon O = Other (Specify)							
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)							
Type: Flush Mount / <input checked="" type="radio"/> Stand Pipe		General Condition: <input checked="" type="radio"/> Good / <input type="radio"/> Needs Repair		Well Caps: <input checked="" type="radio"/> Good / <input type="radio"/> Broken / <input type="radio"/> None		Lock: <input checked="" type="radio"/> Good / <input type="radio"/> Broken / <input type="radio"/> None	
Incidence of Rain Water Between Steel & PVC? Y / <input checked="" type="radio"/> N		Is Well Plumb? Y / <input checked="" type="radio"/> N		PVC Riser: <input checked="" type="radio"/> Good / <input type="radio"/> Damaged / <input type="radio"/> None			
Evidence of Ponding Around Well? Y / <input checked="" type="radio"/> N		Concrete Collar: <input checked="" type="radio"/> Good / <input type="radio"/> Cracked / <input type="radio"/> Leaking / <input type="radio"/> None					
REMARKS:							

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling



PROJECT NAME Foot Drains S/W		PROJECT LOCATION Ayer MA		DATE 10-9-10		WELL ID: SHM-10-11				
WELL NUMBER AC 001		WELL DIAMETER (inches) 2"		DEPTH TO WATER (feet) 40.83		DEPTH TO BOTTOM (feet) 63.13				
				PIC READING (ppmv)						
PURGING DATA										
TUBING DIAMETER (inches)		TUBING MATERIAL CODE (see below) PE		PURGE PUMP TYPE Bladder		PUMP EQUIPMENT MODEL & SERIAL NO. Cont (2916) Rame (10383)				
WELL VOLUME PURGE: 1 WELL VOLUME = (TOTAL WELL DEPTH - STATIC DEPTH TO WATER) X WELL CAPACITY				GALLONS		LITERS				
WELL CAPACITY (Gallons Per Foot): 0.75 * 0.02, 1" = 0.04, 1.25" = 0.06, 2" = 0.16, 3" = 0.32, 4" = 0.65, 5" = 1.02, 6" = 1.47, 12" = 5.88				1 GALLON = 3.785 LITERS		TOTAL VOLUME PURGED:				
WELL SCREEN INTERVAL DEPTH (feet): 52-62		INITIAL PUMP OR TUBING DEPTH IN WELL (feet) 57		FINAL PUMP OR TUBING DEPTH IN WELL (feet) 57		PURGING INITIATED AT: 1400				
						PURGING ENDED AT:  GALLONS: 3.25 gal LITERS				
WATER LEVEL STABILIZATION										
TIME INTERVAL (min)		FLOW RATE (mL/min)		PUMP SETTINGS PSIG - PSI/T -		DEPTH TO WATER (feet) START END				
0-10		400		R- D- PSIG- PSI/T- 2-10 A-S PSIG-50 PSI/T-95		40.88 40.88				
						Water Level Stable (Yes or No) YES				
						VOLUME PURGED DURING INTERVAL (mL) ~1500				
TIME (3-5 minutes)	FLOW RATE (mL/min) (100-500 mL/min)	DEPTH TO WATER (feet) (+/- 0.3")	TURBIDITY (NTU) (+/- 10%)	DISSOLVED OXYGEN (mg/L) (+/- 10%)	pH (+/- 0.1)	TEMP (°C) (+/- 1°C)	SPECIFIC CONDUCTIVITY (µS/cm) (+/- 1%)	DSP (mV) (+/- 10mV)	COLOR (describe)	ODOR (describe)
1415	400	40.88	38.3	0.82	5.20	11.66	416	116.2	clear	None
1420	400	40.88	13.7	0.41	6.40	11.60	418	-42.5	Clear	None
1425	400	40.88	10.29	0.44	6.28	11.60	417	-41.3	Clear	None
1430	400	40.88	8.24	0.42	6.29	11.50	416	-42.3	Clear	None
1435	400	40.88	6.00	0.40	6.22	11.54	415	-41.1	Clear	None
1438	400	40.88	4.97	0.47	6.24	11.57	414	-39.1	Clear	None
1441	400	40.88	4.29	0.46	6.28	11.51	414	-40.8	Clear	None
1444	400	40.88	4.22	0.41	6.25	11.57	414	-42.1	Clear	None

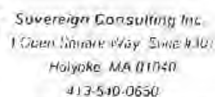
<sup>a</sup> A stabilization parameters from EPA/640/S-95/504 April 1996

SAMPLED BY (PRINT) / AFFILIATION Ena Piny		SAMPLER(S) SIGNATURE(S) Ena Piny		SAMPLING DATA 1445		SAMPLING INITIATED AT 1455	
PUMP OR LIFTING DEPTH IN WELL (feet) 57'		SAMPLE PUMP FLOW RATE (gal per minute) 400ml/min		FIELD PARAMETER MONITORING EQUIPMENT MODEL & SERIAL # 75110F07md) TWTX 2023164 110)			
FIELD DECONTAMINATION <input checked="" type="checkbox"/> N		FIELD FILTERED <input checked="" type="checkbox"/> N Filtration Equipment Type		FILTER SIZE _____ µm		DUPLICATE <input checked="" type="checkbox"/> <input checked="" type="checkbox"/>	
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)							
Type: Flush Mount / Stand Pipe      General Condition: Good / Needs Repair      Well Caps: Good / Broken / None      Lock: Good / Broken / None							
Presence of Rain Water Between Steel & PVC? Y / N      Is Well Plumb? Y / N      PVC Riser: Good / Damaged / None							
Evidence of Ponding Around Well? Y / N      Concrete Collar: Good / Cracked / Leaking / None							
REMARKS:							





### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

## MONITORING WELL SAMPLING LOG

### Low Flow Sampling

[illegible]

\*PA stabilization parameters from EPA/540/S-95/504 April 1996

SAMPLING DATA	
SAMPLED BY (PRINT) / AFFILIATION: <i>Carolyn Hardt</i>	SAMPLER(S) SIGNATURES: <i>Carolyn Hardt</i>
SAMPLING INITIATED AT: <i>10:35</i>	SAMPLING ENDED AT: <i>11:00</i>
PUMP OR TUBING IN THE WELL (feet): <i>52</i>	SAMPLE PUMP FLOW RATE (ml per minute): <i>400</i>
FIELD DECONTAMINATION / REMOUNTING EQUIPMENT MODEL & SERIAL #: <i>Lamotte 2/2012 241-4110 YS1566 10P07M01</i>	
FIELD DECONTAMINATION: <input checked="" type="radio"/> N	FIELD FILTERED: <input checked="" type="radio"/> N FILTER SIZE: <i>0.45</i>
Filtration Fragment Type: <i>In-line</i>	
DUPLICATE: <input checked="" type="radio"/> N	
MATERIAL CODES: AG - Amber Glass, CG - Clear Glass, PE - Polyethylene, PP - Polypropylene, S - Silicon, T - Teflon, O - Other (Specify)	
WELL CONDITION CHECKLIST (circle appropriate item(s), cross out if not applicable)	
Type: Flush Mount / <u>Stand Pipe</u> General Condition: <u>Good</u> / Needs Repair / <del>Bad</del> Well Caps: <u>Good</u> / Broken / None Lock: <u>Good</u> / Broken / None	
Evidence of Rain Water Between Steel & PVC? Y / <u>N</u> Is Well Plumb? <u>Y</u> / <del>N</del> PVC Riser: <u>Good</u> / Damaged / None	
Evidence of Ponding Around Well? <u>Y</u> / N Concrete Collar: <u>Good</u> / Cracked / Leaking / None	
REMARKS: <i>DUP-102010-F/U</i> <i>Collected 10 gallons of H<sub>2</sub>O for As Tests</i>	